




<b>Contractor:</b>  <b>TIANCHEN CORP. CHINA</b>	<b>Project :</b>	<b>MKP Methanol Project</b>			<b>Owner :</b>  شرکت کیمیای پارس خاورمیانه <i>Middle East Kimiya Para Co.</i>
	<b>Unit</b>	<b>General Technical</b>	<b>Phase</b>	<b>Detail Engineering</b>	
	<b>Doc. Title :</b>	<b>PACKAGE HAZOP</b>			
<b>Vendor :</b>  新鼎信息技术(上海)有限公司 <i>Advanced Control &amp; Information Technologies Co., Ltd.</i>	<b>Owner No.</b>	<b>MKP-11-DE-9000-SF-RPT-001B</b>			
	<b>Contr. No.:</b>	<b>MKP-11-DE-9000-SA01-RPT-001B</b>			
	<b>Vendor No.</b>	<b>16E2416A</b>			
				<b>Rev. : 0</b>	<b>Page : 1 of 25</b>

# PACKAGE HAZOP

REV.	DATE	PURPOSE OF ISSUE	PREPARE	CHECK	REVIEW	APPROVE
0	05-04-2017	Approved for Construction	YING YI NING	Wang Shih Huang	Wang Shih Huang	
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## Objectives

The objective of this HAZOP project is Advanced Control and Information Technology, Inc. (ACIT) to contract TCC in conducting HAZOP study as well as the layer of protection analysis (LOPA) on “MEKPCO Methanol Project”. In order to finalize the design of process packages, it is imperative to have a third party conduct Hazard and Operability (HAZOP) study, so that the fitness of safety and risk control measures in the detailed design can be verified. Process and utility systems should include vendor packages. They are the subject of this second HAZOP when details are available.

The analysis methodology of HAZOP as implemented in this project is in accordance with relevant requirements of “Hazard and operability studies (HAZOP studies)—Application guide” (IEC 61882-2003), AIChE CCPS “Guidelines for Hazard Evaluation Procedures” (2008), and the assignment of required Safety Integrity Level (SIL) for Safety Instrumented System (SIS) is in accordance with “Functional safety—Safety instrumented systems for the process industry sector” National Standard (IEC 61511-2016).

## Scope

The assessment scope includes Recycle hydrogen compressor C-2002, Start-up nitrogen compressor C-2001, Flue gas blower and turbine F-2001/FT-2001, Combustion air blower and turbine F-2002/FT-2002, Synthesis compressor package, P-7001A/B/C (BFW pump package), Turbine for P-0501 1/2 (CW pump), Flare system, POC, Polishing Unit and Cooling water system in “MEKPCO Methanol Project”. Description of each node and its associated P&ID’s are shown below.

Node ID_NO	Node Description	Relative Equipments	P&ID	Remark
2007	Recycle hydrogen compressor C-2002	C-2002, MC-2002, D-2070, D-2072, D-2071, D-2073, E-2070, D-2074, D-2075.	MKP-VD-9000-306-00 3-A1~MKP-VD-9000-3 06-007-A1	
2008	Start-up nitrogen compressor C-2001	C-2001	MKP-11-DE-9000-RE- REQ-308, 0514-JA 16704-PID	
2009	Flue gas blower and turbine F-2001/FT-2001	FT-2001, MP-1001, GB-1001, OT-1002, F-2001, MF-2001, OT-1001, AP-1001, OC-1001A/B, OF-1001A/B.	MKP-VD-2000-351-14 5-A1, SH-3~5; MKP-VD-2000-351-30 2-A0	

2010	Combustion air blower and turbine F-2002/FT-2002	FT-2002, MP-2001, GB-2002, OT-2002, F-2002, MF-2002, OT-2001, AP-2001, OC-2001A/B, OF-2001A/B.	MKP-VD-2000-351-12 0-A1, SH-3~5; MKP-VD-2000-351-30 3-A0	
3006	Synthesis compressor package	D-3011, E-3012, C-3001, E-3014, D-3012, C-3002-1, C-3002-2, E-3013, TK-3002, P-3013A/B, PM-3013A/B, E-3018A/B, X-3002A/B, D-3013, P-3012, PM-3012, D-3014, TK-3001, FT-3001, P-3014, PM-3014, E-3011, D-3015, E-3020, P-3011A/B, PM-3011A/B, J-3004, J-3005A/B, J-3006A/B, X-3004A/B, P-3015, E-3021A/B/C, X-3005A/B, E-3016, E-3022A/B/C.	SOK0887013, SH2~7; SOK0880159, SH5~14.	
7007	P-7001A/B/C (BFW pump package)	P-7001A/B/C, FT-7001A/B	DGN-P&ID-DST-01	
7008	Turbine for P-0501 1/2 (CW pump)	P-0501 1/2, FT-0501 1/2	DGN-P&ID-DS-01	
7009	Flare system	D-8511, P-8511, D-8501, E-8501, FL-8501, FL-8502, FL-8503, D-8502, X-8501, PIL-8501A~D.	MKP-11-DE-8500-PR-PID-001~005.	
7010	POC	PD-9401, PD-9402, PD-9403, PD-9404, PD-9406, PD-9407, PD-9408, PD-9409, PD-9410, PD-9411, P-9401A/B, P-9402A/B, P-9403A/B, P-9404A/B, P-9408A/B, P-9409A/B, P-9411.	MKP-11-DE-9400-PR-PID-002	
7201	Polishing Unit	TK-7001 1/2, P-7002A/B,	7200-PID-001 ~ 005	



		P-7204A/B, TK-7202/7204, P-7202/7203, J-7201/7202, D-7205, PD-7206, P-7205A/B, TK-7201, P-7201A/B, R-7201A/B, X-7201, E-7201A/B		
0501	Cooling water system(Side filter of cooling tower)	F-0502 1/2	0500-PID-005;	

## Methodology

The description of HAZOP and LOPA assessment methodology as applied in this project is as follows.

1. Qualitative analysis: traditional HAZOP analysis method is applied to each process node. Guidewords (refer to the Attachment) are used to probe for potential process deviations in the node. List all possible causes for the process deviation, analyze its related hazardous consequences and identify existing safeguards that prevent the process deviation from occurring.
2. Assess the risk following the definitions listed in Tables 2~5. First determine the severity level of the hazard following Table 4, and by doing so one can determine its tolerable risk target (refer to Table 5).
3. If there is a dispute over the severity level in the process of determining severity level of the hazard following Table 4, or if the consequence under discussion is deemed a critical hazardous event by the assessment team, proceed with model-based consequence analysis.
4. For consequence with severity level 4 or above, proceed to LOPA. The assessment team can also proceed to LOPA for the consequence with severity level 3, if necessary.
5. LOPA format in IEC 61511-3 appendix F should be followed.
6. Principle and guidance listed below for each LOPA item should be considered,
  - (1) Impact event description - following the consequence in a process deviation from the HazOp study
  - (2) Severity - following the severity level for the consequence from the HazOp study
  - (3) Initiating cause - all potential causes for a process deviation from the HazOp study. Each cause will be discussed accordingly.
  - (4) Initiation likelihood – values of the typical initiating cause failure rate can be looked up from Mr. Safety software database. Alternatively, one can refer to

*“Layer of Protection Analysis: Simplified Process Risk Assessment(2001)”*  
published by AIChE.

- (5) General process design – check to see if the process area for the initiating cause or impact event under discussion is designed with explosion proof classification, double cannula for toxic or incompatible material leakage prevention, vessel wall thickness or attached with refractory material or any other intrinsically safer design in accordance with the general safety design specifications such as API, ASME or NFPA. Such design must be independent and effective for protection against the event under discussion. Yes(0.1); No(1)
  - (6) Basic process control system (BPCS) – check to see if in addition to the control system that fails, there is any other relevant monitor and control system such as DCS, PLC or PANEL to prevent or mitigate the hazardous event, and such monitor and control system is independent and effective. Yes(0.1); No(1)
  - (7) Alarm, etc. – check to see if there is any independent safety system alarm in addition to the automatic operating system from item 4 or item 6, and if there is corresponding SOP to complement the alarm in preventing or mitigating the impact event under discussion. Yes (0.1); No(1)
  - (8) Additional mitigation, restricted access – external mitigation measures with a lower degree of reliability such as working permit or restricted access to the operating area during process operation, etc. Such additional mitigation measures must be implemented against the initiating cause. Look for the additional mitigation data table in Mr. Safety software database. Alternatively, one can refer to *“Layer of Protection Analysis: Simplified Process Risk Assessment(2001)”* published by AIChE
  - (9) IPL additional mitigation, dike, pressure relief – mitigating system with a higher degree of reliability such as dike, safety relief valve, rupture disc or automatic firefighting sprinkler system. The failure rate of IPL additional mitigation must be less than or equal to 0.01. Look for IPL data table in Mr. Safety software database. Alternatively, one can refer to *“Layer of Protection Analysis: Simplified Process Risk Assessment(2001)”* published by AIChE
  - (10) Intermediate event likelihood – the product of multiplying assigned values of item 4 through item 9
  - (11) Safety Instrumented Function (SIF) Integrity Level –Probability of Failure on Demand (PFD) and the Safety Integrity Level (SIL) that corresponds to it
  - (12) Mitigated event likelihood – possibility of failure event in which all the risk control measures are in effect. The risk must be less than or equal to the tolerable risk target (Table 4).
7. Check the mitigated event likelihood against Table 4 to see if the risk meets the tolerable risk target.
- 8.If the risk of the mitigated event likelihood meets (less than or equal to the frequency of) the tolerable risk target, then determine the likelihood level based on Table 2, determine the risk class based on Table 1 and check whether the risk class is within 4. Also, if necessary, provide safety improvement recommendations with

regards to the operation

9. In case that the risk of the mitigated event likelihood does not meet (less than or equal to the frequency of) the tolerable risk target, then determine the required safety integrity level (SIL) as follows

$$(\text{Intermediate event likelihood}) = (\text{Mitigated event likelihood}) \times \text{RRF}$$

Where RRF = Risk Reduction Factor

$$\text{PFD} = 1/\text{RRF}$$

Proceed to determine the required SIL for the safety instrumented function (SIF) or other risk prevention or mitigation measures with a PFD that is equivalent to this SIL, and provide safety improvement recommendations. HAZOP and LOPA assessment workflow is depicted below in figure 1

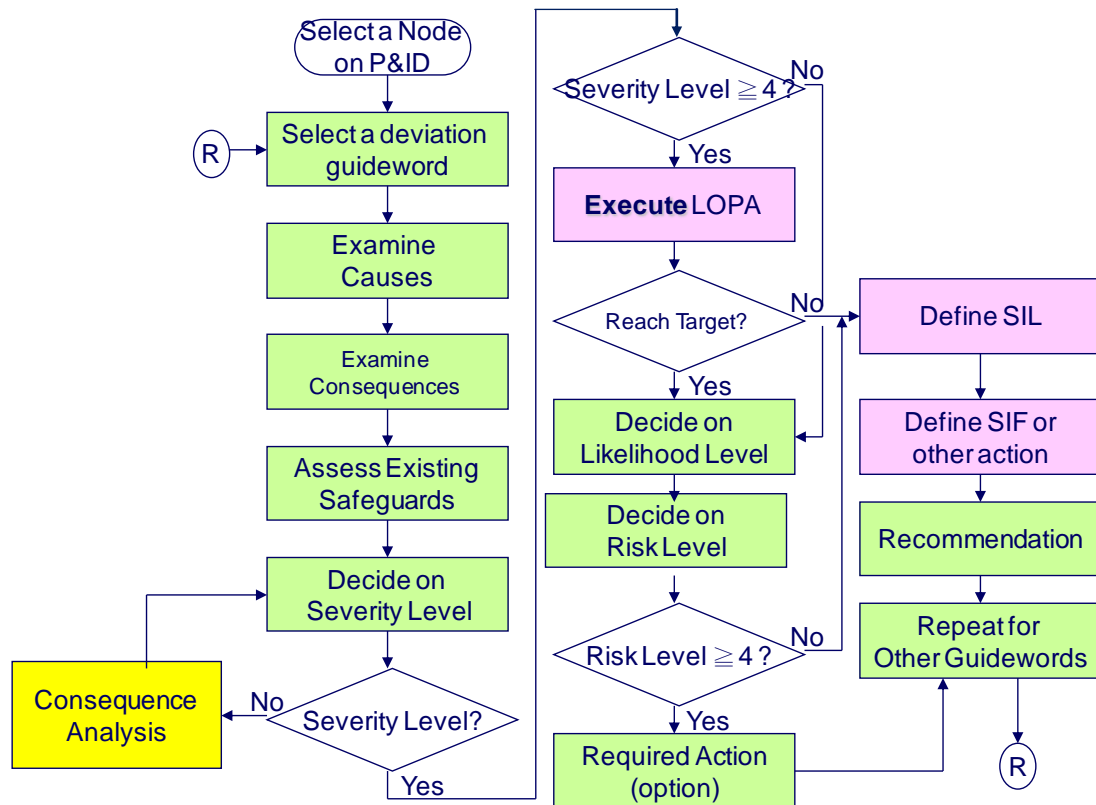


Figure 1 HAZOP/LOPA Assessment Workflow

Table 2 Risk Matrix

Risk matrix		Likelihood							
		1	2	3	4	5	6	7	8
Severity	7	4	5	6	7	7	7	7	7
	6	3	4	5	6	7	7	7	7
	5	2	3	4	5	6	7	7	7
	4	1	2	3	4	5	6	7	7
	3	1	1	2	3	4	5	6	7
	2	1	1	1	2	3	4	5	6
	1	1	1	1	1	2	3	4	5

Note:

	<b>PFD<sub>avg</sub></b>	<b>RRF</b>	<b>Typical implementation</b>
A1	No requirement	No minimum	Alarm only
A2	No requirement	No minimum	DCS action
SIL1	$0.01 \leq \text{PFD} < 0.1$	$100 \geq \text{RRF} > 10$	Trip separate from DCS
SIL2	$0.001 \leq \text{PFD} < 0.01$	$1000 \geq \text{RRF} > 100$	Trip separate from DCS
SIL3	$0.0001 \leq \text{PFD} < 0.001$	$10000 \geq \text{RRF} > 1000$	Redundant trip separate from DCS
B, SIL4			Single SIF is not sufficient, design other protection layers

(PFD<sub>avg</sub>: Average Probability of Failure on Demand)

Table 3 Likelihood Level

	Description	Lower limit $10^{-x}(\geq)$	Upper limit $10^{-y}(<)$
1	Unlikely	7	6
2	Very rare	6	5
3	Rare	5	4
4	Maybe	4	3
5	Possible	3	2
6	Very possible	2	1
7	Frequently	1	0
8	Very frequently	0	0

Table 4 Severity Classification

	Description	Personnel Safety	Financial loss/ US dollar	Environmental influence	Tolerabl e target
1	Negligible	Injury=1	< 50,000	Equipment leakage	0.1
2	Moderate	1 < injury < 5	50,000~100,000	Unit leakage	0.01
3	Highly	Permanent partial disability $\geq 1$ or Temporarily disability < 5	100,000~1 million	Plant leakage	0.001
4	Significant	1 death; Permanent partial disability or temporarily disability $\geq 5$	1 million~10 million	Pollution confined in plant	0.0001
5	Massive	2~4 death or permanent disability	10 million~100 million	Regional pollution; >10,000 bbl oil spill	1E-05
6	Severe	5~29 death or permanent disability	100 million~1 trillion	National pollution; >100,000 bbl oil spill	1E-06
7	Extremely severe	$\geq 30$ death or permanent disability	> 1 trillion	single equipment leakage	1E-07

Table 5 Tolerable Risk Target

Risk Class	Description	Tolerable Frequency Target (/year)
7	Extremely severe / C <sub>G</sub>	< 10 <sup>-7</sup>
6	Severe / C <sub>F</sub>	< 10 <sup>-6</sup>
5	Massive / C <sub>E</sub>	< 10 <sup>-5</sup>
4	Significant / C <sub>D</sub>	< 10 <sup>-4</sup>
3	Highly / C <sub>C</sub>	< 10 <sup>-3</sup>
2	Moderate / C <sub>B</sub>	< 10 <sup>-2</sup>
1	Negligible / C <sub>A</sub>	< 10 <sup>-1</sup>

## Team Member

### Leader –

Wang Shih Huang (consultant for Advanced Control and Information Technology, Inc. (ACIT)), ACIT is a member of CTCI Group)

Mr. Wang has over 24 years of experience in the oil and gas industry in the area of PHA/HAZOP. Prior to joining ACS, he had served as Department Manager for Industrial Safety Technology Department of Industrial Technology Research Institute in Taiwan (ITRI). He has participated in the following projects,

- (1) Project leader, RDS2 Process Safety Evaluation in Taoyuan Refinery, Taiwan CPC, 1991~1992
- (2) Project leader, Alkylation and Dehydrogenation Process Safety Evaluation, Taiwan Styrene Monomer Corporation, 1992~1996.
- (3) Project leader, PP Process Safety Evaluation, Taiwan Polypropylene Inc., 1994~1995.
- (4) Project leader, SBR/BR/TPE Process Hazard Analysis and Risk Assessment, Taiwan Synthesis Rubber Corporation, 1995~1998.
- (5) Auditor and Advisor, PSM Promotion Program and PTA3 HAZOP Review, CAPCO, 1996~1998.
- (6) Project leader, Semiconductor Process Safety Evaluation, Tsmc, 1998~2000.
- (7) Project leader, Liquid Chlorine Transportation QRA, Taiwan DuPont Inc., 2004.
- (8) Project leader, Earth Covered Tanks Quantitative Risk Analysis, FPCC, 2006~2008.
- (9) Project leader, Synlubes Process HAZOP, Cognis Shanghai, 2008.
- (10) Project leader, Ammonia ISO Tank Transportation QRA, Praxair, 2010.
- (11) Assessor, Nitrous Acid Process HAZOP, Taiwan Fertilizer CO., 2010.
- (12) Project leader, Alkylation Process HAZOP and LOPA in Talin Refinery, Taiwan

CPC, 2010~2011.

- (13) Advisor, Mr. Safety – Computer-aided HAZOP/LOPA Software Development, Advanced Control & Systems Inc., 2010~2012.
- (14) Coach, HAZOP Training Program and Workshop, Dowcorning Shanghai, BP/CNOOC Shenzhen, Conocophillips Beijing, Lanxess Qindao, and CNOOC Zhanjiang/Teinjing, 2004~2011.
- (15) Project leader, NO.10 SRU LOPA/SRS, RBI, FMEA/CA in Talin Refinery, Taiwan CPC, 2012~2013.
- (16) Project leader, SNG (Substitute Natural Gas) HAZOP in Xinjiang Yi Nan, ECEC, 2012.
- (17) Project leader, YUTAI Large Scale Natural Gas Liquefaction Technology Engineering Project HAZOP, CTYC, 2013.
- (18) China huaneng Methanol Produce FMTP Process HAZOP, TCC, 2013.

**Scribe –**

Ying Yi Ning 、 Tracy Xie, Jay Liu, Gene Zhang (ACIT)

**Core Team Members –**

Owner:

Engineering Manager: Mahmood Nasrollahi

Process Engineers: Mojtaba Lame 、 Morteza Faghihi

Instrumentation Engineer: Mehdi Movahedi 、 Jalal Behrouzfar

Contractor:

Project Manager: Ji Quangong

Chief Engneer: Lin Binbin

Project Executive Manager: Liu Wei

Engineering Manager: Ai Xiaoxin

Deputy Engineering Manager: Gao Zhihui

HSE Engineer: Ji Weiwei 、 Liu Xianfan

Process Engineers : Xu Hang 、 Tian Tao 、 Jiang yu 、 Xu Yekun 、 Wang Furui 、 Chen Tao 、 Xu Jun 、 Xu Binghao 、 Li Zhijuan

Instrumentation Engineer: Ma Guoqiang 、 Qin yajun

Machinery Engineer: Feng Wei

Experts:

ITT: Valerio Cicono 、 Marcelo Della Coletta 、 Wendy Xie

CW-Hydro: Sun Sy

SYCC: Pan Yi Sia 、 Zheng nai chao

SBW: Li Yueyong 、 Bai Lin 、 Zhang Enyuan

GE: Gluseppe Stella 、 Medagcioni Marta 、 Gaia Cdetti 、 Luca Conti

## Schedule and Deliverables

### Schedule

Date and Time	Agenda
Feb 20, 2017	HAZOP LOPA for Node 2009 / Flue gas blower and turbine F-2001/FT-2001.
Feb 21, 2017	HAZOP LOPA for Node 2010/ Combustion air blower and turbine F-2002/FT-2002.
Feb 22, 2017	HAZOP LOPA for Node 7007/ P-7001A/B/C (BFW pump package), Node 7008/ Turbine for P-0501 1/2 (CW pump), Node 7009/ Flare system.
Feb 23, 2017	HAZOP LOPA for Node 2007/ Recycle hydrogen compressor C-2002.
Feb 24, 2017	HAZOP LOPA for Node 2008/ Start-up nitrogen compressor C-2001.
Feb 27, 2017	HAZOP LOPA for Node 7201/ Polishing Unit.
Feb 28, 2017	HAZOP LOPA for Node 7010/ POC, Node 0501/ Cooling water system
Mar 1, 2017   Mar 3, 2017	HAZOP LOPA for Node 3006/ Synthesis compressor package.

### Output:

Reforming Process Section: HAZOP LOPA analysis – 4 process nodes, 64 process deviations and 15 pcs of P&ID completed;

Methanol Synthesis Loop Process Section: HAZOP LOPA analysis – 1 process nodes, 60 process deviations and 16 pcs of P&ID completed;

Utility Process Section: HAZOP LOPA analysis – 4 process nodes, 52 process deviations and 8 pcs of P&ID completed;

Polishing Process Section: HAZOP LOPA analysis – 1 process nodes, 30 process deviations and 5 pcs of P&ID completed;

Cooling Water Process Section: HAZOP LOPA analysis – 1 process nodes, 5 process deviations and 1 pcs of P&ID completed.



Deliverables:

HAZOP Worksheet, please refer to Attachment 2.

### Recommendations

Serial #	Risk	Recommendation	Accept	Not accept	Alternative/Comment	Follow up
501.3	3	Develop SOP for proper adjusting CW distribution in case of two pumps running and low plant loading situation.	Y			TCC
501.5	3	Add AT-0511 low pH alarm and interlock to auto-stop H <sub>2</sub> SO <sub>4</sub> injection pump.	Y			TCC
501.9	3	Add AT-0511 low pH alarm and interlock to auto-stop H <sub>2</sub> SO <sub>4</sub> injection pump.	Y			TCC
501.10	2	TCC to check: relation between ClO <sup>-</sup> and Cl <sup>-</sup> concentration and relevant reactions (for NaClO dosing in CW).	Y			TCC
501.12	3	Add high alarm to PIA-0514.	Y			TCC
501.13	2	1.Add TE-0511 low temperature alarm. 2.Add PT-0511 low pressure alarm.	Y			TCC
501.17	3	1.Lines from each filter to PD-0502 for discharge of CSW shall be sloped down towards PD-0502.	Y			TCC

501.18	1	Add flow indicator for FT-0516.	Y			TCC
501.23		HAZOP study should be done by vendor for CW filter system package, the owner will check CW filter package after receiving vendor data.	Y			TCC
3006.1	3	1.TCC and GE to review the IS-40 partial trip category (high level of liquid separator, high flow) of compressor 2.LT-3700A/B/C(2oo3) level high high trip, SIF should meet SIL 1.	Y			TCC/GE
3006.4	3	Handvalves at the recycle gas suction and discharge lines should be locked open.	Y			TCC/GE
3006.11	3	Handvalve at the discharge of 2nd stage compressor(C-3002-1) should be lock open.	Y			TCC/GE
3006.12	4	Add a PSV at the discharge of C-3002-2 or use PSHH-3747 high high pressure trip with SIL2.Those two solutions shall be discussed among GE, Owner and TCC.	Y			TCC/GE

3006.14	3	Add high level alarm at pot of sub flare header of compressor house area 3000 and show this pot on P&ID no. 8500-PID-002.	Y			TCC
3006.19	3	Add high temperature alarm on TT-3744.	Y			GE
3006.21	3	Add high temp. alarm for TI-3722.	Y			GE
3006.24	3	to check the capacity of the breathing valve according to the max. gas blow.	Y			TCC
3006.26	3	to check the capacity of the breathing valve according to the max. gas blow.	Y			TCC
3006.32	3	GE provide the information about the oil quantity between the main pumps suction loss level and emergency pump suction loss level.	Y			GE
3006.47	2	Operation Procedure should be placed that stop the steam turbine and remove the vacuum from the condenser in case of loss of LP steam. (To be mentioned in GE operation manual of the compressor package, and incorporated in the plant operation manual.)	Y			GE

2007.3	3	1.Add the branch suction line for AOP with strainer and valve in each line. 2.Add check valve on pump P-2004B discharge.	Y			SYCC
2007.5	3	TIA-2701/2703 add high high temperature trip.	Y			SYCC
2007.9	2	PIAS-2703 add high pressure alarm.	Y			SYCC
2007.11	3	PIAS-2703 add low pressure alarm.	Y			SYCC
2007.12	3	TIA-2701/2703 add high high temperature trip.	Y			SYCC
2007.14	2	Add LST-2474A/B/C (medium of three) high high alarm and trip C-2002 by way of DCS during start-up.	Y			TCC/SYCC
2007.16	2	1.Add level switch for crank shaft tank with low trip. 2.Forbdden to start compressor when the oil level is low.	Y			SYCC
2007.17	2	PT/PI-2706/2707 add low pressure alarm.	Y			SYCC
2008.2	3	1.Revise P&ID to show alarm and interlock for temperature, pressure and flow if any. 2.Add alarm high and high high trip for TT-2579.	Y			SBW

2008.4	2	Show check valve and manual valve on 2000-PID-018	Y			TCC
2008.7	2	PI-2579 add high pressure alarm.	Y			SBW
2008.9	1	Lube oil supply main line PT-9672 add high pressure alarm.	Y			SBW
2008.13	2	Show the autostart of lube oil heater in P&ID.	Y			SBW
2008.15	3	LS-9671 low level alarm change to low low level trip.	Y			SBW
2009.3	2	PDI-2811 add high d/p alarm.	Y			ITT
2009.7	1	Add desuperheater on the LP steam header.	Y			TCC
2009.8	1	1.PDI-2811 add high d/p alarm. 2.Add TI-2801 low temperature alarm.	Y			ITT
2009.9	2	Add blind flange after the drain valve.	Y			ITT
2009.13		Due to incomplete data of P&ID for MF-2001, it will be checked later. TCC shall be issued completed P&ID like other MV motors of plant and consider auto start and relevant signals for it.	Y			ITT/TCC
2010.3	2	PDI-2861 add high d/p alarm.	Y			ITT

2010.7	1	Add desuperheater on the LP steam header.	Y			TCC
2010.8	1	1.PDI-2861 add high d/p alarm. 2.Add TI-2862 low temperature alarm.	Y			ITT
2010.9	2	Add blind flange after the drain valve.	Y			ITT
2010.13		Due to incomplete data of P&ID for MF-2002, it will be checked later. TCC shall be issued completed P&ID like other MV motors of plant and consider auto start and relevant signals for it.	Y			ITT/TCC
2010.14	2	Add PICA-2163 high pressure alarm.	Y			ITT/TCC
7007.1	3	Add high pressure alarm and high high pressure trip at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.	Y			CW-Hydro
7007.2	3	Add high pressure alarm and automatic stop auxiliary oil pump.	Y			CW-Hydro

7007.4	3	1.Cancel PSL-7710A/B/C switch. 2.Use transmitter instead of all switch(PDT-7710A/B/C, PT-7710A/B/C, 7720A/B/C, 7730A/B/C and others). 3.PT-7710A/B/C, 7720A/B/C, 7730A/B/C (medium of 3) low pressure alarm and start the auxiliary oil pump, low low pressure(2oo3) to trip.	Y			CW-Hydro
7007.6	3	Add high temperature alarm and high high temperature trip at turbine inlet pipe.	Y			CW-Hydro
7007.7	2	Add TT high temperature alarm and high high temperature trip at turbine outlet pipe.	Y			CW-Hydro
7007.8	2	Add low temperature alarm and auto start oil heater EH-7001A/B/C.	Y			CW-Hydro
7007.9	2	Add low level alarm and low low level trip for LSL-7710A/B/C.	Y			CW-Hydro

7007.11	3	1.Add low pressure and low temperature alarm at turbine inlet utilizing inlet PT and TT to send signal to CW-Hydro PLC. 2.Add minimum allowable low continuous speed alarm.	Y			CW-Hydro
7007.13		Due to absence of CW-Hydro representative in HAZOP meeting, some HAZOP items will be checked by Owner later. As the latest P&ID of vendor are not received in HAZOP meeting, further recommendations can be stated later. TCC should prepare the latest P&IDs of this package and send them to Owner during two weeks.	Y			CW-Hydro / TCC
7008.1	3	Add high pressure alarm and high high pressure trip at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.	Y			CW-Hydro
7008.2	3	Add high pressure alarm and automatic stop auxiliary oil pump.	Y			CW-Hydro



7008.3	3	Add low pressure alarm at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.	Y			CW-Hydro
7008.4	3	1.Cancel PSL-0541 1/2 switch. 2.Use transmitter instead of all switch(PDT-0541 1/2, PSL-0541 1/2, 0542 1/2, 0543 1/2 and others). 3.PT-0541 1/2, 0542 1/2, 0543 1/2 (medium of 3) low pressure alarm and start the auxiliary oil pump, low low pressure(2oo3) to trip.	Y			CW-Hydro
7008.6	3	Add high temperature alarm and high high temperature trip at turbine inlet pipe.	Y			CW-Hydro
7008.7	2	Add TT high temperature alarm and high high temperature trip at turbine outlet pipe.	Y			CW-Hydro
7008.8	2	Add low temperature alarm and auto start oil heater EH-0501 1/2.	Y			CW-Hydro
7008.9	2	Add low level alarm and low low level trip for LSL-0541 1/2 .	Y			CW-Hydro

7008.11	3	1.Add low pressure and low temperature alarm at turbine inlet utilizing inlet PT and TT to send signal to CW-Hydro PLC. 2.Add minimum allowable low continuous speed alarm.	Y			CW-Hydro
7008.13		Due to absence of CW-Hydro representative in HAZOP meeting, some HAZOP items will be checked by Owner later. As the latest P&ID of vendor are not received in HAZOP meeting, further recommendations can be stated later. TCC should prepare the latest P&IDs of this package and send them to Owner during two weeks.	Y			CW-Hydro / TCC
7009.2	3	Add another level transmitter of D-8511 with high level alarm.	Y			TCC
7009.7	4	PG-8541 change to PT-8541 and send a signal to PLC and add high pressure alarm.	Y			TCC
7009.8	3	PG-8541 change to PT-8541 and send a signal to PLC and add low pressure alarm.	Y			TCC

7009.11	3	Vendor to advise: TIAS/TV-8544 as a safeguard.	Y			TCC
7009.13		HAZOP study should be done by vendor for flare gas system package, the owner will check flare package after receiving vendor data.	Y			TCC
7010.9	2	1.Add plant air connection for portable pumps.	Y			TCC
7010.13		1.Consider curb with anti-acid brick for H2SO4 solution tank and NaOH solution tank.	Y			TCC
7201.3	2	1.Add a temperature transmitter and send the signal to control room, set high alarm in the 8"-TC-72-201-B50-N inlet line of X-7201A/B and X-7204.	Y			TCC
7201.5	3	1.Change FIQ-7204 to FI-7204.	Y			TCC
7201.6	2	1.Add low alarm for FT-7205.	Y			TCC
7201.7	2	1.Add low alarm for FI-7201. 2. Add FI and low alarm for FI-7204 (DMW from B.L)	Y			TCC
7201.8	2	1.Add low alarm for FT-7203A/B.	Y			TCC

7201.9	2	1.Add check valve on 8"-DMW-70-108-B50-N of 7000-PID-020.	Y			TCC
7201.10	2	1.Add check valve on 8"-TC-72-201-B50-N. 2.P-3011A/B should be considered as auto start(should be confirmed with GE).	Y			TCC
7201.11	3	Supply chemical from well known vendor, with high quality and test before use in plant.	Y			TCC
7201.12	2	1.Add alarm high for PT-7202. 2. Correct setpoint of PSV-7205 and PSV-7206A/B to 10 barg.	Y			TCC
7201.13	2	1.Add alarm high for PT-7203. 2.Correct setpoint of PSV-7205 and PSV-7206A/B to 10 barg.	Y			TCC
7201.14	3	1.Add alarm high for PT-7207A/B. 2. Correct setpoint of PSV-7203A/B to 7 barg.	Y			TCC
7201.15	1	1.Correct design pressure of discharge line from P-7002A/B to 14 barg.	Y			TCC
7201.23	2	1.Add high alarm for AT/AI-7208. 2.Add high alarm for AT/AI-7209.	Y			TCC

7201.30		1.HAZOP study should be done by vendor for polishing unit package, the owner will check polishing unit package after receiving vendor data.	Y			TCC
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Attachment 1  
Process Deviation Guidewords

High Flow  
Low/ No Flow  
Mal-distributed Flow  
Incorrect Flow Direction  
Reverse Flow  
Part of Flow/Composition  
As well as Flow/Impurity  
Other than Flow/Incorrect Substance  
High Concentration  
Low Concentration  
High Pressure  
Low Pressure  
Vacuum  
High Temperature  
Low Temperature  
High Level  
Low/ No Level  
Heat Exchanger Tube Rupture/ Leak  
Plate Heat Exchanger Failure  
Action Not Execute  
Extra Execute Action  
Rupture/ Leak  
Other

Attachment 2  
HAZOP Worksheet



# HAZOP analyzing record

2017/2/28

Project name : MKP Methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Cooling Water Unit

Node description Cooling water system

Drawing no : 0500-PID-001~005;7000-PID-016

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n F-0501A/B/C/D, T-0501A/B/C/D, PD-0501, P-0501 1/2, P-0502A/B, P-0504A/B, F-0502 1/2, P-0505A/B, PD-0502, P-0506A/B, TK-0503, P-0507, TK-0508, P-0510A/B, TK-0509, P-0511A/B, TK-0510, P-0512A/B, E-0501

Design purpos Cooling water circulating, CW supply 38 degree C, CW return 48 degree C, Cl- less than 65 mg/L.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
501 . 1	High flow(CW)	1 1.Incorrect pump selection which lead to high flow, pressure and velocity. 2.P-0501 1/2 turbine steam flow increased. 3.Manual valve of consumers abnormally open too big due to human error. 4.Exchanger or cooling water line leak or rupture. 5.Human error in opening manual valves at the end of CWS for circulating into CWR.	1.CW system pressure decreased. 2.Inlet pressure to all CW consumers decreased (especially E-3003 1/2/3 and E-5010 which are located the highest location) hence complete cooling is not achieved.	1.FIA-0514 high flow alarm. 2.FIA-0511 high flow alarm. 3.PIA-0514 low pressure alarm. 4.Turbine control system adjust turbine speed.	4	2	2	N	
. 2	High flow(FT-0501 1/2 steam)	1 HPS header pressure increasing.	1.High flow and pressure in CWS. 2.High speed of steam turbine shaft.	1.FIA-0514 high flow alarm. 2.FIA-0511 high flow alarm. 3.PIA-0514 low pressure alarm. 4.Turbine control system adjust turbine speed. 5.Same as high pressure(HPS inside plant) 7001.9.	2	2	1	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 3	low/no flow(CW)	1 1.HPS flow decreased. 2.P-0501 1/2 or P-0502A/B failure. 3.Turbine of P-0501 1/2 failure. 4.Manual valve of consumers abnormally closed due to human error. 5.Exchanger or cooling water line blockage or rupture. 6.Pump strainers blockage. 7.Manual valves on inlet or outlet route closing due to human error. 8.Failure of check valve, remaining in semi-open situation.	1.Plant shutdown. 2.Shortage of CW in consumers, lead to high temperature and finally failure of cooling in CW exchanger.	1.PIA-0514 low pressure alarm at P-0501 1/2, P-0502A/B outlet. 2.FIA-0514 flow indicator. 3.FIA-0511 flow indicator. 4.CW pumps 3 operate 1 spare(two pumps running with steam turbine and one with electrical driven, so in this case only one pump will be in the service up to another electrical driven pump come in the service and the plant maybe face to the shutdown).	4	3	3	N	Develop SOP for proper adjusting CW distribution in case of two pumps running and low plant loading situation.
. 4	low/no flow(FT-0501 1/2 steam)	1 1.HPS header pressure decreasing. 2.Rupture of HPS pipe. 3.Loss of hydraulic oil pressure and close the steam valve.	1.Plant shutdown. 2.Shortage of CW in consumers, lead to high temperature and finally failure of cooling in CW exchanger.	1.PIA-0514 low pressure alarm at P-0501 1/2, P-0502A/B outlet. 2.FIQ-0514 indicator. 3.CW pumps 3 operate 1 spare(two pumps running be able to keep plant operation).	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 5	part of flow/composition(H2SO4)	1 1.P-0512A/B failure. 2.TK-0510 empty. 3.Blockage or rupture of pipe. 4.Concentration of H2SO4 is lower than normal.	1.pH increase. 2.Increasing of exchanger and pipe fouling.	1.LALL-0517 low level alarm. 2.P-0512 A/B 1 operate 1 spare. 3.ML-0512A/B(running status), XA-0512A/B(fault status). 4.AIA-0511 online analyzer(for pH). 5.AIH-0511 high pH alarm and auto-start P-0512A/B. 6.AI-0512 online analyzer(for conductivity) 7.AI-0513 online analyzer(for ORP) 8.AP-0501 sampling point.	4	3	3	N	Add AT-0511 low pH alarm and interlock to auto-stop H2SO4 injection pump.
. 6	part of flow/composition(anti-scal e)	1 1.P-0511A/B failure. 2.TK-0509 empty. 3.Pipe leakage or rupture.	Exchanger and pipe fouling	1.LALL-0516 low level alarm. 2.P-0511 A/B 1 operate 1 spare. 3.ML-0511A/B(running status), XA-0511A/B(fault status). 4.AIA-0515 online analyzer(for anti-scale agent). 5.AIL-5015 low alarm and auto-start P-0511A/B. 5.AP-0501 sampling point.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 7	part of flow/composition(inhibitor )	1 1.P-0510A/B failure. 2.TK-0508 empty. 3.Pipe leakage or rupture.	Exchanger and pipe corrosion.	1.LALL-0515 low level alarm. 2.P-0510 A/B 1 operate 1 spare. 3.ML-0510A/B(running status), XA-0510A/B(fault status). 4.AIA-0514 online analyzer(for corrosion inhibitor). 5.AIL-0514 low alarm and auto-start P-0510A/B. 6.AI-0512 online analyzer(for conductivity) 7.AI-0513 online analyzer(for ORP) 8.AP-0501 sampling point.	4	3	3	N	
. 8	part of flow/composition(NaClO)	1 1.P-0506A/B failure. 2.TK-0503 empty. 3.Pipe leakage or rupture. 4Low concentration of NaClO in TK-0503.	1.Algae formation in CW. 2.Affect CW quality. 3.Increasing CW temperature for decreasing the cooling tower efficiency.	1.LALL-0503 low level alarm. 2.P-0506 A/B 1 operate 1 spare. 3.ML-0506A/B(running status), XA-0506A/B(fault status). 4.AP-0501 sampling point.	4	3	3	N	
. 9	high concentration(H2SO4)	1 1.P-0512A/B adjustment failure cause H2SO4 exceeding. 2.Human error. 3.AT-0511 failure. 4.High concentration of H2SO4 in TK-0510.	1.Corrosion in the equipments and pipe. 2.High consumption of H2SO4.	1.AIA-0511 online analyzer(for pH). 2.AI-0512 online analyzer(for conductivity) 3.AI-0513 online analyzer(for ORP) 4.AP-0501 sampling point.	4	3	3	N	Add AT-0511 low pH alarm and interlock to auto-stop H2SO4 injection pump.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 10	high concentration(NaClO)	1 1.P-0506A/B adjustment failure cause NaClO exceeding. 2.Human error in starting both pump at the same time. 3.High concentration NaClO in TK-0503.	ClO- increase in CW, cause stress corrosion in case of stainless steel exchanger.	1.AP-0501 sampling point. 2.COC of Cl- control to keep to 4. 3.AI-0512 conductivity analyzer. 4.AI-0512 ORP analyzer.	3	3	2	N	TCC to check: relation between ClO- and Cl- concentration and relevant reactions (for NaClO dosing in CW).
. 11	low concentration	1 Same as part of flow/composition(H2SO4),part of flow/composition(anti-scale), part of flow/composition(inhibitor), part of flow/composition(NaClO) 0501.5/6/7/8	Same as part of flow/composition(H2SO4),part of flow/composition(anti-scale), part of flow/composition(inhibitor), part of flow/composition(NaClO) 0501.5/6/7/8	Same as part of flow/composition(H2SO4),part of flow/composition(anti-scale), part of flow/composition(inhibitor), part of flow/composition(NaClO) 0501.5/6/7/8				N	
. 12	high pressure	1 1.Exchanger blockage. 2.Manual valve abnormally closed (partial or total) due to human error(along the circulation route from pump discharge to cooling tower). 3.High pressure of HPS. 4.Low pressure in LPS header.	1.Circulation water pressure increased. 2.P-0501 1/2, P-0502A/B trip. 3.Plant shutdown. 4.Due to high discharge pressure of turbine driver pumps, electrical pumps may not be able to deliver the same pressure and may damage. 5.Rate of water circulation increased (in case of cause 3&4).	1.FIA-0514 high flow alarm(in case of cause 3&4). 2.FIA-0511 high flow alarm(in case of cause 3&4). 3.Turbine control system adjust turbine speed. 4.Same as high pressure(HPS inside plant) 7001.9.	4	3	3	N	Add high alarm to PIA-0514.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	low pressure	1 1.Incorrect pump selection which lead to high flow, pressure and velocity. 2.P-0501 1/2 turbine steam flow or pressure decreased. 3.Manual valve of consumers abnormally open too big due to human error. 4.Exchanger or cooling water line leak or rupture. 5.Human error in opening manual valves at the end of CWS for circulating into CWR. 6.Strainers blockage.	1.Inlet pressure to all CW consumers decreased (especially E-3003 1/2/3 and E-5010 which are located the highest location) hence complete cooling is not achieved. 2.Loss of production capacity due to high temperature in C-3001 inlet and incomplete cooling in 5000 unit exchangers, finally high high temperature and shut down.	1.FIA-0514 high flow alarm. 2.FIA-0511 high flow alarm. 3.PIA-0514 low pressure alarm. 4.Turbine control system adjust turbine speed. 5.TIA-0511 high temperature alarm.	4	2	2	N	1.Add TE-0511 low temperature alarm. 2.Add PT-0511 low pressure alarm.
. 14	vacuum	1 Pump suction strainer blockage.	1.Damage to P-0501 1/2, P-0502A/B. 2.Loss of CW system, overtemperature and shut down.	PIA-0512A/B, PIA-0513A/B low pressure alarm and low low pressure alarm.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 15	high temperature	1 1.Cooling tower failure. 2.High temperature of CWR. 3.High temperature and humidity of ambient. 4.High flow rate of CW.	1.Process temperature increased, high temperature in process units, in extreme case plant shut down. 2.Excessive growth of algae, high consumption rate of NaClO.	1.TIA-0513 high temperature alarm. 2.Possibility of using all of 4 cooling towers to reduce the CWS temperature.	4	3	3	N	
. 16	low temperature	1 non actual hazard and operation identify						N	
. 17	action not execute(CW filter operation)	1 1.PDI-0518A/B failure. 2.Failure of valving system. 3.Human error in closing the valve. 4.P-0504A/B failure.	1.Affect CW quality, suspended solid formation. 2.Blockage of heat exchangers.	PIA-0515 low pressure alarm.	4	3	3	N	1.Lines from each filter to PD-0502 for discharge of CSW shall be sloped down towards PD-0502.
. 18	extra action execute(CW filter operation)	1 1.PDI-0518A/B failure. 2.Failure of valving system.	1.Waste CW and increase R.O. water as make-up. 2.Increasing CSW output from unit towards DMPC.	1.FIQ-0516 flow indicator. 2.LI-0512 level indicator.	2	3	1	N	1.Add flow indicator for FT-0516.
. 19	As well as flow(water quality)	1 1.Low quality make up water. 2.High d/p of filter.	1.Impact the purity of product. 2.More make up water. 3.Block exchanger.	1.AI-0512 conductivity indicator. 2.PDI-0518A/B high d/p alarm.	3	3	2	N	
. 20	low pressure(CW filter)	1 1.P-0504A/B failure.	1.No outlet of filter. 2.High impurity.	1.PT/PIA-0515 low pressure alarm.	3	3	2	N	



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 21	high temperature(CW filter)	1 1.Cooling tower failure. 2.High temperature of CWR. 3.High temperature and humidity of ambient. 4.High flow rate of CW.	1.Process temperature increased, high temperature in process units, in extreme case plant shut down. 2.Excessive growth of algae, high consumption rate of NaClO. 3.Low efficiency of filter.	1.TIA-0513 high temperature alarm. 2.Possibility of using all of 4 cooling towers to reduce the CWS temperature.	4	3	3	N	
. 22	no/low flow(CW filter)	1 same as 501.20						N	
. 23	other	1						N	HAZOP study should be done by vendor for CW filter system package, the owner will check CW filter package after receiving vendor data.

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Establish dt : 2016/8/10 Am12:00:00

Company nam Middle East Kimiaye Pars Company

Plant site :

Project no :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Process name : 2000# AREA

Node description Recycle hydrogen compressor C-2002

Pipe / equipment n C-2002, MC-2002, D-2070, D-2072, D-2071, D-2073, E-2070, D-2074, D-2075.

Drawing no : MKP-VD-9000-306-003-A1~MKP-VD-9000-306-007-A1

Design purpos To provide H2 gas for reduction of catalyst during start-up, operation condition:inlet 7/24 barG, 48 degree C; outlet 15/50.4barG, 48 degree C.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
2007 . 1	High flow	1 FT/FIC/FV-2150 fails open	Decreasing pressure in hydrogen header, increasing hydrogen recycling.	1.PI-2150 low alarm. 2.PT/PIC/PV-2608 adjust pressure.				N	
. 2	low/no flow	1 1.PT/PIC/PV-2481 fail open. 2.USV-2482 abnormally open. 3.PT/PIC/PV-2406 fail open. 4.PSV-2354~2360 abnormally open.	1.Compressing ratio increase, and damage compressor in worst case. 2.Compressor outlet and capacity control valves temperature increase, and damage compressor in worst case.	1.PIA-2700 low pressure alarm at C-2002 inlet. 2.TIA-2701/2703 high temperature alarm and high high temperature alarm at C-2002 outlet. 3.PIAS-2701 open PV-2704 for keeping compression ratio when pressure $\geq$ 52 barG. 4.VIAS-2700/2701 high vibration alarm and high high vibration trip.	3	4	3	N	
. 3	No flow(Lube oil)	1 1.Inlet strainer blocked. 2.Oil filter blocked. 3.Pipe leakage.	Damage crank shaft and bearings.	1.PIAS-2703 $\leq$ 2.7 barG automatic start auxiliary oil pump, and PIAS-2703/2704/2705(2oo3) $\leq$ 2.0 barG shut down. 2.PDIA-2702 high d/p alarm for filter blockage.	3	4	3	N	1.Add the branch suction line for AOP with strainer and valve in each line. 2.Add check valve on pump P-2004B discharge.
. 4	incorrect flow direction	1 non actual hazard identify						N	
. 5	reverse flow	1 Capacity control valves (suction valves) failure.	Temperature increase, and damage piston ring, rider ring and packing ring.	1.TIA-2701/2703 high temperature alarm, and high high temperature alarm. 2.Check valve at C-2002 outlet.	3	4	3	N	TIA-2701/2703 add high high temperature trip.
. 6	part of flow/composition	1 non actual hazard identify						N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 7	as well as flow/impurity	1 non actual hazard identify						N	
. 8	high pressure(process side)	1 1.Manual valve abnormally closed at C-2002 outlet. 2.PT/PIC/PV-2608 fails open.	Overpressure and H2、CO leak cause fire and explosion and toxic release in worst case.	1.PV-2701 open (pressure $\geq$ 52 barG). 2.PISA-2701 high high alarm (pressure $\geq$ 53 barG), and high high trip (pressure $\geq$ 54 barG). 3.PSV-2701 (set @ 55.4 barG). 4.PSV-2604/2605 (set @ 60barG).	5	2	3	Y	
. 9	high pressure(Lube oil)	1 P-2004A/B switch error cause two pumps running simultaneously.	Lube oil system pressure increase and cause pipe leak.	PIAS-2703 pressure $\geq$ 4.5 barG automatic stop auxiliary oil pump.	2	4	2	N	PIAS-2703 add high pressure alarm.
. 10	low pressure(process side)	1 Same as 2007.2 low/no flow(process side).						N	
. 11	low pressure(Lube oil)	1 1.P-2004A/B failure. 2.Filter blockage. 3.PCV-2703 fail closed. 4.Pipe leak.	Damage crank shaft and bearings.	1.PIAS-2703 $\leq$ 2.7 barG automatic start auxiliary oil pump, and PIAS-2703/2704/2705(2003) $\leq$ 2.0 barG shut down. 2.PDIA-2702 high d/p alarm for filter blockage.	3	4	3	N	PIAS-2703 add low pressure alarm.
. 12	high temperature(Process gas outlet)	1 1.Cooling water supply failure. 2.Capacity control valves failure. 3.Feed gas low flow.	1.Compressing ratio increase 2.Temperature increase, and damage piston ring,rider ring and packing ring.	1.TIA-2701/2703 high temperature alarm, and high high temperature alarm at compressor outlet. 2.Process gas inlet low pressure alarm PIA-2700.	3	4	3	N	TIA-2701/2703 add high high temperature trip.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	low temperature(Process gas)	1 non actual hazard identify						N	
. 14	high level(D-2074)	1 1.D-2005 LST/LIC/LV-2474 fail closed. 2.P-2003A/B failure and lead liquid carry to compressor C-2002.	Damage compressor.	LICA-2474 high level alarm.	3	3	2	Y	Add LST-2474A/B/C (medium of three) high high alarm and trip C-2002 by way of DCS during start-up.
. 15	low level(D-2074)	1 LV-2701 abnormally open.	Recycle H2 impact drain system.	LIAS-2700 low level to close LV-2701 and low low level alarm.	3	3	2	N	
. 16	low level(Oil tank/crank shaft tank)	1 1.Crank shaft casing leakage. 2.Piping leakage.	Damage bearings and oil pump.	1.LG-2700 2.PIAS-2703/2704/2705(2oo3) $\leq$ 2.0 barG shut down.	3	3	2	N	1.Add level switch for crank shaft tank with low trip. 2.Forbdden to start compressor when the oil level is low.
. 17	rupture/leak(seal gas system)	1 1.PCV-2700/2701 fail closed. 2.Packing failure.	Loss of N2 and recycle hydrogen release and vent to flare.	1.PT/PI-2706/2707.	2	4	2	N	PT/PI-2706/2707 add low pressure alarm.
. 18	High Vibration	1 Parts loosing.	Damage crank shaft and bearings,and damage compressor in the worst case.	VIAS-2700/2701 high vibration alarm and high high vibration trip.	3	3	2	N	
. 19	other	1 non actual hazard identify						N	

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Establish dt : 2016/8/10 Am12:00:00

Company nam Middle East Kimiaye Pars Company

Plant site :

Project no :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Process name : 2000# AREA

Node description Start-up nitrogen compressor C-2001

Pipe / equipment n C-2001

Drawing no : MKP-11-DE-9000-RE-REQ-308, 0514-JA 16704-PID

Design purpos Pressurizing system for start-up.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
2008 . 1	High flow(Process Side)	1 non actual hazard identify						N	
. 2	low/no flow	1 1.Suction filter blockage. 2.HV-2750 fail closed.	1.Compressor surge and damage. 2.Increasing outlet line and compressor temperature.	1.Anti-surge valve FV-2575 open, and PLC set a delay time to trip. 2.VISA-2750~2753 high vibration alarm and high high vibration set a delay time to trip. 3.PDG-2754 d/p indicator for temporary filter blockage.	3	4	3	N	1.Revise P&ID to show alarm and interlock for temperature,pressure and flow if any. 2.Add alarm high and high high trip for TT-2579.
		2 1.Discharge manual valve abnormally closed. 2.PSV fail open. 3.C-2001 trip due to high temperature and lube oil low pressure, etc.	E-2002 tube side overtemperature and damage.	FST-2582 low flow alarm and low low flow trip to activate IS-1 with POS(process override switch).	3	4	3	Y	
. 3	incorrect flow direction	1 non actual hazard identify						N	
. 4	reverse flow	1 Trip of C-2001.	Back flow.	Check valve on discharge line.	2	4	2	N	Show check valve and manual valve on 2000-PID-018
. 5	part of flow/composition	1 non actual hazard identify						N	
. 6	as well as flow/impurity	1 non actual hazard identify						N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 7	high pressure(process side)	1 Discharge manual valve abnormally closed.	1.Overpressure and N2 release. 2.Compressor inlet chocking.	PSV	2	4	2	N	PI-2579 add high pressure alarm.
. 8	low pressure(process side)	1 Leakage of system.	Reduce nitrogen flow, same as low/no flow (process side) cause 2.	Same as low/no flow (process side) cause 2.				N	
. 9	high pressure(lube oil)	1 MOP and AOP switch error cause two pumps running simultaneously.	Lube oil system pressure increase and cause pipe leak.	1.PCV-2750/2751 2.PSV-2750	2	3	1	N	Lube oil supply main line PT-9672 add high pressure alarm.
. 10	low pressure(lube oil)	1 1.Oil pump failure. 2.Filter blockage. 3.PCV-9671/9672 fail closed. 4.Pipe leak.	Gear and bearings wear out and compressor damage in worst case.	1.PT-9672 low alarm and low low pressure trip. 2.PDS-9671 high d/p alarm for filter blockage.	3	3	2	N	
. 11	high temperature(process side)	1 Same as 2008.2 low/no flow cause 1.						N	
. 12	high temperature(lube oil)	1 Cooling water supply failure.	Damage compressor.	1.TIA-9671 high temperature alarm on the lube oil pipe. 2.TISA-2760~2765,TISA-2766~2769, TISA-2770/2771 high temperature alarm and high high temperature trip.	3	3	2	N	
. 13	low temperature(lube oil)	1 1.External low temperature. 2.Cooling water overflow.	1.Viscosity of lube oil increase and cause shaft to wear out and damage turbine and CW pump. 2.Decrease the performance of lube oil pump and decrease the oil supply. 3.Increase d/p of the filter.	1.Lube oil heater will switch on when external low temperature. 2.PDS-9671 high d/p alarm for filter.	2	4	2	N	Show the autostart of lube oil heater in P&ID.



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 14	rupture/leak(seal gas system)	1 1.PDCV-12270 fail closed on primary sealing line. 2.Filter blockage on primary sealing line. 3.PCV-12270 on secondary sealing line. 4.Filter blockage on secondary sealing line.	Nitrogen and flammable gas release and vent to the atmosphere.	1.PDAL-12272 low d/p alarm and PDALL-12272 low low d/p alarm for primary sealing gas. 2.PDAH-12273 high d/p alarm for primary sealing gas filter. 3.PDAH-12270 high d/p alarm for secondary sealing gas filter. 4.PAH-12271 high pressure alarm and PAHH-12271 high high pressure alarm on vent line.	3	3	2	N	
. 15	low level(oil tank)	1 1.Oil tank leakage. 2.Oil pipe leakage.	Loosing of lube and compressor damage.	1.LS-9671 low level alarm. 2.Forbdden to start compressor when the oil level is low.	3	4	3	N	LS-9671 low level alarm change to low low level trip.
. 16	high vibration	1 Parts loosing.	Damage shaft and bearings,and damage compressor in the worst case.	VISA-2750~2753 high vibration alarm and high high vibration set a delay time to trip.	3	3	2	N	
. 17	other	1 Axial displacement.	Damage bearings.	ZISA-2750/2751 high axial displacment alarm and high high axial displacment trip.	2	4	2	N	

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Establish dt : 2016/8/10 Am12:00:00

Company nam Middle East Kimiaye Pars Company

Plant site :

Project no :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Process name : 2000# AREA

Node description Flue gas blower and turbine F-2001/FT-2001

Pipe / equipment n FT-2001, MP-1001, GB-1001, OT-1002, F-2001, MF-2001, OT-1001, AP-1001, OC-1001A/B, OF-1001A/B.

Drawing no : MKP-VD-2000-351-145-A1, SH-3~5; MKP-VD-2000-351-302-A0

Design purpos Flue gas blower and turbine F-2001/FT-2001 for primary reformer.(inlet steam condition: 43 barG, 345 degree C, 44395 kg/hr ; trubine:4200 rpm , ID Fan: 1560 rpm)

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
2009 . 1	high pressure(Lube oil)	1 1.MP-1001/AP-1001 switch error cause two pumps running simultaneously. 2.Filter blocked. 3.Very low temperature.	Lube oil system pressure increase and cause pipe leak.	1.PT-2822 high pressure alarm and automatic stop auxiliary oil pump AP-1001. 2.PCV-2804 adjust pressure. 3.PSV-2802 on the circulating pipe(set pressure: 10kg/cm2G). 4.PSV-2803 on the outlet of auxiliary oil pump (set pressure: 10kg/cm2G). 5.Two filters, one run one spare.	2	3	1	N	
. 2	high pressure(turbine)	1 HPS from header high pressure.	Damage turbine(casing failure) and steam inlet pipe leak.	1.PT-2804 high pressure alarm and high high pressure trip. 2.PV-7004 open. 3.PSV-7010/7011/7012(set pressure :52 barG).	3	2	1	N	
. 3	low pressure(Lube oil)	1 1.MP-1001/AP-1001 failure. 2.OF-1001A/B blocked or switch operation error. 3.PCV-2804 fail open. 4.Oil pipe leakage.  5.HO-1005 not correctly adjust.	Turbine and ID fan wear out and damage bearings in worst case.	1.PT-2822 low pressure alarm and start-up auxiliary L.O. pump. 2.PT-2822 low low pressure trip. 3.OT-1002 overhead tank. 4.PDI-2811 d/p indicator for filter blockage.	3	3	2	Y	PDI-2811 add high d/p alarm.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 4	low pressure(turbine)	1 HPS from header low pressure.	1.Loss power of turbine and increase pressure of flue gas. 2.Increase consumption of the steam.	1.PT-2804 low pressure alarm and low low pressure to drive the fan by electric motor MF-2001. 2.PASH-2224(2003) high pressure alarm and trip IS-01. 3.PAHH-2224 high pressure trip I-15 open the damper on the top of H-2001.	4	3	3	N	
. 5	high temperature(Lube oil)	1 1.Cooling water failure. 2.Oil heater fail to overheating.	Loss of oil film cause shaft to wear out and damage turbine bearings and ID fan bearings.	1.High temperature alarms and high high temperature trip on bearings. 2.TI-2811 high temperature alarm and high high temperature switch off L.O. heater. 3.TI-2801 overheating protection.	3	3	2	N	
. 6	high temperature(inlet turbine)	1 HPS from header high temperature.	Turbine overtemperature, damage turbine and steam inlet pipe leak.	1.TT-2801 high temperature alarm and high high temperature trip. 2.Desuperheater on the steam header DS-7010A/B.	3	2	1	N	
. 7	high temperature(outlet turbine)	1 No load operation.	High temperature in exhaust of turbine.	TI-2802 high temperature alarm and high high temperature trip.	2	2	1	N	Add desuperheater on the LP steam header.
. 8	low temperature(Lube oil)	1 1.External low temperature. 2.Cooling water overflow.	1.Viscosity of lube oil increase and cause shaft to wear out and damage turbine and ID fan. 2.Decrease the performance of lube oil pump and decrease the oil supply. 3.Increase d/p of the filter.	1.Lube oil heater will switch on when external low temperature. 2.PDI-2811 d/p indicator for filter.	1	4	1	N	1.PDI-2811 add high d/p alarm. 2.Add TI-2801 low temperature alarm.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 9	low level (OT-1001)	1 1.Oil tank leakage. 2.Pipe leakage. 3.Drain abnormally open.	1.No oil to the bearings. 2.Damage oil pump.	1.LI-2813 low level alarm and low low level trip. 2.PT-2822 low pressure alarm and low low pressure trip due to pipe leakage.	3	3	2	N	Add blind flange after the drain valve.
. 10	high speed	1 1.SE-2801A/B, SIC-2167 failure high. 2.HIC-2167 high input due to human error. 3.Actuator/governor valve fail open. 4.Coupling fracture.	Overspeed and damage turbine rotor and ID fan impeller.	1.SE-2802A/B/C(2oo3) high high speed trip SV-2801/2813 and drain control oil, close HPS. 2.Mechanical device ZE-2811 activate spring and drain control oil, close HPS.	4	2	2	Y	
. 11	low speed	1 1.Turbine running is lower than operating speed due to steam header low pressure 2.Governor valve fail closed.	1.Loss power of turbine and increase pressure of flue gas. 2.Increase consumption of the steam. 3.Decrease oil pressure.	1.PT-2804 low pressure alarm and low low pressure to drive the fan by electric motor MF-2001. 2.PASH-2224(2oo3) high pressure alarm and trip IS-01. 3.PAHH-2224 high pressure trip I-15 open the damper on the top of H-2001.	4	3	3	N	
. 12	high vibration	1 1.Turbine rotor unbalanced. 2.Oil film unstable between shaft and bearing. 3.Parts loosing. 4.Misalignment between equipments.	Damage turbine, gear box and ID fan.	VI-2803/2804/2805/2806/2811/2812/2813/2814 high vibration alarms and high high vibration trip.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	other	1 1.Axial displacement. 2.Excess force due to steam with water.	Damage thrust bearings and damage rotor.	1.ZI-2801 high axial displacement alarm and high high axial displacement trip on coupling with turbine and gear box. 2.ZI-2802 high axial displacement alarm and high high axial displacement trip on coupling with gear box and flue gas fan. 3.Desuperheater on the steam header DS-7010A/B. 4.Steam trap and condensate collector.	3	3	2	N	
		2						N	Due to incomplete data of P&ID for MF-2001, it will be checked later. TCC shall be issued completed P&ID like other MV motors of plant and consider auto start and relevant signals for it.

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Establish dt : 2016/8/10 Am12:00:00

Company nam Middle East Kimiaye Pars Company

Plant site :

Project no :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Process name : 2000# AREA

Node description Combustion air blower and turbine F-2002/FT-2002

Pipe / equipment n FT-2002, MP-2001, GB-2002, OT-2002, F-2002, MF-2002, OT-2001, AP-2001, OC-2001A/B, OF-2001A/B.

Drawing no : MKP-VD-2000-351-120-A1, SH-3~5; MKP-VD-2000-351-303-A0

Design purpos Combustion air blower and turbine F-2002/FT-2002 for primary reformer.(inlet steam condition: 43 barG, 345 degree C, 27700 kg/hr ; trubine:5956 rpm , ID Fan: 1560 rpm)

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
2010 . 1	high pressure(Lube oil)	1 1.MP-2001/AP-2001 switch error cause two pumps running simultaneously. 2.Filter blocked. 3.Very low temperature.	Lube oil system pressure increase and cause pipe leak.	1.PT-2872 high pressure alarm and automatic stop auxiliary oil pump AP-2001. 2.PCV-2001 adjust pressure. 3.PSV-2002 on the circulating pipe(set pressure: 10kg/cm2G). 4.PSV-2003 on the outlet of auxiliary oil pump (set pressure: 10kg/cm2G). 5.Two filters, one run one spare.	2	3	1	N	
. 2	high pressure(turbine)	1 HPS from header high pressure.	Damage turbine(casing failure) and steam inlet pipe leak.	1.PT-2854 high pressure alarm and high high pressure trip. 2.PV-7004 open. 3.PSV-7010/7011/7012(set pressure :52 barG).	3	2	1	N	
. 3	low pressure(Lube oil)	1 1.MP-2001/AP-2001 failure. 2.OF-2001A/B blocked or switch operation error. 3.PCV-2001 fail open. 4.Oil pipe leakage.  5.HO-2005 not correctly adjust.	Turbine and ID fan wear out and damage bearings in worst case.	1.PT-2872 low pressure alarm and start-up auxiliary L.O. pump. 2.PT-2872 low low pressure trip. 3.OT-2002 overhead tank. 4.PDI-2861 d/p indicator for filter blockage.	3	3	2	Y	PDI-2861 add high d/p alarm.



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 4	low pressure(turbine)	1 HPS from header low pressure.	1.Loss power of turbine and air deficiency , low temperature afterburning ,flame out ,leakage of flammable gas, the system shut down possible explosion. 2.Decrease reaction conversion in reformer.	1.PT-2854 low pressure alarm and low low pressure to drive the fan by electric motor MF-2002. 2.PSAL-2163(2oo3) low pressure activate IS-01.	4	3	3	N	
. 5	high temperature(Lube oil)	1 1.Cooling water failure. 2.Oil heater fail to overheating.	Loss of oil film cause shaft to wear out and damage turbine bearings and ID fan bearings.	1.High temperature alarms and high high temperature trip on bearings. 2.TI-2861 high temperature alarm and high high temperature switch off L.O. heater. 3.TI-2862 overheating protection.	3	4	3	N	
. 6	high temperature(inlet turbine)	1 HPS from header high temperature.	Turbine overtemperature, damage turbine and steam inlet pipe leak.	1.TT-2851 high temperature alarm and high high temperature trip. 2.Desuperheater on the steam header DS-7010A/B.	3	3	2	N	
. 7	high temperature(outlet turbine)	1 No load operation.	High temperature in exhaust of turbine.	TI-2852 high temperature alarm and high high temperature trip.	2	2	1	N	Add desuperheater on the LP steam header.
. 8	low temperature(Lube oil)	1 1.External low temperature. 2.Cooling water overflow.	1.Viscosity of lube oil increase and cause shaft to wear out and damage turbine and ID fan. 2.Decrease the performance of lube oil pump and decrease the oil supply. 3.Increase d/p of the filter.	1.Lube oil heater will switch on when external low temperature. 2.PDI-2861 d/p indicator for filter.	1	4	1	N	1.PDI-2861 add high d/p alarm. 2.Add TI-2862 low temperature alarm.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 9	low level (OT-2001)	1 1.Oil tank leakage. 2.Pipe leakage. 3.Drain abnormally open.	1.No oil to the bearings. 2.Damage oil pump.	1.LI-2863 low level alarm and low low level trip. 2.PT-2872 low pressure alarm and low low pressure trip due to pipe leakage.	3	3	2	N	Add blind flange after the drain valve.
. 10	high speed	1 1.SE-2851A/B, SIC-2119 failure high. 2.HIC-2119 high input due to human error. 3.Actuator/governor valve fail open. 4.Coupling fracture.	Overspeed and damage turbine rotor and ID fan impeller.	1.SE-2852A/B/C(2oo3) high high speed trip XY-2861 and drain control oil, close HPS. 2.Mechanical device ZE-2861 activate spring and drain control oil, close HPS.	4	2	2	Y	
. 11	low speed	1 1.Turbine running is lower than operating speed due to steam header low pressure 2.Governor valve fail closed.	1.Loss power of turbine and air deficiency , low temperature afterburning ,flame out ,leakage of flammable gas, the system shut down possible explosion. 2.Decrease reaction conversion in reformer.	1.PT-2854 low pressure alarm and low low pressure to drive the fan by electric motor MF-2002. 2.PSAL-2163(2oo3) low pressure activate IS-01.	4	3	3	N	
. 12	high vibration	1 1.Turbine rotor unbalanced. 2.Oil film unstable between shaft and bearing. 3.Parts loosing. 4.Misalignment between equipments.	Damage turbine, gear box and ID fan.	VI-2851/2852/2853/2854/2855/2856/21857/2858 high vibration alarms and high high vibration trip.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	other	1 1.Axial displacement. 2.Excess force due to steam with water.	Damage thrust bearings and damage rotor.	1.ZI-2851 high axial displacement alarm and high high axial displacement trip on coupling with turbine and gear box. 2.ZI-2852 high axial displacement alarm and high high axial displacement trip on coupling with gear box and flue gas fan. 3.Desuperheater on the steam header DS-7010A/B. 4.Steam trap and condensate collector.	3	4	3	N	
		2						N	Due to incomplete data of P&ID for MF-2002, it will be checked later. TCC shall be issued completed P&ID like other MV motors of plant and consider auto start and relevant signals for it.
. 14	High flow(air)	1 1.FT/FIC/FV-2111 fail open. 2.HIC/SIC-2119 set failure high by human error. 3.F-2002 loading too high during start up case and low operating load of plant.	Flame out and combust gas full of the chamber could cause explosion.	1.AIA-2223 2 combustibles high alarm. 2.AIA-2223 1 O2 high alarm. 3.TIC-2221 B temperature indicator. 4.SI-2852 speed high alarm.	4	2	2	N	Add PICA-2163 high pressure alarm.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 15	High flow(fuel gas)	1 1.FT/FIC/FV-2531 1/2 fail open. 2.FT/FIC/FV-2536 A fail open. 3.FT/FIC/FV-3169 fail open. 4.PT/PIC/PV-1011 fail open.	Flame out and combust gas full of the chamber could cause explosion.	1.AIA-2223 2 combustibles high alarm. 2.AIA-2223 1 O2 high alarm. 3.TIC-2221 B temperature indicator.	4	2	2	N	

# HAZOP analyzing record

2017/3/3

Project name : MKP Methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Methanol synthesis

Node description Synthesis Gas Compressing

Drawing no : 3000-PID-001

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n C-3001/C-3002, FT-3003 1/2

Design purpos Synthesis Gas Compressing,24.0~80.0 barG.48~74 degree C.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
3001 . 1	High flow(Synthesis gas)	1 Refer to node 2005,2006.	1.C-3001/3002 outlet pressure decrease. 2.R-3001 1/2/3 low reaction and cause production decreasing, inert gas increasing. 3.C-3001/3002 overspeed and mechanical failure. 4.Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor.	1.C-3001/3002 overspeed trip. 2.FIA-2476 high flow alarm.	4	3	3	Y	1.C-3001/3002 overspeed trip, SIF should be meet SIL 1. 2.Ask from compressor vendor for the proper safeguard about liquid droplet in compressor.  GE has confirmed item 1. Item 2 has already been analyzed in the Node 3006.
. 2	High flow(Recycle gas)	1 1.Upstream synthesis gas high flow. 2.FT/FIC/FV-3169 fail closed. 3.High speed on synthesis turbine. 4.Overspeed of turbine. 5.Failure of damper(controlling flow of recycle gas).	1.C-3001/3002 circulator inlet pressure decrease, outlet pressure decrease.(Check by GE) 2.R-3001 1/2/3 low reaction and cause production increasing slightly, inert gas increasing. 3.C-3001/3002 overspeed and mechanical failure. 4.Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor. 5.Higher pressure drop across the catalyst bed led to damage to catalyst support.	1.C-3001/3002 overspeed trip. 2.FIA-2476 high flow alarm. 3.FIA-3167 high flow alarm. 4.PDIA-3112/3115/3117 high d/p alarm.	4	4	4	N	1.Ask from compressor vendor for the proper safeguard about liquid droplet in compressor. 2.C-3001/3002 circulator inlet pressure decrease, outlet pressure decrease(for recycle gas high flow).(Check by GE)  Item 1/2 has already been analyzed in the Node 3006.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 3	low/no flow(Synthesis gas)	1 1.Manual valve abnormally closed due to operator error in inlet of C-3001/3002. 2.C-3001 synthesis gas inlet SDV valve abnormally closed. 3.Low/no flow of upstream. 4.Human error to open HV-3011. 5.Failure compressor or turbine.	C-3001/3002 surge and mechanical damage.	1.FIC-500 anti-surge control to open FCV-500.(Refer to GE P&IDs) 2.High vibration trip.	4	3	3	Y	1.High vibration trip, SIF should be meet SIL 1. (Check with GE) 2.Ask from compressor vendor for the proper safeguard about liquid droplet in compressor. 3.Ask and confirm from GE about SIL level.  GE has confirmed item 1 for radial vibration. Item 2 have already been analyzed in Node 3006. Item 3 will be confirmed by way of SIL verification.
. 4	low/no flow(Recycle gas)	1 1.Upstream synthesis gas low flow. 2.FT/FIC/FV-3169 fail open. 3.C-3002 recycle gas inlet SDV valve abnormally closed. 4.PT/PIC/PV-3166 fail open. 5.Failure of compressor or turbine or damper.	C-3001/3002 surge and mechanical damage.	1.FIC-503 anti-surge control to open FCV-503.(Refer to GE P&IDs) 2.FI-3167 flow indicator.	4	3	3	N	High vibration trip, SIF should be meet SIL 1. (Check with GE)  GE has confirmed item 1 for radial vibration.
. 5	incorrect flow direction	1 Operator mistake in opening HV-3011 or its bypass.	1.Same as low/no flow(synthesis gas) 3001.3 2.Environmental pollution.	1.FIC-500 anti-surge control to open FCV-500.(Refer to GE P&IDs) 2.High vibration trip. 3.PICA-3007 low pressure alarm.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 6	reverse flow	1 Surge in compressor.	Damage of compressor.	Anti-surge control.	4	4	4	N	
. 7	part of flow/composition	1 Same as upstream part of flow/composition.	Changing the molecular weight of synthesis gas and more consumption energy.	AI-3001/3002/3003 CO/CO2/H2 analyzer.	3	4	3	N	
. 8	as well as flow/impurity	1 Refer to 1000/2000 area.						N	
. 9	high concentration(synthesis gas)	1 High concentration(synthesis gas) in upstream.	Changing the molecular weight of synthesis gas and more consumption energy.	AI-3001/3002/3003 CO/CO2/H2 analyzer.	3	4	3	N	Check by GE for effect of (cause, consequence, safeguard) changing the molecular weight of synthesis gas.  This item has already been analyzed in Node 3006.
. 10	low concentration(synthesis gas)	1 Upstream R-2004 abnormal conversion.	Affect methanol reaction.	AI-3001/3002/3003 CO/CO2/H2 analyzer.				N	Check by GE for effect of (cause, consequence, safeguard) changing the molecular weight of synthesis gas.  This item has been already analyzed in Node 3006.
. 11	high pressure	1 1.C-3001/3002 discharge SDV abnormally closed. 2.High pressure in upstream.	Overpressure and flammable release.	1.PSV-502.(Refer to GE P&IDs) 2.High vibration trip. 3.High temperature trip. 4.Anti-surge control.	4	3	3	Y	



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 12	low pressure	1 1.HV-3011 fail open. 2.PV-3166 fail open. 3.FV-3169 fail open. 4.Low pressure in upstream.	Same as low/no flow(Synthesis gas) 3001.3.	Same as low/no flow(Synthesis gas) 3001.3.				N	
. 13	vacuum	1 Not possible.						N	
. 14	high temperature	1 1.Upstream RFG high temperature. 2.C-3001/2 intercooler CW failure. 3.High temperature of D-3001 outlet recycle gas. 4.High pressure in downstream synthesis gas compressor. 5.Low pressure in upstream synthesis gas compressor.	C-3001/3002 overtemperature and mechanical damage.	1.TIA-2476 high temperature alarm. 2.TIA-3164 high temperature alarm. 3.TIA-3113/3116/3118 high temperature alarm. 4.C-3001/3002 package high temperature alarm and trip.	4	3	3	Y	C-3001/3002 package high temperature alarm and trip, SIF should be meet SIL 1. (Check with GE)  This item has been already analyzed in Node 3006.
. 15	low temperature	1 1.Low temperature of upstream. 2.High pressure of compressor suction.	No safety and operation hazard concern.					N	
. 16	rupture/leak	1 Flange/gasket or pipe fitting leak.	1.Fire and explosion. 2.CO toxic release.	1.Fire and gas detection system. 2.Fire fighting system.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Seve rity	Likeli hoo	Risk	LO PA	Recommendation
. 17	other	1 Refer to compressor C-3001/3002 package node.						N	

# HAZOP analyzing record

2017/3/3

Project name : MKP Methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Methanol synthesis

Node description Synthesis compressor package

Drawing no : SOK0887013, SH2~7; SOK0880159, SH5~14.

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n D-3011, E-3012, C-3001, E-3014, D-3012, C-3002-1, C-3002-2, E-3013, TK-3002, P-3013A/B, PM-3013A/B, E-3018A/B, X-3002A/B, D-3013, P-3012, PM-3012, D-3014, TK-3001, FT-3001, P-3014, PM-3014, E-3011, D-3015, E-3020, P-3011A/B, PM-3011A/B, J-3004, J-3005A/B, J-3006A/B, X-3004A/B, P-3015, E-3021A/B/C, X-3005A/B, E-3016, E-3022A/B/C.

Design purpos Synthesis Gas Compressing, operating conditions:24.0~80.0 barG, 48~122 degree C.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
3006 . 1	High flow (syngas suction)	1 Upstream high flow.	1.C-3001/3002 outlet pressure decrease. 2.R-3001 1/2/3 low reaction and cause production decreasing, inert gas increasing. 3.Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor, and damage compressor in worst case. 4.High pressure at the inlet of the compressor.	1.Same as high pressure. 2.FIA-2476 high flow alarm. 3.D-3011 syngas inlet separator, LCV-3700 will open when level high, LSH-3700 level high alarm and LSHH-3700 level high high trip. 4.D-2005 is installed upstream for liquid separation, with LICA-2474 high level alarm and LSAH-2474 high high level trip.	4	3	3	Y	1.TCC and GE to review the IS-40 partial trip category (high level of liquid separator, high flow) of compressor 2.LT-3700A/B/C(2oo3) level high high trip, SIF should meet SIL 1.
. 2	High flow(recycle gas)	1 1.Upstream synthesis gas high flow. 2.FT/FIC/FV-3169 fail closed. 3.High speed on synthesis turbine. 4.HIC/FCV-3725 failure open due to operator error.	1.Higher pressure drop across the catalyst bed led to damage to catalyst support. 2.Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor, and damage compressor in worst case.	1.FIA-2476 high flow alarm. 2.FIA-3167 high flow alarm. 3.PDIA-3112/3115/3117 high d/p alarm. 4.LICA-3161 high level alarm. 5.LSAH-3161(2oo3) activate IS-03 to trip 3000 area.	4	3	3	N	
. 3	low/no flow(syngas suction)	1 1.Upstream low flow. 2.PV-2481/USV-2482 fail open. 3.USV-3011 abnormally closed. 4.Handvalve at the syngas suction abnormally closed	1.C-3001 surge and damage. 2.No production 3.C-3002-1 syngas 2nd stage compressor surge and damage.	1.FIC/FCV-3702 anti-surge control valve open. 2.PAL-3702 low pressure alarm. 3.XT-3555X/Y, XT-3556X/Y, XT-3520X/Y, XT-3521X/Y, XT-3557X/Y, XT-3558X/Y high vibration alarm and high high trip. 4.Handvalve at the syngas suction lock open. 5.FIC/FCV-3712 anti-surge control valve open.	4	3	3	Y	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 4	low/no flow(recycle gas)	1 1.Upstream synthesis gas low flow. 2.FT/FIC/FV-3169 fail open. 3.Low speed on synthesis turbine. 4.HIC/FCV-3725 failure closed due to operator error. 5.Handvalve at the recycle gas suction or discharge line is abnormally closed.	1.C-3002-2 surge and damage. 2.No/low production	1.FIC/FCV-3722 anti-surge control valve open. 2.PAL-3722 low pressure alarm. 3.XT-3555X/Y, XT-3556X/Y, XT-3520X/Y, XT-3521X/Y, XT-3557X/Y, XT-3558X/Y high vibration alarm and high high trip.	4	3	3	N	Handvalves at the recycle gas suction and discharge lines should be locked open.
. 5	incorrect flow direction	1 1.USV-3750 or 3751 fail open.	1.Low production. 2.High d/p between syngas and recycle gas discharge.	1.UZAH-3750/3751 open alarm 2.Balancing line UV-3714 open in case of high d/p between syngas and recycle gas discharge.	3	3	2	N	
. 6	reverse flow	1 1.Compressor sudden shut-off	1.Compressor counter rotation. 2.Compressor suction high pressure.	1.Anti-surge valves open. 2.Check valve at compressor suction. 3.Compressor suction design pressure high enough to bear shut-off pressure.	2	3	1	N	
. 7	part of flow/composition	1 1.Change composition from upstream.	1.Changing the molecular weight of synthesis gas and more consumption energy. 2.High pressure at discharge	1.AI-3001/3002/3003 CO/CO2/H2 analyzer. 2.Anti-surge control valves open.	3	4	3	N	
. 8	as well as flow/impurity	1 1.Change composition from upstream.	1.Changing the molecular weight of synthesis gas and more consumption energy. 2.Increase pressure of purge gas to fuel gas system. 3.Loss of production.	AI-3001/3002/3003 CO/CO2/H2 analyzer.	2	4	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 9	high pressure(1st stage suction)	1 1.Upstream high pressure. 2.High flow 3.Discharge of C-3002-1 abnormally closed (interstage check valve blocked close isn't considered).	1.High pressure at discharge of C-3001. 2. C-3001 overpressure.	1.PT/PIC/PV-2481 vent to flare. 2.USV-2482 vent to flare. 3.PT-3740A/B/C(2oo3) high pressure alarm and high high pressure trip.	3	3	2	Y	
. 10	high pressure(1st stage discharge)	1 1.Same as high pressure(first stage suction). 2.High speed.	1.Same as high pressure(first stage suction). 2.Compressor, equipment and piping damage.	1.PT/PIC/PV-2481 vent to flare. 2.USV-2482 vent to flare. 3.PT-3740A/B/C(2oo3) high pressure alarm and high high pressure trip. 4.Overspeed trip. 5.PSV-3720A/B.	3	3	2	N	
. 11	high pressure(2nd stage discharge)	1 1.USV-3012 abnormally closed. 2.C-3002-1 outlet manual valve abnormally closed.	1.C-3002-1 overpressure,compressor, equipment and piping damage.	1.PT-3719A/B/C(2oo3) high pressure alarm and high high pressure trip. 2.PSV-3720A/B.	4	3	3	Y	1.Handvalve at the discharge of 2nd stage compressor(C-3002-1) should be lock open.
. 12	high pressure(recycle gas compressor)	1 1.USV-3014 abnormally closed. 2.C-3002-2 outlet manual valve abnormally closed. 3.High pressure upstream.	C-3002-2 overpressure, 2nd compressor,equipment and piping damage.	1.PT-3747A/B/C(2oo3) high pressure alarm and high high pressure trip. 2.PT/PIC/PV-3166 vent to flare.	4	4	4	Y	Add a PSV at the discharge of C-3002-2 or use PSHH-3747 high high pressure trip with SIL2.Those two solutions shall be discussed among GE, Owner and TCC.
. 13	low pressure(1st stage suction)	1 1.Low flow from upstream. 2.Malfunctioning of compressor speed control.	1.C-3001 surge and damage. 2.Effect reaction operation.	1.PAL-3702 low alarm. 2.Anti-surge valve FCV-3702.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 14	low pressure(1st stage discharge)	1 1.Malfunctioning of compressor speed control. 2.Anti-surge valve FCV-3702 fail open. 3.Tube rupture of E 3014.	1.C-3002-1 surge and damage. 2.Effect reaction operation. 3.Gas leaks into CW side of E 3014, causing shell side high pressure.	1.PI-3740A/B/C indicator. 2.Anti-surge valve FCV-3712. 3.PAL-3712 low alarm. 4.PSE-3744 protects shell of E 3014.	4	3	3	N	Add high level alarm at pot of sub flare header of compressor house area 3000 and show this pot on P&ID no. 8500-PID-002.
. 15	low pressure(2nd stage discharge)	1 1.Malfunctioning of compressor speed control. 2.Anti-surge valve FCV-3712 fail open.	1.Effect reaction operation.	1.PI-3719A/B/C indicator.	2	3	1	N	
. 16	low pressure(recycle gas compressor suction)	1 1.Malfunctioning of compressor speed control. 2.Tube rupture of E 3013. 3.Same as low flow of recycle gas.	1.Low production. 2.Gas leaks into CW side of E 3013, causing shell side high pressure. 3. Same as low flow.	1.PAL-3722 low pressure alarm. 2.PSE-3749 protects shell of E 3013. 3. Same as low flow.	4	3	3	N	
. 17	low pressure(recycle gas compressor discharge)	1 1.Malfunctioning of compressor speed control. 2.Anti-surge valve FCV-3722 fail open. 3.USV-3750 fail open.	1.Low production.	1.PI-3747(2oo3) indicator. 2.PI-3729 indicator. 3.UZAH-3750 alarms fail open of USV-3750.	2	3	1	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 18	high temperature(1st stage suction)	1 1.Upstream high temperature. 2.Cooling water failure during surging.	Mechanical damage to compressor and piping.	1.TTA-2476 high temperature alarm. 2. TI-3701 indicator. 3. TIA-3709A/B/C(2oo3) high temperature alarm and high high temperature trip at 1st stage outlet. 4.TI-3740 indicator. 5. TI-3741 indicator.	4	3	3	N	
. 19	high temperature(2nd stage suction)	1 1.Cooling water failure of E 3014.	1.Mechanical damage to compressor and piping.	1.TI-3743/3744 indicators. 2.TI-3712 indicator. 3.TT-3719A/B/C(2oo3) high temperature alarm and high high temperature trip at 2nd stage outlet.	4	3	3	N	Add high temperature alarm on TT-3744.
. 20	high temperature(2nd stage discharge)	1 same as high temperature( 2nd stage suction).	same as high temperature( 2nd stage suction).	same as high temperature( 2nd stage suction).	4	3	3	N	
. 21	high temperature(recycle gas)	1 1.Upstream high temperature. 2.Cooling water failure during surging.	1.Mechanical damage to compressor and piping.	1.TT-3729A/B/C(2oo3) high temperature alarm and high high temperature trip at recycle gas compressor outlet. 2.TI-3722 indicator.	4	3	3	N	Add high temp. alarm for TI-3722.
. 22	low temperature(process gas)	1 1.Low temperature upstream.	no safety concern					N	
. 23	high level(D-3011)	1 1.Upstream high flow. 2.LCV-3700 fail close. 3.Low temperature.	Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor, and damage compressor in worst case.	1.LAH-3700 level high alarm and LSHH-3700 level high high trip. 2.LZAL-3700 alarms fail open of LCV-3700.	4	3	3	N	



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 24	low level(D-3011)	1 LT/LIC/LCV-3700 abnormally open.	24 barG syngas impact drain header.	1.LT-3700A/B/C(2oo3) low level alarm and low low level trip. 2.Closed drain drum has a breathing valve with flame arrester.	4	3	3	N	1.to check the capacity of the breathing valve according to the max. gas blow.
. 25	high level(D-3012)	1 1.Upstream high flow. 2.LCV-3701 fail close. 3.Low temperature.	Incomplete separation of liquid droplet of synthesis gas cause problems in suction of compressor, and damage compressor in worst case.	1.LAH-3701 level high alarm and LSHH-3701 level high high trip. 2.LZAL-3701 alarms fail open of LCV-3701.	4	3	3	N	
. 26	low level(D-3012)	1 LT/LIC/LCV-3701 abnormally open.	High pressure syngas impact drain header.	LT-3701A/B/C(2oo3) low level alarm and low low level trip.	4	3	3	N	1.to check the capacity of the breathing valve according to the max. gas blow.
. 27	high pressure(Lube oil pump discharge side)	1 1.P-3013A/B switch error cause two pumps running simultaneously. 2.X-3002A/B clogging. 3.Manual valve of the L.O. pump discharge abnormally closed.	1.Damage the L.O. pumps and piping.	1.PCV-3505 will regulate the pressure in case of two pump running at the same time. 2. PSV-3503, 3504 on pump discharge. 3.PDT-3508 high d/p alarm.	3	3	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 28	high pressure(Lube oil header)	1 1.PCV-3510 failure open.	1.Excessive lube oil to bearings, and potentially vibration.	1.PAH-3520A/B/C high pressure alarm. 2.XT-3555X/Y , XT-3556X/Y high vibration alarms and high high vibration trip on C-3001 shaft. 3.XT-3520X/Y , XT-3521X/Y high vibration alarms and high high vibration trip on FT-3001 shaft. 4.XT-3557X/Y , XT-3558X/Y high vibration alarms and high high vibration trip on C-3002 shaft.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 29	low pressure(Lube oil)	1 1.P-3013A/B, PM-3013A/B failure. 2.X-3002A/B clogging or switch operation error. 3.PCV-3510 fail closed. 4.Oil pipe leakage. 5.Tube rupture of E-3018A/B.	1.Damage the bearings. 2.Compressor vibration.	1.PT-3506 low pressure alarm and start-up standby L.O. pump. 2.PT-3520A/B/C(2oo3) low pressure alarm, and start standby L.O. pump, low low pressure trip. 3.TK-3001 run down tank for the first part of run down, and emergency pump P-3012 for the last part of run down, and emergency cool down. 4.PDSH-3508 high d/p alarm for failter blockage. 5.XT-3555X/Y , XT-3556X/Y high vibration alarms and high high vibration trip on C-3001 shaft. 6.XT-3520X/Y , XT-3521X/Y high vibration alarms and high high vibration trip on FT-3001 shaft. 7.XT-3557X/Y , XT-3558X/Y high vibration alarms and high high vibration trip on C-3002 shaft.	3	2	1	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 30	high temperature(Lube oil)	1 1.Cooling water failure. 2.E-3015 failure. 3.TCV-3506 fully open.	1.Low oil viscosity causing potentially vibration. 2.Bearing damage.	1.TSH-3502 high temperature L.O. heater switch off. 2.TSHH-3503 overheating protection. 3.TSH-3506 high temperature alarm. 4.High temperature alarm for bearings of compressor and turbine. 5. XT-3555X/Y , XT-3556X/Y high vibration alarms and high high vibration trip on C-3001 shaft. 6.XT-3520X/Y , XT-3521X/Y high vibration alarms and high high vibration trip on FT-3001 shaft. 7.XT-3557X/Y , XT-3558X/Y high vibration alarms and high high vibration trip on C-3002 shaft.	3	3	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 31	low temperature(Lube oil)	1 External low temperature.	1.Viscosity of lube oil increase and cause shaft to wear out and damage compressor. 2.Damage L.O. pump P-3013A/B.	1.E-3015 electric heater and TSL-3502 low tempertaure L.O. heater switch on. 2.TSLL-3502 low low temperature inhibit to L.O. pumps start-up. 3.TAL-3506 low temperature alarm unit start inhibit. 4.XT-3555X/Y , XT-3556X/Y high vibration alarms and high high vibration trip on C-3001 shaft. 5.XT-3520X/Y , XT-3521X/Y high vibration alarms and high high vibration trip on FT-3001 shaft. 6.XT-3557X/Y , XT-3558X/Y high vibration alarms and high high vibration trip on C-3002 shaft.	3	3	2	N	
. 32	low level(oil tank TK-3002)	1 1.Drain valve abnormally open. 2. Oil piping leak. 3. No fill of the oil tank.	1.Damage of the E-3015 due to overtemperature. 2. P-3013A/B cavitation and damage. 3. Bearing damage.	1.TSHH-3503 heater cut off. 2. LSL-3501 low level alarm, heater switch off and inhibit lube oil pump start.	4	3	3	N	GE provide the information about the oil quantity between the main pumps suction loss level and emergency pump suction loss level.
. 33	low level(oil tank TK-3001)	1 1.Tank leak. 2.No fill to the tank.	1.No oil for machine run down, and damage the bearing.	1. LSL-3520 low level alarm, inhibit compressor start. 2.Emergency pump P-3012 for run down.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 34	high speed	1 1.PT-3701(load controller demand) 、SE-3525A/B/C 、SY-3536 servovalve 、SCV-3536 fail open. 2.PT-3701(load controller demand) 、PT-3594A/B/C (HP extration pressure) 、SE-3525A/B/C 、SY-3539 servovalve 、FCV-3539 fail open. 3.PT-3701(load controller demand) 、PT-3597A/B/C (LP extration pressure) 、SE-3525A/B/C 、SY-3537/3538 servovalve 、FCV-3537/3538 fail open. 4.Coupling fracture.	Overspeed and damage compressor.	1.SE-3526A/B/C(2oo3) high high speed trip to solenoid valve XY-3532A/3532B, and XV-3534/3535 steam trubine inlet, 2.XY-3595 close command to HP steam extration line check valve, XY-3598 close command to LP steam extration line check valve.	4	3	3	Y	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 35	high pressure(turbine inlet)	1 Upstream D-2001 high pressure.	1.Damage turbine. 2.Overspeed.	1.PSV-2376,2377,2378,2380. 2.PIA-2372 high pressure alarm. 3.PT-3590A/B/C(2oo3) high pressure alarm and high high pressure trip. 4.SE-3525A/B/C,3526A/B/C speed control. 5.SE-3526A/B/C(2oo3) high high speed trip to solenoid valve XY-3532A/3532B, and XV-3534/3535 steam turbine inlet, XY-3595 and close HP steam extraction line, XY-3598 and close LP steam extraction line.	4	2	2	N	
. 36	high pressure(turbine extraction)	1 1.FCV-3539 fail close. 2.FCV-3538/3537 fail close. 3.PT-3592 or PT-3593 control failure.	1.High pressure to damage the piping and turbine.	1.PAH-3594 high pressure alarm,PSHH-3594 high high pressure trip on HP steam turbine extraction. 2.PAH-3597 high pressure alarm,PSHH-3597 high high pressure trip on LP steam turbine extraction. 3.PSV-3594A/B/C on HP steam turbine extraction. 4.PSV-3597A/B/C on LP steam turbine extraction. 5.PIAC-7004 high pressure alarm.	4	2	2	N	
. 37	low pressure(turbine inlet)	1 1.Upstream low pressure.	1.Low production. 2.Upset on extraction steam headers.	1.PICA-2363 low pressure alarm, PV-2363 open. 2.PIA-2372 low pressure alarm. 3.PI-3590 indicator.	2	3	1	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 38	low pressure(turbine extraction)	1 1.PT-3592 or PT-3593 control failure. 2.Low pressure downstream header.	1.Damage the turbine blade due to high D/P.	1.PSL-3596 low pressure alarm, PSL-3596 low low pressure trip or inhibit to start. 2.1.PSL-3599 low pressure alarm, PSL-3599 low low pressure trip or inhibit to start.	3	3	2	N	
. 39	high pressure(E-3011)	1 1.Cooling water high temperature or failure. 2.Loss of vacuum unit.	1.Affect the efficiency and operation of turbine. 2.Overpressure to damage E-3011.	1.PT-3547A/B/C(2oo3) high pressure alarm and high high pressure trip. 2.PSV-3547. 3.TIA-0513 high temperature alarm in the cooling water supply. 4.FIA-0514 low flow alarm in the cooling water supply.	3	3	2	N	
. 40	high pressure(E-3020)	1 1.J-3006A/B malfunction due to no/low steam. 2.Discharge of J-3005A/B manual valve abnormally close.	1.Lose condensate. 2.Turbine efficiency decrease.	1.J3006A/B redundant 2.PSV-3587, PSV-3586	2	3	1	N	
. 41	high temperature(turbine inlet)	1 Upstream D-2001 high temperature.	1.Turbine damage due to overtemperature.	1.TT-3590A/B/C(2oo3) high temperature alarm and high high temperature trip. 2.TIA-2355/2356 high temperature alarm.	3	3	2	N	
. 42	high temperature(E-3011)	1 1.Cooling water high temperature or failure. 2.Loss of vacuum inside E-3011.	1.Affect the efficiency and operation of turbine. 2.Overpressure to damage E-3011.	1.PT-3547A/B/C(2oo3) high pressure alarm and high high pressure trip. 2.PSV-3547. 3.TIA-0513 high temperature alarm in the cooling water supply. 4.FIA-0514 low flow alarm in the cooling water supply.	3	3	2	N	



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 43	low temperature(turbine inlet)	1 1.Upstream low temperature.	1.Damage the turbine blade.	1.PIA-2372 low pressure alarm. 2.TICA-2360 low temperature alarm. 3.TAL-3590 low temperature alarm. 4.Steam quality protection USLL-3590 turbine trip/inhibit to start. 5.Proper warm-up line for startup.	3	3	2	N	
. 44	high level(E-3011)	1 1.P-3011A/B failure. 2.Steam condenser E-3011 tube rupture. 3.LCV-3540B failure open.	1.Condenser efficiency decrease. 2.High pressure of E-3011. 3.High impurity of condensate.	1.LT-3540A/B/C(2oo3) high level alarm and start stand-by condensate pump. 2.PT-3547A/B/C high pressure alarm, and high high trip. 3.Polishing unit.	3	3	2	N	
. 45	low level(E-3011)	1 1.Pipe leakage. 2.E-3011 shell leakage. 3.LCV-3540A fail open.	P-3011A/B cavitation and damage.	LT-3540A/B/C(2oo3) low level alarm and stop standby P-3011, low low level trip P-3011A/B.	2	3	1	N	
. 46	high pressure(turbine seal steam)	1 1.L.P.steam header high pressure. 2.PT/PIC/PCV-3549 fail open.	1.Increase the seal steam consumption. 2. Damage the sealing.	1.PSV-3550. 2.PSV-7057,7058,7059,7060,7061 at L.P.steam header.	2	2	1	N	
. 47	low pressure(turbine seal steam)	1 1.PT/PIC/PCV-3549 control loop failure. 2.L.P. steam header low pressure.	1.Loss of sealing and vacuum. 2. Thermal stress on the turbine rear end.	1.PAL-3548 low pressure alarm. 2.PCV-3548 fail open. 3.PICA-7056 low pressure alarm. 4.FO-3549 manual bypss 5. Vacuum Trip PT-3547A/B/C.	3	3	2	N	Operation Procedure should be placed that stop the steam turbine and remove the vacuum from the condenser in case of loss of LP steam. (To be mentioned in GE operation manual of the compressor package, and incorporated in the plant operation manual.)

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 48	high temperature(turbine seal steam)	1 non actual hazard identify						N	
. 49	low temperature(turbine seal steam)	1 1.L.P. steam header low temperature.	1.Condensate formed in the turbine steam and potentially damage the sealing and shaft.	1.TAL-3548 low temperature alarm. 2.TAL-7052/7053 low temperature alarm. 3.Steam quality UAL-3548 low alarm. 4.Drainage at the steam sealing LCV-3542. 5. Condensate from LP steam header is drained into the condensate recovery system.	3	3	2	N	
. 50	low flow(C-3001 seal gas)	1 1.FIC-3631A/B/F Y-3631/FCV-3631 control loop failure. 2.Filter X-3004A/B clogging. 3.Booster P-3015 failure during start-up and SOP.	1. Damage of dry gas seal. 2. Process gas leak into the atmosphere, cause fire and toxic release in worst case.	1.PDSH-3682 high d/p alarm for X-3004A/B clogging. 2.PDSL-3683 inhibit to compressor(s) pressurization. 3.FAL-3631A/B low flow alarm. 4.H2 and CO gas detector in the field. 5. PSHH-3660A/B/C and 3661A/B/C high high pressure trip with vent of the compressors. 6. FCV-3631 is fail-open type. 7.Redundant control loop of FIC-3631A/B.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 51	low pressure(C-3001 N2 isolation gas)	1 1.N2 supply failure. 2.X-3003A/B clogging. 3.PCV-3653 failure. 4.Manual valve in the N2 inlet abnormally closed.	1. Oil containment to the dry gas seal, potentially dry gas seal to the bearings. 2. Process gas leak into the atmosphere, cause fire and toxic release in worst case.	1.PDSH-3652 high d/p alarm for X-3003A/B clogging. 2.PT-3660A/B/C(2oo3) low low pressure trip with vent. 3.PT-3661A/B/C(2oo3) low low pressure trip with vent. 4.PT-3655A/B/C low pressure alarm and inhibit the lube oil pump to start, low low pressure trip for oil containment. 5.H2 and CO gas detector in the field.	4	2	2	N	
. 52	low flow(C-3002 seal gas)	1 1.FIC-3636A/B/F Y-3636/FCV-3636 control loop failure. 2.Filter X-3005A/B clogging. 3.Booster P-3016 failure during start-up and SOP.	1. Damage of dry gas seal. 2. Process gas leak into the atmosphere, cause fire and toxic release in worst case.	1.PDSH-3692 high d/p alarm for X-3005A/B clogging. 2.PDSL-3693 inhibit to compressor(s) pressurization. 3.FAL-3636A/B low flow alarm. 4.H2 and CO gas detector in the field. 5. PSHH-3660A/B/C and 3661A/B/C high high pressure trip with vent of the compressors. 6. FCV-3636 is fail-open type. 7.Redundant control loop of FIC-3636A/B.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 53	low pressure(C-3002 N2 isolation gas)	1 1.N2 supply failure. 2.X-3003A/B clogging. 3.PCV-3653 failure. 4.Manual valve in the N2 inlet abnormally closed.	1.Oil contamination to the dry gas seal, potentially dry gas seal to the bearings. 2. Process gas leak into the atmosphere, cause fire and toxic release in worst case.	1.PDSH-3652 high d/p alarm for X-3003A/B clogging. 2.PT-3676A/B/C(2oo3) low low pressure trip with vent. 3.PT-3677A/B/C(2oo3) low low pressure trip with vent. 4.PT-3655A/B/C low pressure alarm and inhibit the lube oil pump to start, low low pressure trip for oil containment. 5.H2 and CO gas detector in the field.	4	2	2	N	
. 54	high pressure in the N2 line	1 1.Failure of primary dry gas seal.	1.Overpressure of N2 line, potentially contamination of N2 source.	1.PSV-3659 2.Check valves downstream FO-3654A/B.	3	3	2	N	
. 55	low temperature of seal gas(C-3001)	1 1.Condensation of seal gas due to the low temperature below the dew point during the SOP condition.	1.Potentially damage dry gas seal.	1.E-3021A/B/C, two operation and one stand by.	3	2	1	N	
. 56	low temperature of seal gas(C-3002)	1 1.Condensation of seal gas due to the low temperature below the dew point during the SOP condition.	1.Potentially damage dry gas seal.	1.E-3022A/B/C, two operation and one stand by.	3	2	1	N	
. 57	high vibration	1 1.Discuss in other deviation.						N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 58	axial displacement	1 1.Compressor surge. 2. Wear of thrust bearing.	1.High axial displacement. 2.Vibration.	1.ZT-3552A/B, ZT-3520A/B, ZT-3553A/B high axial displacement alarms and high high axial displacement trip. 2.XT-3555X/Y , XT-3556X/Y high vibration alarms and high high vibration trip on C-3001 shaft. 3.XT-3520X/Y , XT-3521X/Y high vibration alarms and high high vibration trip on FT-3001 shaft. 4.XT-3557X/Y , XT-3558X/Y high vibration alarms and high high vibration trip on C-3002 shaft.	3	3	2	N	
. 59	power failure	1 1.Cause form DMPC (loss of AC 400V and 230V).	1.Loss of turbine and compressor control. 2.Main lube Oil pump and condensate pump motors, heaters stop. 3.Turbine trip. 4.Refer to low flow of lube oil.	1.UPS and EDG feed UCP and emergency pump.	4	2	2	N	
. 60	instrument air failure	1 1.Causes from source. 2.Rupture of IA line.	1.Loss of control. 2.Plant including compressor shut down and depressuring.	1.N2 backup.	3	3	2	N	

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Utility

Node description P-7001A/B/C (BFW pump package)

Drawing no : DGN-P&ID-DST-01

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Pipe / equipment n P-7001A/B/C, FT-7001A/B

Design purpos To provide HP BFW pump driving force.(turbine operation condition: steam inlet 43 barG, 345 degree C)

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
7007 . 1	high pressure(turbine)	1 HPS from header high pressure.	Damage turbine(casing failure) and steam inlet pipe leak.	1.PV-7004 open. 2.PSV-7010/7011/7012(set pressure:52 barG).	3	4	3	N	Add high pressure alarm and high high pressure trip at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.
. 2	high pressure(Lube oil)	1 1.Oil pumps switch error cause two pumps running simultaneously. 2.Filter blocked. 3.Very low temperature.	1.Lube oil system pressure increase and cause pipe leak. 2.Damage bearings and might be damage shaft.	1.PCV-7710A/B/C adjust pressure. 2.PSV-7710A/B/C, 7720A/B/C on the outlet of oil pumps. 3.PDSH-7710A/B/C high d/p alarm for filter blocked. 4.Two filters, one run one spare.	3	4	3	N	Add high pressure alarm and automatic stop auxiliary oil pump.
. 3	low pressure(trubine)	1 HPS from header low pressure.	1.Same as 2005.4 low/no flow(BFW). 2.Increase consumption of the steam.	1.PALL-7127 low pressure alarm and low low pressure auto start P-7001C. 2.LSAL-2372(2oo3) low level trip IS-01. 3.LIA-2373 low level alarm. 4.LICA-2372 low level alarm.	4	3	3	N	
. 4	low pressure(Lube oil)	1 1.Oil pumps failure. 2.Filter blocked or switch operation error. 3.PCV-7710A/B fail closed. 4.Oil pipe leakage.	Turbine and HP BFW pump wear out and damage in worst case.	1.PSL-7710A/B/C low pressure switch. 2.PSLL-7710A/B/C, 7720A/B/C, 7730A/B/C(2oo3) low low pressure switch. 3.PDSH-7710A/B/C high d/p alarm for filter blockage.	3	4	3	N	1.Cancel PSL-7710A/B/C switch. 2.Use transmitter instead of all switch(PDT-7710A/B/C, PT-7710A/B/C, 7720A/B/C, 7730A/B/C and others). 3.PT-7710A/B/C, 7720A/B/C, 7730A/B/C (medium of 3) low pressure alarm and start the auxiliary oil pump, low low pressure(2oo3) to trip.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 5	high temperature(Lube oil)	1 1.Cooling water failure. 2.Oil heater fail to overheating.	Loss of oil film cause shaft to wear out and damage bearings .	1.High temperature alarms and high high temperature trip on bearings. 2.TSH-7710A/B/C high temperature alarm and high high temperature switch off L.O. heater. 3.TCV-7710A/B/C adjust temepature.	2	3	1	N	
. 6	high temperature(inlet turbine)	1 HPS from header high temperature.	Turbine overtemperature, damage turbine and steam inlet pipe leak.	Desuperheater on the steam header DS-7010A/B.	3	4	3	N	Add high temperature alarm and high high temperature trip at turbine inlet pipe.
. 7	high temperature(outlet turbine)	1 No load operation.	High temperature in exhaust of turbine.		2	4	2	N	Add TT high temperature alarm and high high temperature trip at turbine outlet pipe.
. 8	low temperature(Lube oil)	1 1.External low temperature. 2.Cooling water overflow.	1.Viscosity of lube oil increase and cause shaft to wear out and damage turbine and BFW pump. 2.Decrease the performance of lube oil pump and decrease the oil supply. 3.Increase d/p of the filter.	1.Lube oil heater will switch on when external low temperature. 2.PDSH-7710A/B/C d/p switch for filter.	2	4	2	N	Add low temperature alarm and auto start oil heater EH-7001A/B/C.
. 9	low level (oil tank)	1 1.Oil tank leakage. 2.Pipe leakage. 3.Drain abnormally open.	1.No oil to the bearings. 2.Damage oil pump.	1.LSL-7710A/B/C low level switch. 2.PSLL-7710A/B/C, 7720A/B/C, 7730A/B/C low low pressure switch. 3.Blind after the drain valve.	3	3	2	N	Add low level alarm and low low level trip for LSL-7710A/B/C.



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 10	high speed	1 1.Increase turbine speed due to human error. 2.Actuator/governor valve fail open. 3.Coupling fracture or pump no load.	Overspeed and damage turbine and HP BFW pump.	1.SE(2oo3) overspeed trip and drain control oil, close HPS trip valve. 2.Mechanical device activate spring to close HPS trip valve. 3.HS bottom to close HPS trip valve.	4	2	2	N	
. 11	low speed	1 1.Turbine running is lower than minimum allowable operating speed due to steam header low pressure 2.Governor valve fail closed. 3.Pump overload.	1.Loss power of turbine and low pressure of BFW. 2.Increase consumption of the steam. 3.Decrease oil pressure.	PALL-7127 low pressure alarm and low low pressure auto start P-7001C.	3	4	3	N	1.Add low pressure and low temperature alarm at turbine inlet utilizing inlet PT and TT to send signal to CW-Hydro PLC. 2.Add minimum allowable low continuous speed alarm.
. 12	high vibration	1 1.Turbine rotor unbalanced. 2.Oil film unstable between shaft and bearing. 3.Parts loosening. 4.Misalignment between equipments.	Damage turbine, gear box and HP BFW pump.	High vibration alarms and high high vibration trip.	4	2	2	N	
. 13	other	1 1.Axial displacement. 2.Excess force due to steam with water.	Damage thrust bearings and damage rotor.	1.High axial displacement alarm and high high trip. 2.Steam trap in each steam turbine inlet and steam piping condensate will be collected by unit X-7020.	3	3	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	other	2						N	Due to absence of CW-Hydro representative in HAZOP meeting, some HAZOP items will be checked by Owner later. As the latest P&ID of vendor are not received in HAZOP meeting, further recommendations can be stated later. TCC should prepare the latest P&IDs of this package and send them to Owner during two weeks.

# HAZOP analyzing record

2017/3/22

Project name : MKP methanol Project

Establish dt : 2016/8/10 Am12:00:00

Company nam Middle East Kimiaye Pars Company

Plant site :

Project no :

Risk matrix : 8X7(TCC) (imported) (imported) (imported)

Process name : Utility

Node description Turbine for P-0501 1/2 (CW pump)

Pipe / equipment n P-0501 1/2, FT-0501 1/2

Drawing no : DGN-P&ID-DS-01

Design purpos To provide cooling water pump driving force.(operation condition: steam inlet  
43 barG, 345 degree C)

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
7008 . 1	high pressure(turbine)	1 HPS from header high pressure.	Damage turbine(casing failure) and steam inlet pipe leak.	1.PV-7004 open. 2.PSV-7010/7011/7012(set pressure:52 barG).	3	4	3	N	Add high pressure alarm and high high pressure trip at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.
. 2	high pressure(Lube oil)	1 1.Oil pumps switch error cause two pumps running simultaneously. 2.Filter blocked. 3.Very low temperature.	1.Lube oil system pressure increase and cause pipe leak. 2.Damage bearings and might be damage shaft.	1.PCV-0541 1/2 adjust pressure. 2.PSV-0541 1/2, PSV-0542 1/2 on the outlet of oil pumps. 3.PDSH-0541 1/2 high d/p alarm for filter blocked. 4.Two filters, one run one spare.	3	4	3	N	Add high pressure alarm and automatic stop auxiliary oil pump.
. 3	low pressure(trubine)	1 HPS from header low pressure.	1.Plant shutdown. 2.Shortage of CW in consumers, lead to high temperature and finally failure of cooling in CW exchanger. 3.Increase consumption of the steam.	1.PIA-0514 low pressure alarm at P-0501 1/2, P-0502A/B outlet. 2.FIA-0514 flow indicator. 3.FIA-0511 flow indicator. 4.CW pumps 3 operate 1 spare(two pumps running with steam turbine and one with electrical driven, so in this case only one pump will be in the service up to another electrical driven pump come in the service and the plant maybe face to the shutdown).	4	3	3	N	Add low pressure alarm at turbine inlet utilizing inlet PT to send signal to CW-Hydro PLC.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 4	low pressure(Lube oil)	1 1.Oil pumps failure. 2.Filter blocked or switch operation error. 3.PCV-0541 1/2 fail closed. 4.Oil pipe leakage.	Turbine and HP BFW pump wear out and damage in worst case.	1.PSL-0541 1/2 low pressure switch. 2.PSLL-0541 1/2, 0542 1/2, 0543 1/2(2oo3) low low pressure switch. 3.PDSH-0541 1/2 high d/p alarm for filter blockage.	3	4	3	N	1.Cancel PSL-0541 1/2 switch. 2.Use transmitter instead of all switch(PDT-0541 1/2, PSLL-0541 1/2, 0542 1/2, 0543 1/2 and others). 3.PT-0541 1/2, 0542 1/2, 0543 1/2 (medium of 3) low pressure alarm and start the auxiliary oil pump, low low pressure(2oo3) to trip.
. 5	high temperature(Lube oil)	1 1.Cooling water failure. 2.Oil heater fail to overheating.	Loss of oil film cause shaft to wear out and damage bearings .	1.High temperature alarms and high high temperature trip on bearings. 2.TSH-0541 1/2 high temperature alarm and high high temperature switch off L.O. heater. 3.TCV-0541 1/2 adjust temeprature.	2	3	1	N	
. 6	high temperature(inlet turbine)	1 HPS from header high temperature.	Turbine overtemperature, damage turbine and steam inlet pipe leak.	Desuperheater on the steam header DS-7010A/B.	3	4	3	N	Add high temperature alarm and high high temperature trip at turbine inlet pipe.
. 7	high temperature(outlet turbine)	1 No load operation.	High temperature in exhaust of turbine.		2	4	2	N	Add TT high temperature alarm and high high temperature trip at turbine outlet pipe.
. 8	low temperature(Lube oil)	1 1.External low temperature. 2.Cooling water overflow.	1.Viscosity of lube oil increase and cause shaft to wear out and damage turbine and CW pump. 2.Decrease the performance of lube oil pump and decrease the oil supply. 3.Increase d/p of the filter.	1.Lube oil heater will switch on when external low temperature. 2.PDSH-0541 1/2 d/p switch for filter.	2	4	2	N	Add low temperature alarm and auto start oil heater EH-0501 1/2.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 9	low level (oil tank)	1 1.Oil tank leakage. 2.Pipe leakage. 3.Drain abnormally open.	1.No oil to the bearings. 2.Damage oil pump.	1.LSL-0541 1/2 low level switch. 2.PSLL-0541 1/2, 0542 1/2, 0543 1/2 low low pressure switch. 3.Blind after the drain valve.	3	3	2	N	Add low level alarm and low level trip for LSL-0541 1/2 .
. 10	high speed	1 1.Increase turbine speed due to human error. 2.Actuator/governor valve fail open. 3.Coupling fracture or pump no load.	Overspeed and damage turbine and CW pump.	1.SE-0541 1/2, SE-0542 1/2, SE-0543 1/2 (2oo3) overspeed trip and drain control oil, close HPS trip valve. 2.Mechanical device activate spring to close HPS trip valve. 3.HS bottom to close HPS trip valve.	4	2	2	N	
. 11	low speed	1 1.Turbine running is lower than minimum allowable operating speed due to steam header low pressure 2.Governor valve fail closed. 3.Pump overload.	1.Loss power of turbine and low pressure of CW. 2.Increase consumption of the steam. 3.Decrease oil pressure.	Start standby pump.	3	4	3	N	1.Add low pressure and low temperature alarm at turbine inlet utilizing inlet PT and TT to send signal to CW-Hydro PLC. 2.Add minimum allowable low continuous speed alarm.
. 12	high vibration	1 1.Turbine rotor unbalanced. 2.Oil film unstable between shaft and bearing. 3.Parts loosing. 4.Misalignment between equipments.	Damage turbine, gear box and CW pump.	High vibration alarms and high high vibration trip.	4	2	2	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 13	other	1 1.Axial displacement. 2.Excess force due to steam with water.	Damage thrust bearings and damage rotor.	1.High axial displacement alarm and high high trip. 2.Steam trap in each steam turbine inlet and steam piping condensate will be collected by unit X-7020.	3	3	2	N	
		2						N	Due to absence of CW-Hydro representative in HAZOP meeting, some HAZOP items will be checked by Owner later. As the latest P&ID of vendor are not received in HAZOP meeting, further recommendations can be stated later. TCC should prepare the latest P&IDs of this package and send them to Owner during two weeks.

# HAZOP analyzing record

2017/2/28

Project name : MKP Methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Utility

Node description Flare system

Drawing no : MKP-11-DE-8500-PR-PID-001~005.

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n D-8511, P-8511, D-8501, E-8501, FL-8501, FL-8502, FL-8503, D-8502,  
X-8501, PIL-8501A~D.

Design purpos Tail gas treatment.



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
7009 . 1	no flow(flare gas)	1 Same as 7009.10 vacuum.						N	
. 2	high level(D-8511)	1 1.Flare gas high flow and/or flare gas contenting liquid too much. 2.Failure of LT-8511.	D-8511 overfill, cause explosion in worst case.	LIA-8511A high level alarm and high high level activate I-8511A to start P-8511 to remove liquid to TK-5003.	5	2	3	Y	Add another level transmitter of D-8511 with high level alarm.
. 3	low/no level(D-8511)	1 No significant issue identified.						N	
. 4	high level(D-8501)	1 Overflow of flare gas or content too much liquid.	D-8501 overfill, cause explosion in worst case.	LIAS-8502 high level alarm and high high level to start electric heater E-8501.	5	2	3	N	
. 5	low/no level(D-8501)	1 No significant issue identified.						N	
. 6	high pressure(flare gas)	1 1.Molecular seal FL-8503 blockage. 2.D-8511 overfill.	Flare system overprssure.	1.PIA-8514 high pressure alarm. 2.PIAS-8524A/B high pressure alarm.	4	3	3	N	
. 7	high pressure(D-8502)	1 PT/PIC/PV-8529 fail open.	D-8502 overpressure.	D-8502 have a PSV.	4	4	4	Y	PG-8541 change to PT-8541 and send a signal to PLC and add high pressure alarm.
. 8	low pressure(D-8502)	1 1.PSV of D-8502 open prematurely or leak. 2.PT/PIC/PV-8529 fail closed.	Pilot gas supply failure.	PIA-8527 low pressure alarm.	3	4	3	N	PG-8541 change to PT-8541 and send a signal to PLC and add low pressure alarm.
. 9	low pressure(flare gas)	1 No significant issue identified.						N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 10	vacuum(flare gas)	1 1.No flaring. 2.Flare gas condensation cause vacuum.	Back pressure, air to flare system.	1.N2 supply (FO-8501~8505) keep pressure in flare header ° 2.PT/PIC/PV-8516 open. 3.PIA-8514 low pressure alarm. 4.PIAS-8524A/B low pressure alarm and low low pressure to activate I-8523 to open UV-8523 to make up fuel gas.	3	3	2	N	
. 11	high temperature(flare gas)	1 Low pressure cause flame in flare tips.	Back fire.	1.TIAS-8544 high temperature alarm. 2.TIAS/TV-8544 open. 3.TIAS-8541 high temperature alarm activate TV-8541 to open HPS.	4	3	3	Y	Vendor to advise: TIAS/TV-8544 as a safeguard.
. 12	low temperature(flare gas)	1 No significant issue identified.						N	
. 13	others	1 Ignition system failure.	No ignition function if pilot need to be ignited.					N	HAZOP study should be done by vendor for flare gas system package, the owner will check flare package after receiving vendor data.

# HAZOP analyzing record

2017/2/28

Project name : MKP Methanol Project

Company nam Middle East Kimiaye Pars Company

Project no :

Process name : Utility

Node description POC

Drawing no : MKP-11-DE-9400-PR-PID-002

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n PD-9401, PD-9402, PD-9403, PD-9404, PD-9406, PD-9407, PD-9408,  
PD-9409, PD-9410, PD-9411, P-9401A/B, P-9402A/B,  
P-9403A/B, P-9404A/B, P-9408A/B, P-9409A/B, P-9411.

Design purpos

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
7010 . 1	high level(PD-9401/9402/9403/9404 for submerged pump)	1 1.Overflow blocked.	1.Flooding.	1.LT/LIA-9401/9402/9403/9404 High level alarm,manually start pump P-9401//9402/9403/9404A/B.	2	4	2	N	
. 2	low level(PD-9401/9402/9403/9404 for submerged pump)	1 non actual hazard identify						N	
. 3	high level(PD-9409/9410 for submerged pump)	1 1.Too much liquid from upstream. 2. Discharge of pump abnormally close.	1.Flooding.	1.LT/LIA-9409/9410 High level alarm,automatically start pump P-9409//9410A/B.	2	4	2	N	
. 4	low level(PD-9409/9410 for submerged pump)	1 non actual hazard identify						N	
. 5	high level(PD-9411 for submerged pump)	1 1.Too much liquid from upstream. 2. Discharge of pump abnormally close.	1.Flooding	1.LT/LIA-9411 High level alarm,manually start pump P-9411.	2	4	2	N	
. 6	low level(PD-9411 for submerged pump)	1 non actual hazard identify						N	
. 7	high level(PD-9408 for centrifugal pump)	1 1.Too much liquid from upstream. 2.Discharge of pump abnormally close.	Flooding	1.LT/LIA-9408 high level alarm,manually start pump P-9408A/B.	2	4	2	N	
. 8	low level(PD-9408 for centrifugal pump)	1 non actual hazard identify						N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 9	high level(PD-9406/9407 for portable pump)	1 1.Too much liquid from upstream. 2.Discharge of pump abnormally close.	Flooding	1.LT/LIA-9406/9407 high level alarm,manually start portable pump.	2	4	2	N	1.Add plant air connection for portable pumps.
. 10	low level(PD-9406/9407 for portable pump)	1 non actual hazard identify						N	
. 11	As well as flow(PD-9408)	1 1.High/low pH.	1.Pollution. 2.Water isn't accepted by DMPC.	1.AI-9402 pH indicator. 2.AI-9401 pH gauge on site.	3	4	3	N	
. 12	low pressure of discharge pump(PD-9411)	1 1.P-9411 broken.	1.Flooding.	1.LT/LIA-9411 high alarm.	2	4	2	N	
. 13	other	1						N	1.Consider curb with anti-acid brick for H2SO4 solution tank and NaOH solution tank.

# HAZOP analyzing record

2017/2/27

Project name : MKP Methanol Project

Company name Middle East Kimiaye Pars Company

Project no :

Process name : Polishing Unit

Node description Polishing Unit

Drawing no : 7200-PID-001~005

Establish dt : 2016/8/10 Am12:00:00

Plant site :

Risk matrix : 8X7(TCC) (imported) (imported)

Pipe / equipment n TK-7001 1/2, P-7002A/B, P-7204A/B, TK-7202/7204, P-7202/7203,  
J-7201/7202, D-7205, PD-7206, P-7205A/B, TK-7201, P-7201A/B,  
R-7201A/B, X-7201, E-7201A/B

Design purpos cooling water circulating, CW supply 38 degree C, CW return 48 degree C, Cl-  
less than 65 mg/L.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
7201 . 1	High flow(DMW inlet)	1 1.DMW from BL high flow. 2.FV-7202 fail. 3.FV-7202 bypass valve abnormally open due to human error .	1.TK-7201 high level and flood. 2.High consumption of DMW.	1.LT/LIA-7201 high level alarm. 2.Overflow line.	3	3	2	N	
. 2	High flow(DMW outlet)	1 1.P-7201 A/B standby pump abnormally start. 2.FV-7091 fail open.	1.TK-7001 1/2 low level and P-7002 A/B damage. 2.D-7001 high level. Refer to node 7004 high level(D-7001). 3.DMW to deaerator temperature decrease and low deaerator efficiency.	1.LT-7202A/B low level alarm, low low level alarm and stop the P-7002A/B. 2.FIC-7091 high flow alarm. 3.FI-7205 flow indicator. 4.TV-2457 and TE-2457 control the temperature.	3	3	2	N	
. 3	High flow(condensate inlet)	1 1.High flow in upstream.	1.X-7201A/B and X-7204 high d/p and running period decrease. 2.High temperature of X-7201A/B and X-7204. 3.TK-7201 high level.	1.PDIA-7210/7211A/B high d/p alarm. 2.LIA-7201 high level alarm. 3.Overflow line TK-7201. 4.LICA-7202 A/B high level alarm. 5.FV-7202.	3	3	2	N	1.Add a temperature transmitter and send the signal to control room, set high alarm in the 8"-TC-72-201-B50-N inlet line of X-7201A/B and X-7204.
. 4	High flow(R-7201A/B inlet)	1 1.P-7201 A/B standby pump abnormally start.	1.Overflow of R-7201A/B.	1.FT-7203A/B. 2.PDT-7207/8 high alarm.	3	3	2	N	
. 5	low/no flow(DMW inlet)	1 1.Low/no flow in upstream. 2.FV-7202 fail closed.	1.TK-7201 low level and P-7201A/B cavitation and damage.	1.FT/FIQ-7204 alarm. 2.LICA-7201 low level alarm. 3.LALL-7201 activate I-721 to trip P-7201A/B.	4	3	3	N	1.Change FIQ-7204 to FI-7204.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 6	low/no flow(DMW outlet)	1 1.P-7002 A/B failure. 2.P-7002 outlet manual valve abnormally closed due to operator error. 3.FT/FIC/FV-7091 fail closed. 4.TK-7001 1/2 outlet manual valve abnormally closed due to operator error. 5.ARV in the discharge of pump fail and return maximum possible flow back to TK-7001 1/2.	1.TK-7001 A/B high level and flood. 2.Refer to node 7004 low flow(DMW). 3.Low/no flow of BFW in downstream especially steam drum. 4.P-7002 A/B cavitation and damage.(in the case of cause 4)	1.P-7002 A/B 1 operate 1 spare. 2.FI-7205 flow indicator. 3.LICA-7202 A/B high level alarm. 4.Refer to node 7004 low flow(DMW).	3	3	2	N	1.Add low alarm for FT-7205.
. 7	low/no flow(condensate intlet)	1 1.Low/no flow in upstream,C-3001/2 FT-3001 shutdown. 2.Human error in closing manual valve. 3.X-7201A/B and X-7204 blocked. 4.E-7201 A/B blocked.	1.TK-7201 low level and P-7201 A/B cavitation and damage.	1.FI-7201 flow indicator. 2.LIA-7201 low level alarm. 3.LALL-7201 activate I-721 to trip P-7201A/B. 4.X-7201 standby. 5.E-7201 A/B, 1 operate 1 spare. 6.PT-7203/7202 low alarm. 7.PDT-7210/11A/B high d/p alarm.	3	3	2	N	1.Add low alarm for FI-7201. 2. Add FI and low alarm for FI-7204 (DMW from B.L)
. 8	low flow (R-7201A/B inlet)	1 1.P-7201A/B failure. 2. Manual valve abnormally close.	1.TK-7001 1/ 2 low level.	1.LT-7202A/B low level alarm. 2.FT-7203A/B indicator. 3.Auto start P-7201A/B by PT-7209.	2	4	2	N	1.Add low alarm for FT-7203A/B.



Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 9	reverse flow(DMW)	1 1.Low pressure of DMW from B.L. 2. High pressure of TC.	1.Loss of condensate. 2.Low level TK-7201. 3.Pollution of DMW to B.L.	None	2	4	2	N	1.Add check valve on 8"-DMW-70-108-B50-N of 7000-PID-020.
. 10	reverse flow(condensate)	1 1.Low pressure/failure of TC from P-3011A/B. 2.High pressure of DMW.	1.Loss of DMW. 2.Low level TK-7201.	1.PSL-3584 on C-3001 Package.	2	4	2	N	1.Add check valve on 8"-TC-72-201-B50-N. 2.P-3011A/B should be considered as auto start(should be confirmed with GE).
. 11	as well as flow/impurity	1 1.R-7201A/B low efficiency. 2.Impurity in upstream(DMPC). 3.Failure of turbine surface exchanger lead to impurities in condensates. 4.Impurity in chemicals NaOH and H2SO4.	1.Fe2+ and SiO2 carry over to downstream and affect steam quality and damage turbine. 2.High demand to blowdown in deaerator and steam drum. 3.Incorrect pH in downstream and corrosion.	1.R-7201 A/B ,1 operate 1 spare. 2.AI-7203 high SiO2 alarm. 3.AI-7204A/B high conductivity alarm. 4.AAHH-7203,AAHH-7204A/B activate I-727A/B to regeneration. 5.AIA-7211A/B high/low pH alarm.	3	4	3	N	Supply chemical from well known vendor, with high quality and test before use in plant.
. 12	high pressure(condensate)	1 1.X-7201A/B,X-7204 blockage. 2.Human error in operating both P-3011A/B at the same time.	1.Overpressure damage equipment and pipe.	1.PT-7202 indicator. 2.PSV-7206A/B and PSV-7205 @9bar.	3	3	2	N	1.Add alarm high for PT-7202. 2. Correct setpoint of PSV-7205 and PSV-7206A/B to 10 barg.
. 13	high pressure(DMW)	1 1.X-7201A/B,X-7204 blockage. 2.High pressure in upstream.	1.Overpressure damage equipment and pipe. 2.Back pressure to P-3011A/B.	1.PT-7203 indicator. 2.PSV-7206A/B and PSV-7205 @9bar. 3.Check valve on discharge of P-3011A/B.	3	3	2	N	1.Add alarm high for PT-7203. 2.Correct setpoint of PSV-7205 and PSV-7206A/B to 10 barg.

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LO PA	Recommendation
. 14	high pressure(R-7201A/B)	1 1.R-7201A/B blocked; 2.XV-7209A/B abnormally closed. 3. P-7201A/B start at the same time.	1.Damage of R-7201A/B. 2.Low Mixed bed efficiency.	1.PSV-7203A/B @6bar. 2.PT-7207A/B indicator.	3	4	3	N	1.Add alarm high for PT-7207A/B. 2. Correct setpoint of PSV-7203A/B to 7 barg.
. 15	high pressure(DMW to user)	1 1.P-7002A/B start at the same time. 2.Closed failure of FV-7091.	1.High pressure of E-2025 shell side.	1.PSV-2458 @ 14 barg.	2	3	1	N	1.Correct design pressure of discharge line from P-7002A/B to 14 barg.
. 16	low pressure(Condensate)	1 1.Low pressure due to P-3011A/B failure.	1.Low level of TK-7201.	1.PT/PIA-7202 low pressure alarm. 2.PT/PAL-3584 low pressure alarm.	3	2	1	N	
. 17	low pressure(DMW)	1 1.Low pressure in B.L.	1.Low level of TK-7201.	1.PT/PIA-7203 low pressure alarm.	3	2	1	N	
. 18	low pressure(R-7201A/B)	1 1.P-7201A/B failure.	1.Low level of TK-7001 1/2.	1.PT/PIA-7209 low alarm and low low auto start standby pump.	3	3	2	N	
. 19	low pressure(DMW to user)	1 1.P-7002A/B failure.	1.DMW supply failure.	1.PT/PIA-7204 low pressure alarm and low low auto start standby pump.	3	3	2	N	
. 20	vacuum	1 Not possible.						N	
. 21	high temperature	1 1.CW failure. 2.High temperature from upstream. 3.TE/TT/TIC/TV-7201 fail closed.	1.Process condensate temperature increased and resin failure. 2.Fe2+ and SiO2 carry over to downstream and affect steam quality and damage turbine. 3.Damage pump due to low NPSHa.	1.FI-7202 flow indicator. 2.AI-7203 high SiO2 alarm. 3.AI-7204A/B high conductivity alarm. 4.AAHH-7203,AAHH-7204A/B activate I-727A/B to regeneration.	4	3	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 22	low temperature	1 non actual hazard identify						N	
. 23	concentration of H2SO4 and NaOH	1 1.Failure of H2SO4 injection system. 2.Failure of NaOH injection system. 3.High or low concentration in upstream. 4.Low quality of raw chemical material. 5.Low flow rate of DMW for preparing solution.	1.Low quality and high impurity of final DMW product. 2.Incomplete resin regeneration(in case of low concentration), or high temperature inside ion exchanger(in case of high concentration). 3.Need for more blowdown in downstream. 4.More clean salty water.	1.AAHH-7203 high high SiO2 concentration alarm activate I-727A/B to regeneration. 2.AIA-7206 high conductivity alarm. 3.AIA-7207 pH indicator. 4.AT/AI-7208 H2SO4 indicator. 5.AT/AI-7209 NaOH indicator.	3	3	2	N	1.Add high alarm for AT/AI-7208. 2.Add high alarm for AT/AI-7209.
. 24	high level(TK-7201)	1 1.XV-7201A/B failure. 2.XV-7209A/B failure. 3.P-7201A/B failure. 4.High flow in upstream.	1.TK-7201 overflow.	1.LIAH-7201 high level alarm. 2.Overflow line.	3	2	1	N	
. 25	high level(TK-7001 1/2)	1 1.Blockage of outlet. 2.P-7002A/B failure. 3.High flow in upstream.	1.TK-7001 1/2 high level and flood. 2.High consumption of DMW.	1.LICA-7202A/B high level alarm. 2.Overflow line.	3	2	1	N	
. 26	high level(PD-7206)	1 1.XV-7207~7210 A/B fail open after regeneration.	PD-7206 high level and may flood since liquid content is acid or base so environmental pollution or injury personnel is possible.	1.LIA-7205 high level alarm. 2.The pond is located in a curb.	3	4	3	N	

Serial #	Deviation	Cause	Consequence	Safeguard	Severity	Likelihood	Risk	LOPA	Recommendation
. 27	low/no level(TK-7201)	1 1.Low/no flow in upstream. 2.Human error in opening drain valve.	1.pump damage. 2.Low/no flow in downstream. 3.Loss of condensate.	1.LALL-7201 low low level activate I-721 trip P-7201A/B. 2.FI-7204 flow indicator.	3	3	2	N	
. 28	low/no level(TK-7001 1/2)	1 1.Low/no flow in upstream. 2.Human error in opening drain valve.	1.Pump damage. 2.Low/no flow in downstream, perhaps low/no of BFW.	1.LALL-7202A/B low low level activate I-723 to trip P-7002A/B, P-7204A/B. 2.FI-7205 flow indicator.	3	3	2	N	
. 29	low/no level(PD-7206)	1 Emptying the pond by manual turning on the pump.	1.Pump damage.	1.LIA-7205 low level alarm. 2.LALL-7205 low low level activate I-726 trip P-7205A/B.	2	4	2	N	
. 30	other	1						N	1.HAZOP study should be done by vendor for polishing unit package, the owner will check polishing unit package after receiving vendor data.

Attachment 3  
Attendance sheet

TCC 公司 MKP Methanol 项目

Flue gas blower and turbine Unit

(F1-2001 / F11-2001)  
2017年2月20日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业 Discipline	手机 Mobile phone	邮箱 e-mail
1	S. H. Wang	HAZOP Leader			
2	Y. N. Ying	HAZOP Assistance			
3	Qin Yajun 秦亚君	TCC - Instrument			
4	Morteza Faghhi	MEKPCO. process Eng.			
5	Mojtaba Lame	MEKPCO PROCESS Eng.			
6	Mahmoud Naskollahi	Eng. Manager	Eng	09122505127	
7	Wendy Xie	ITT Representative			
8	VALERIO CICERO	IT PROCESS			
9	MARCELO DELLA COLETTA	PROJECT ENGINEER	ENG		mcoletta@mgmeta lurgica.com.br
10	Wang Fumi Process	Process engineer			
11	Jr Wermer	Process safety engineer			
12	Wang Haijun	TCC			
13	Gao Zhihui 高志辉	TCC. process Eng.			
14					
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TCC 公司 MKP Methanol Project  
Combustion air blower and turbine (F-2002/FT-2002) Unit.  
2017 年 2 月 21 日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业 DISCIPLINE	手机 MOBILE PHONE	邮箱 E-MAIL
1	S.H. Wang	HAZOP Leader			shihhuang.wang@ctci.com
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4	M. Lame	MEKPCO Process			m.lame@mekpco.com
5	Bin Yajun 袁斌君	TCC	Instrument		ea-84j@ctcc.cn
6	Wang Haijun	TCC			
7	Ji Weiwei	TCC	PS		
8	Wang Futui	TCC	PS		
9	MARCELO DELLA COLETTA	NG METALURGIA			mcoletta@ngmetalurgia.com.br
10	Valerio Cicero	Process Engineer ITT			valerio.cicero@ittch.ch
11	Wendy xie	ITT Representative in china			wendyxie@188.com
12	Gao Zhikai	deputy Eng. manager			
13	Chen Tao	TCC			
14					
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16					
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TCC 公司 MKP Methanol Project

Turbine for P-7001 (BFW pump) and  
P-0501 (cooling water pump) Unit

2017年2月22日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业 DISCIPLINE	手机 MOBILE PHONE	邮箱 E-MAIL
1	S.H. Wang	HAZOP Leader			shihhuang.wang@ctci.com
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3	M. Lame	MEKPCO Process Eng.			m.lame@mekpc.com
4	M. Faghihi	MEKPCO Process Eng.			m.faghihi@mekpc.com
5	许秉浩	工艺			aa-xbh@ctcc.cn
6	高翔	deputy eng. manager			
7	田涛	Process			tiantao@ctcc.cn
8	Ji Wei wei	PS			
9	徐军	TCC	Instrument		
10	王江	TCC	Mechanical		
11	孙宇	Dresser-Rand	steam turbine		sun.yu@siemens.com
12					
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TCC 公司 MKP Methanol 项目(Project)  
C-2002 H<sub>2</sub> Recycle Compressor Unit

2017年2月23日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业 DISCIPLINE	手机 MOBILE PHONE	邮箱 E-MAIL
1	S. H. Wang	HAZOP leader.			shihuang.wang@ctci.com
2	谢武	HAZOP engineer			
3	刘松林	HAZOP Engineer			songlin.liu@ctcish.com.cn
4	潘昌霞	YuanDa mech. Engineer		18640099887	ydtc@yuanda.compressor.com
5	邹正超	YuanDa elec. Engineer		15998109324	ydtc@yuanda.compressor.com
6	M. Lame	MEKPCO Process			m.lame@mekpco.com
7	M. Faghghi	MEKPCO Process			m.faghghi@mekpco.com
8	Gao Zhihui	Deputy eng. manager			
9	Wang Furui	Process			
10	李强	TCC	Instrument		
11	Ji Weiwei	TCC	PS		
12					
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TCC

公司 MKP Methanol

项目 (Project)

C-2001 start-up nitrogen compressor Unit

2017年 2月 24日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业 DISCIPLINE	手机 MOBILE PHONE	邮箱 E-MAIL
1	S. H. Wang	HAZOP Leader			shihkuang.wang@ctci.com
2	Troeng Xie	HAZOP engineer			
3	刘松林	engineer			
4	M. lame	mekpco Process Eng.			
5	M. Faghghi	MEKPCO Process Eng.			m.faghghi@mekpco.com
6	徐松	process.			
7	何志辉	Deputy Eng. Manager			
8	李岳洋	项目经理			yueryang.li@shusungpo.com
9	何林	Engineer			
10	张恩远	Engineer			
11					
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TCC

公司 MEKPCO Methanol 项目 (Project)

Polishing Unit

2017年2月27日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业	手机 MOBILE-PHONE	邮箱 E-MAIL
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6	TianTan	Process Engin			tiantan@entec.cn
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8	刘松林	Assistance			
9					
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TCC 公司 MEKPCO Methanol 项目 (project)

POC ponds, side filter of cooling tower Unit

2017 年 2 月 28 日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业	手机 MOBILE PHONE	邮箱 E-MAIL
1	S. H. Wang	HAZOP leader			
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5	Tian Tao	Process Engineer			tiantao@cntec.cn
6	刘松林	Assistance			
7	Ji Weiwei	PS			
8	Nie Xiao	process Engineer			
9					
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TCC 公司 MEKPCO Methanol 项目 (project)

Synthesis compressor package: C3001/C3002/ET3001 Unit

2017年3月1日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业	手机 MOBILE PHONE	邮箱 E-MAIL
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2	Gene Zhang	HAZOP Assistance			
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4	李延海	工艺			qa-hj@cntcc.cn
5	许骏	工艺			
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7	M. Faghghi	MEKPCO Process Eng.			m.faghghi@MEKPCO.com
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9	MASSIMO DIAMANTI	SYSTEMS ENGINEER		3386403522	maite.medapl@unige.com
10	GAIA COSTI	PROCESS ENGINEER		+393423302466	gaia.costi@ge.com
11	LUCA CONTI	GE SYSTEM/CONTROL ENG.			luca.conti@ge.com
12	江昱	工艺		18698080527	jiangyu@cntcc.cn
13					
14					
15					
16					
17					

TCC 公司 MEKPCO Methanol 项目 (project)

Synthesis Compressor Package: (300) / (3002 / FT300) Unit

2017年 3月 2日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业	手机 MOBILE PHONE	邮箱 E-MAIL
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2	Gene Zhang	HAZOP ASSISTANCE			
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4	M. Faghghi	MEKPCO PROCESS			m.faghghi@MEKPCO.com
5	GIUSEPPE STELLA	GE ENGINEERING MANAGER		18918372585	
6	MENAGLIONI DARTA	SYSTEM ENGINEER			monta.meda@hotmail.it
7	CONTI LUCA	SYSTEM ENGINEER			luca.conti@ge.com
8	GAIA COLETTI	PROCESS ENGINEER			gaia.coletti@ge.com
9	Qin Xujun 秦旭军	TCC Instrument			aa-qyj@cntcc.cn
10	秦旭军 Xujun Qin	TCC PROCESS			xujun@cntcc.cn
11	李永华	TCC			aa-lwj@CNTCC.cn
12	侯秋义	TCC			hqy@cntcc.cn
13	江宇	TCC			jiangyu@cntcc.cn
14					
15					
16					
17					

TCC 公司 MEKPCO Methanol 项目 (Project)  
 Synthesis Compressor package, C3001/C3002/FUnit<sup>3001</sup>

2017年3月3日 HAZOP、LOPA、SIL 分析签到表

会议提要: \_\_\_\_\_

序号	姓名 NAME	岗位 POSITION	专业	手机 MOBILE PHONE	邮箱 E-MAIL
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5	李永明	TCC process			aa-bj@cn-tcc.cn
6	M. Fagbibi	MEKPCO Process			m.fagbibi@mekpc.com
7	M. lame	MEKPCO Process			m.lame@mekpc.com
8	MARTA MEDAGLIONI	SYSTEM GE ENGINEER			marta.medaglioni@ge.com
9	GIUSEPPE STELLA	GE ENGINEERING MANAGER			GIUSEPPE.STELLA@GE.COM
10	LUCA CONTI	GE SYSTEM ENGINEER			LUCA.CONTI@GE.COM
11					
12					
13					
14					
15					
16					
17					

Attachment 4  
Mark-up P&ID



# Node 0501

## GENERAL NOTES

1. INSTRUMENT AIR PIPE HEADER WILL BE CONNECTED TO ALL PNEUMATIC VALVE.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

Approved For Construction	11.10.2016	Nie Xiao	Tian Tao	Xie Xuan			
Issued For Approval	15.07.2016	Nie Xiao	Tian Tao	Xie Xuan			
Issued For Comments	06.06.2016	Nie Xiao	Tian Tao	Xie Xuan			
REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

THIS DOCUMENT IS THE PROPERTY OF TCC. NO PART OF THIS DOCUMENT SHALL BE REPRODUCED OR DISCLOSED TO OTHERS OR USED FOR ANY PURPOSE WHATSOEVER EXCEPT WITH THE PRIOR WRITTEN PERMISSION OF TCC.

OWNER:

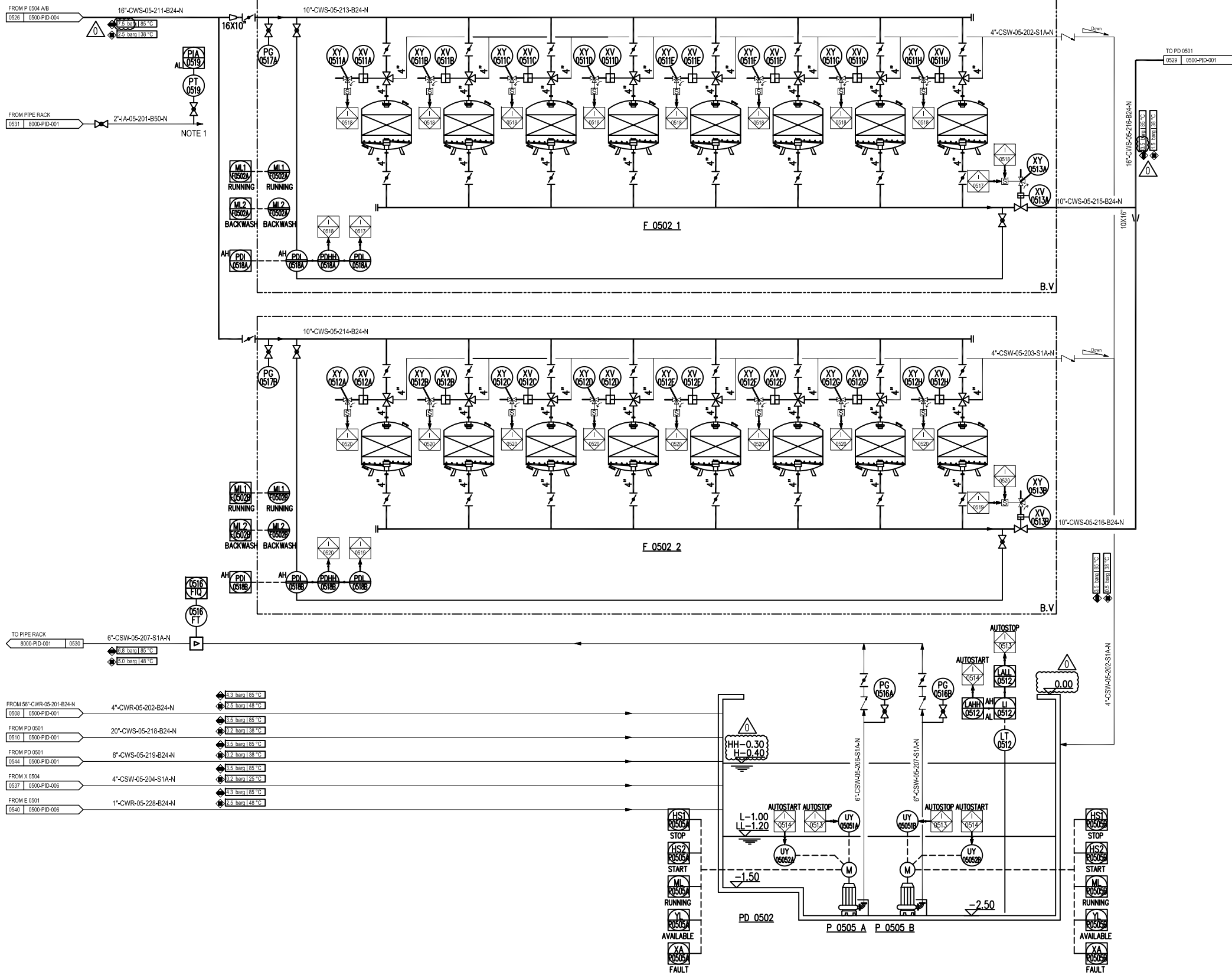
**Middle East  
Kimiaye Pars Company**

HALDOR TOPSØE A/S	DOCUMENT NAME:	JOB NO.:	DOC. NO.:	REV.:
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<b>TCC</b> 中國天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION	CONTRACTOR DRAWING NO.			
	MKP-11-DE-0500-EE06-PID-005			
	SHEET	TOTAL	01	

SUB-CONTRACTOR DRAWING NO.	
SHEET	TOTAL

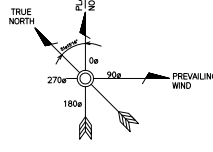
P&ID FOR COOLING WATER FILTER		PROJECT	MKP Methanol Project
		UNIT	COOLING WATER UNIT
		PHASE	DETAIL ENGINEERING
SCALE	SHEET 1	TOT. 1	SIZE A1
OWNER DWG NO.	MKP-11-DE-0500-PR-PID-005		



FROM P.0504 A/B	16" CW-05-211-B24-N	EL. 135.70 m	2.5 barg
FROM PIPE RACK	2" IA-05-201-B50-N		
FROM 56" CWR-05-201-B24-N	4" CWR-05-202-B24-N	EL. 148.70 m	1.5 barg
FROM PD.0501	20" CW-05-218-B24-N	EL. 138.70 m	2.2 barg
FROM PD.0501	8" CW-05-219-B24-N	EL. 135.70 m	2.5 barg
FROM X.0504	4" CSW-05-204-S1A-N	EL. 125.70 m	2.5 barg
FROM E.0501	1" CWR-05-228-B24-N	EL. 148.70 m	1.5 barg

F.0502 1/2	COOLING WATER FILTER QUARTZ SAND	PD.0502	CLEAN SALTY WATER POND	P.0505 A/B	CLEAN SALTY WATER PUMP
CAPACITY	320 m <sup>3</sup> /h	LXWXH(mm)	10000X6500X1500	CAPACITY	55 m <sup>3</sup> /h
MATERIAL SHELL	C.S	NOMINAL CAPACITY	80 m <sup>3</sup>	HEAD	50 m
DENSITY@OT	993 kg/m <sup>3</sup>	DESIGN PRESS.	ATM	DENSITY@OT	989 kg/m <sup>3</sup>
INSULATION/TRACING	NONE	DESIGN TEMP.	85 °C	INSULATION/TRACING	NONE
AUXILIARY PIPING	BY VENDOR	INSULATION	NONE	AUXILIARY PIPING	BY VENDOR
MATERIAL CASING	C.S+RUBBER			TYPE	SUBMERGED
MATERIAL FILTER ELEMENT	QUARTZ SAND			MATERIAL	C.S
ELEV. OF FOUNDATION	EL. +100.70 m			ELEV. OF FOUNDATION	EL. +97.80 m

Counter	Sign	Date
---------	------	------



N-10 To flare  
Class150 NPS1 1/2"  
ASME B16.5 WN/RF

N-9 N2 inlet  
Class150 NPS1"  
ASME B16.5 WN/RF

N-11 Vent to safe location  
Class150 NPS1 1/2"  
ASME B16.5 WN/RF

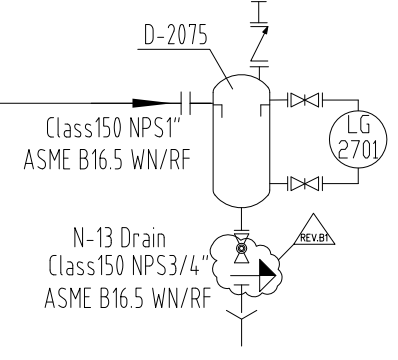
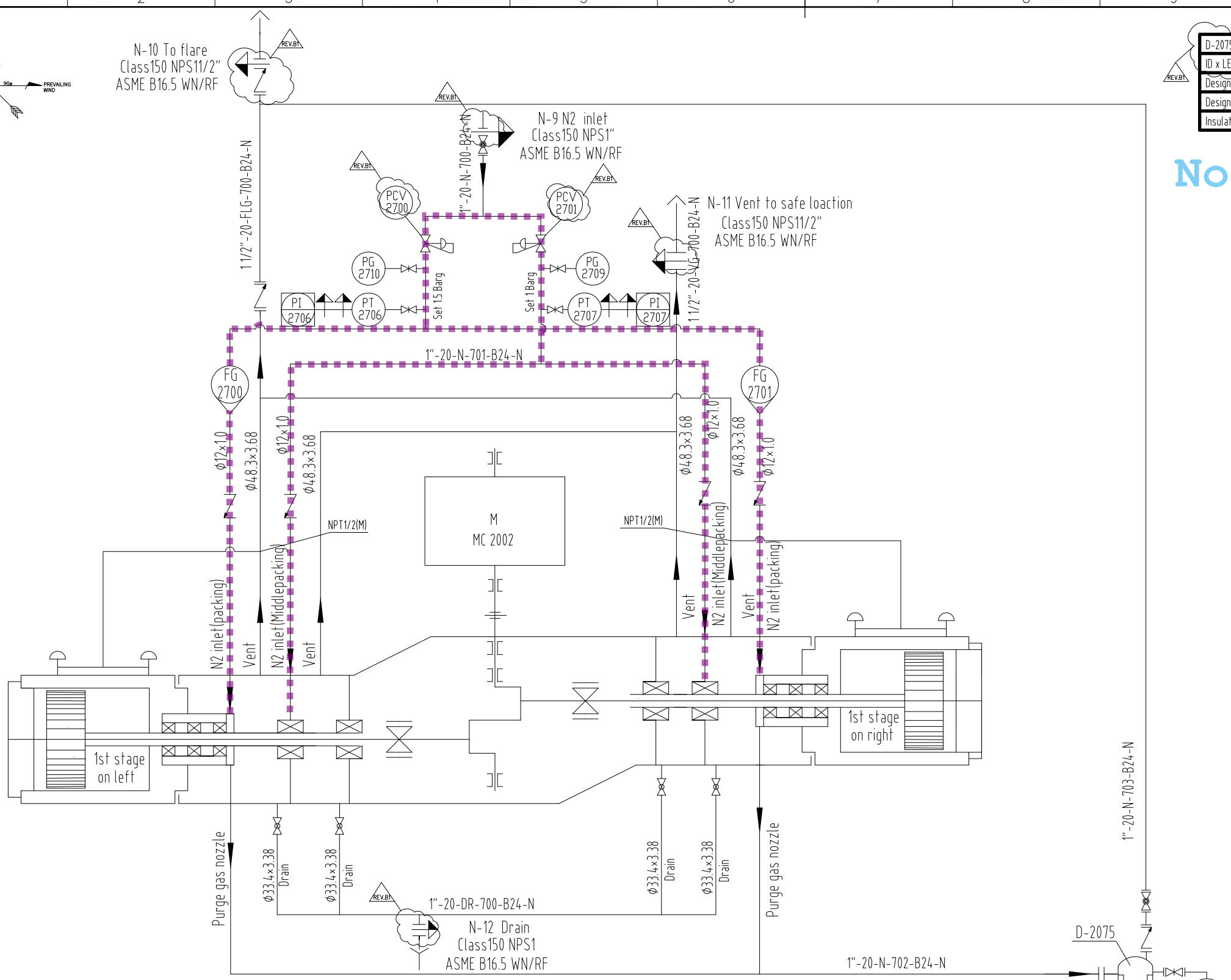
D-2075	Purge tank
ID x LENGTH	219 x 850 mm
Design Press.	10 Barg
Design Temp.	100°C
Insulation	None

# Node 2007

## Legend

Symbol	Description
	Purge tank
	Gate Valve
	Globe Valve
	Ball Valve
	Needle Valve
	Local Gauge
	PLC instrument
	Pipe
	Unloader
	Regulator Valve
	Check Valve
	Drain
	Vent

Scope Split  
User Vendor



Counter Signing	Sign	Date

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

OWNER: Middle East Kimiaye Pars Company

LENSOR: HALDOR TOPSØE A/S

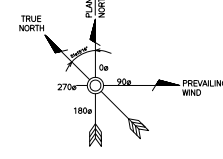
CONTRACTOR: 中国天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION

CONTRACTOR DRAWING NO.	
SHEET	TOTAL
SUB-CONTRACTOR DRAWING NO.	
2D6.5(Y95).00	
SHEET	TOTAL
1	1

PROJECT: MKP Methanol Project  
UNIT: REFORMER  
PHASE: DETAIL\_ENGINEERING

OWNER DWG NO. MKP-VD-9000-306-003-A1

SCALE 1:1 SHEET:1 TOT.:1 SIZE: A1



D-2070/D-2072	1st stage suction damper on left/on right
ID x LENGTH	325 x 1310 mm
Design Press.	60 Barg
Design Temp.	100°C
Insulation	None

D-2071/D-2073	1st stage discharge damper on left/on right
ID x LENGTH	325 x 1310 mm
Design Press.	60 Barg
Design Temp.	200°C
Insulation	Personnel Protection

D-2074	1st stage separator
ID x LENGTH	424 x 1980 mm
Design Press.	60 Barg
Design Temp.	100°C
Insulation	None

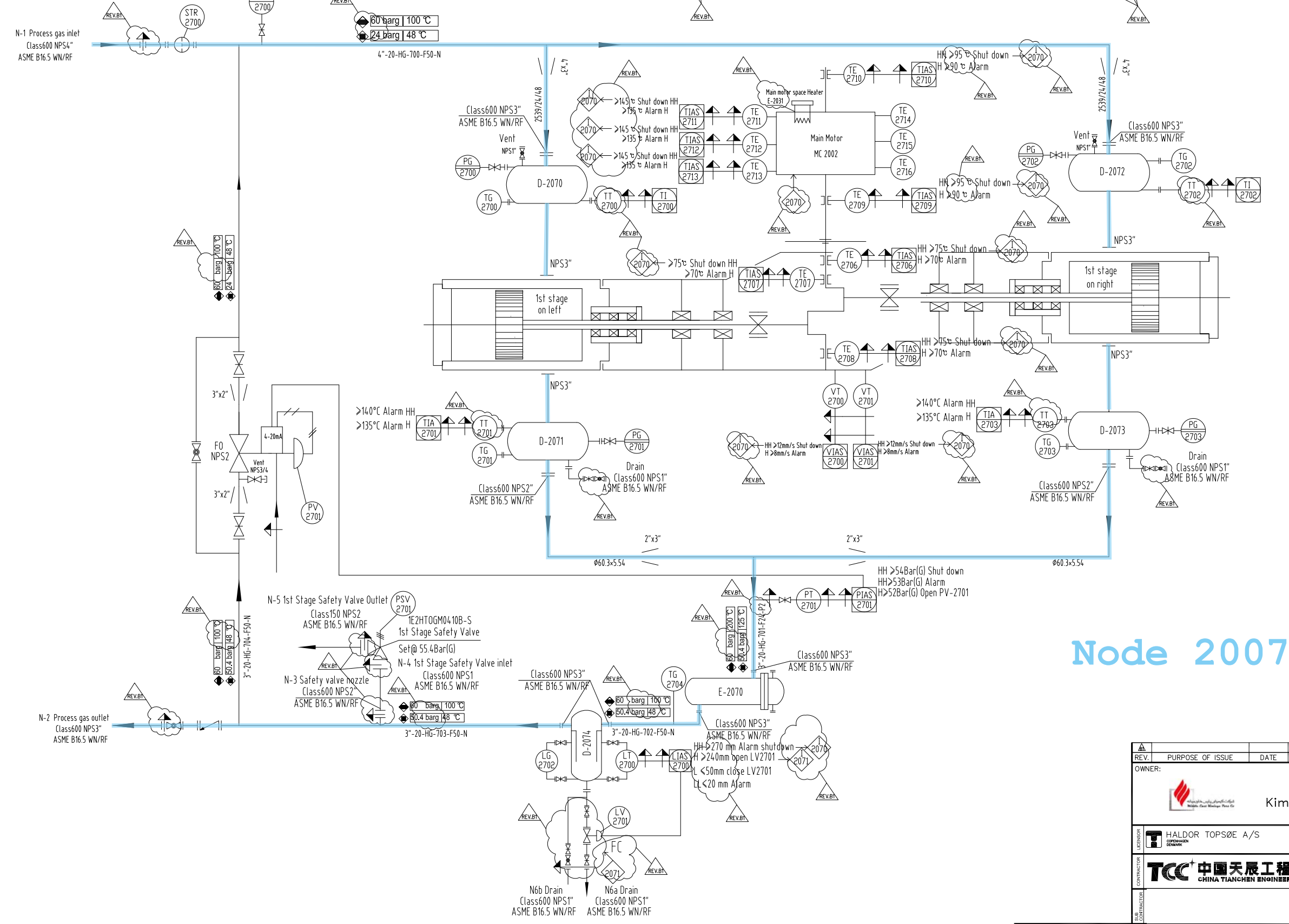
E-2070	After cooler
ID x LENGTH	28 x 3800 mm
Design Press. (shell/tube)	60 Barg / 10 Barg
Design Temp. (shell/tube)	200°C / 85°C
Insulation	Personnel Protection

E-2031	Main motor space Heater
Voltage	230 V
Power	0.6 Kw

MC 2002	Main motor
Voltage	6000 V
Power	200 Kw

### Legend

Symbol	Description
	Temporary Strainer
	Damper
	Cooler
	Separator
	Motor
	Safety Valve
	Gate Valve
	Globe Valve
	Ball Valve
	Control Valve
	Check Valve
	Needle Valve
	Field mounted
	Local gauge board
	PLC instrument
	Pipe
a/b/c	Flow/Pres./Temp. Nm/Bar(G)/°C
	Screwed Cap

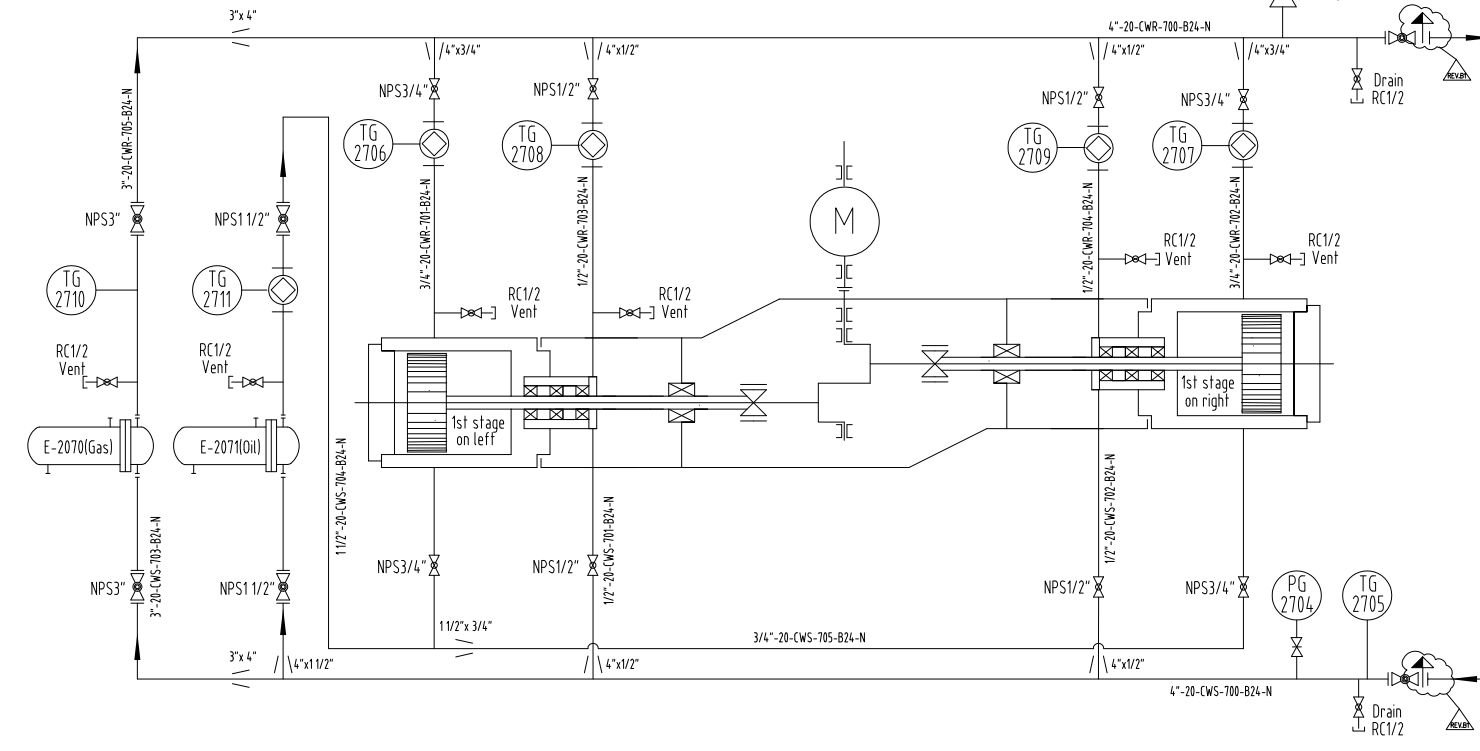
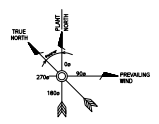


# Node 2007

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
OWNER:							
LICENSOR: HALDOR TOPSØE A/S							
CONTRACTOR:							
CONTRACTOR DRAWING NO.				SHEET TOTAL			
SUB-CONTRACTOR DRAWING NO.				SHEET 1 TOTAL 1			
PROJECT: MKP Methanol Project							
UNIT: REFORMER							
PHASE: DETAIL_ENGINEERING							
OWNER DWG NO. MKP-VD-9000-306-004-A1							

Drawing2.dwg

# Node 2007



**Legend**

Symbol	Description
	Sight glass
	Cooler
	Safety Valve
	Globe Valve
	Ball Valve
	Field mounted
	Local gauge board
	PLC instrument
	Water Pipe
	Screwed Cap

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

OWNER: Middle East Kimiaye Pars Company

DESIGNER: HALDOR TOPSØE A/S

CONTRACTOR DRAWING NO. \_\_\_\_\_

CONTRACTOR: TCC 中國天辰工程有限有限公司 CHINA TIANGEN ENGINEERING CORPORATION

SHEET	TOTAL
1	1

PROJECT: MKP Methanol Project

UNIT: REFORMER

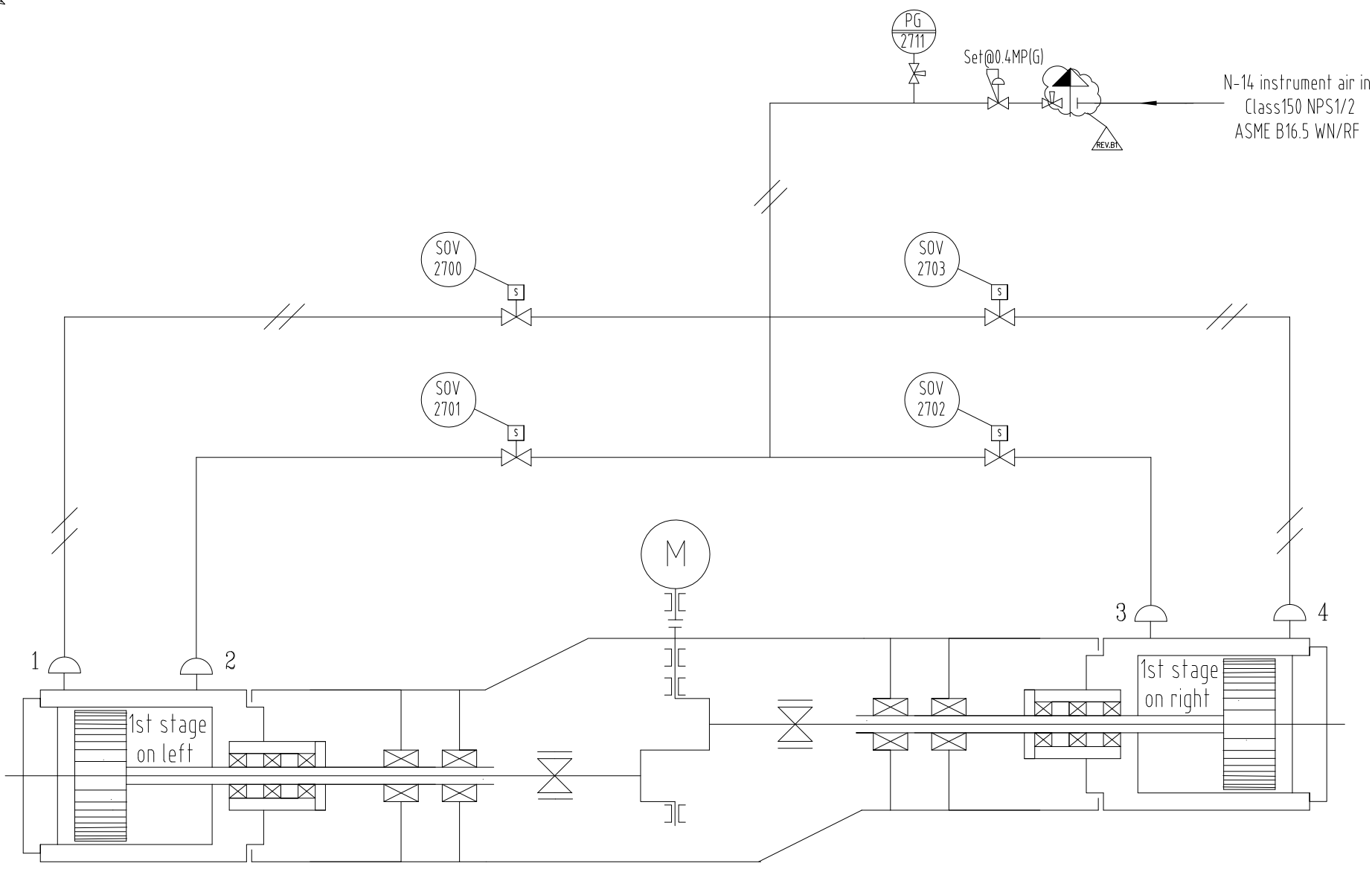
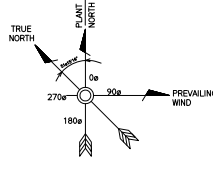
PHASE: DETAIL\_ENGINEERING

OWNER DWG NO. MKP-YD-9000-306-005-A1

SCALE	1:1
SHEET	1
TOT.	1
SIZE	1

Drawing2.dwg

# Node 2007



Legend

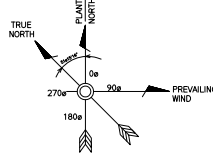
Symbol	Description
	Solenoid valve
	Motor
	Needle Valve
	Field mounted
	PLC instrument
	Pipe
	Unloader
	Regulator Valve

Scope Split  
 User Vendor

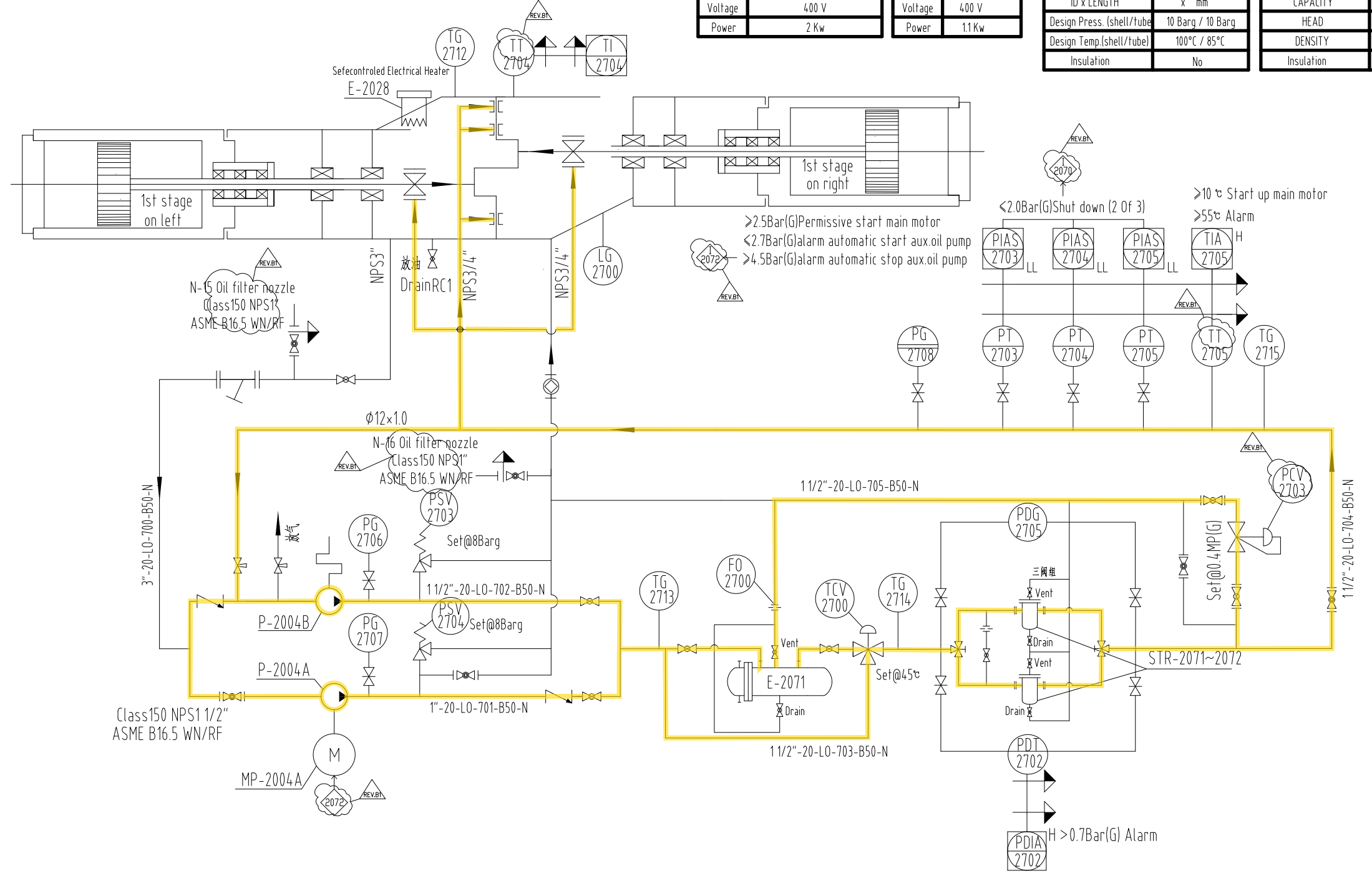
Stage	1st stage on left				1st stage on right				solenoid valve			
	HE-1	CE-2	HE-4	CE-3	SOV-2700	SOV-2701	SOV-2702	SOV-2703	SOV-2700	SOV-2701	SOV-2702	SOV-2703
0%	NA	NA	NA	NA	E	E	E	E	E	E	E	E
25%	NA	A	NA	NA	E	DE	E	E	E	DE	E	E
50%	NA	A	NA	A	E	DE	DE	E	DE	DE	DE	E
75%	NA	A	A	A	E	DE	DE	E	DE	DE	DE	DE
100%	A	A	A	A	DE	DE	DE	E	DE	DE	DE	DE

C-Close NA-No Acting HE-Head End DE-De Energized  
 O-Open A-Acting CE-Crank End E-Energized

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
OWNER:  Middle East Kimiaye Pars Company							
LEASER: HALDOR TOPSØE A/S							
CONTRACTOR:  TCC 中国天辰工程技术有限公司 CHINA TIANCHEN ENGINEERING CORPORATION							
CONTRACTOR DRAWING NO.				SHEET TOTAL			
SUB-CONTRACTOR DRAWING NO.				SHEET 1 TOTAL 1			
C 2002_H2 Recel compressor Unloading Control System P&ID				PROJECT: MKP Methanol Project		UNIT: REFORMER	
				PHASE: DETAIL_ENGINEERING			
SCALE 1:1 SHEET:1 TOT.:1 SIZE: A1				OWNER DWG NO. MKP-VD-9000-306-006-A1			



E-2028	Safecontrolled Electrical Heater	MP-2004A	Aux.Pump motor	E-2071	Oil cooler	R-2004A	Aux.Pump	P-2004B	Main Pump
Voltage	400 V	Voltage	400 V	ID x LENGTH	x mm	CAPACITY	m <sup>3</sup> /h	CAPACITY	m <sup>3</sup> /h
Power	2 Kw	Power	1.1 Kw	Design Press. (shell/tube)	10 Barg / 10 Barg	HEAD	m	HEAD	m
				Design Temp.(shell/tube)	100°C / 85°C	DENSITY	Kg/m <sup>3</sup>	DENSITY	Kg/m <sup>3</sup>
				Insulation	No	Insulation	No	Insulation	No



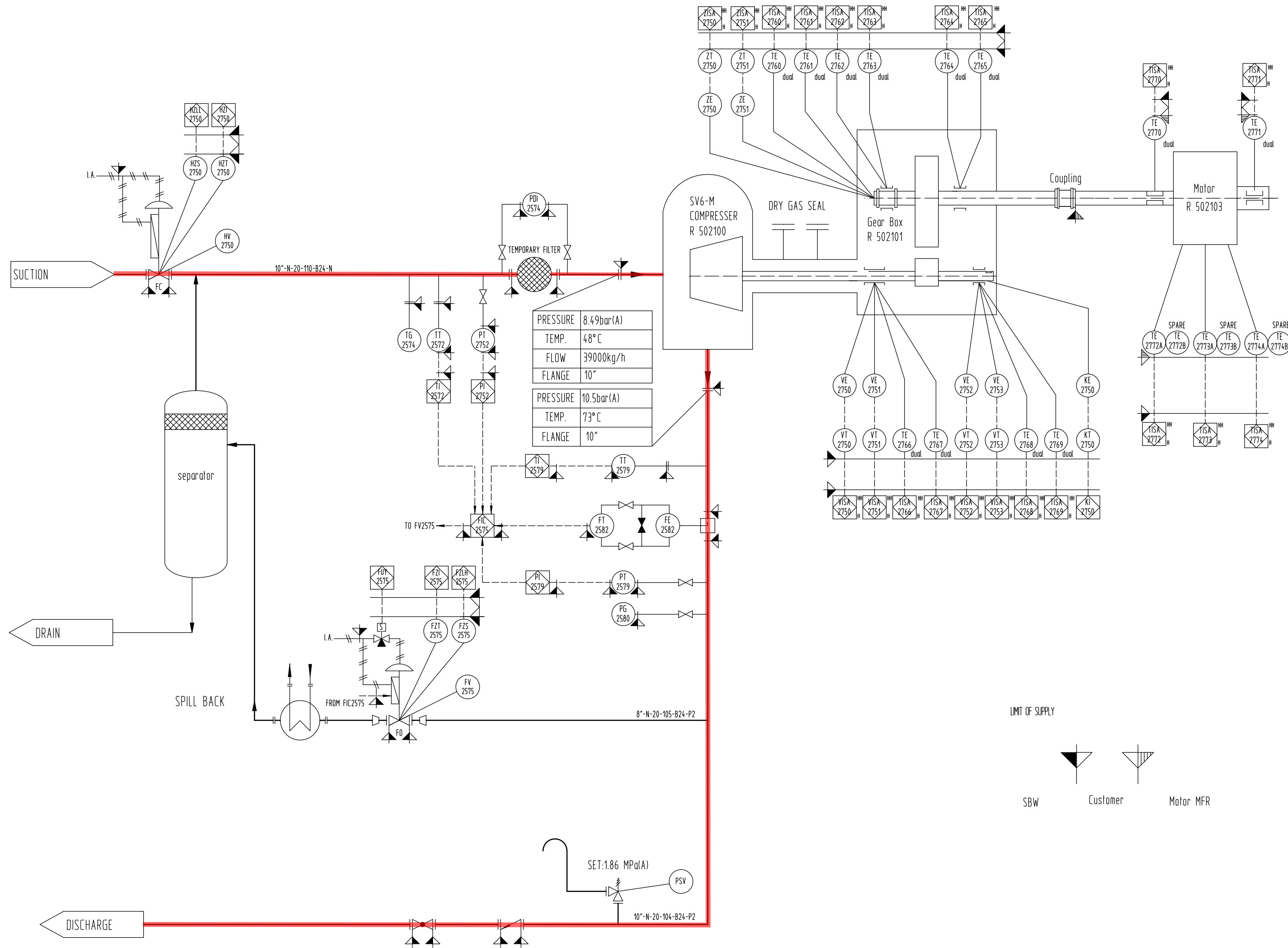
Symbol	Description
	Filter
	Main Pump
	Aux Pump
	Oil cooler
	Motor
	sight glass
	Regulator Valve
	Safety Valve
	Globe Valve
	Check Valve
	Ball Valve
	Needle Valve
	Field mounted
	Local gauge board
	PLC instrument
	Oil Pipe
	Orifice
	Y-Strainer
	Safecontrolled Electrical Heater
	3-Way valve

# Node 2007

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
OWNER:  Middle East Kimiaye Pars Company							
LESSOR: HALDOR TOPSØE A/S							
CONTRACTOR:  TCC 中国天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION							
CONTRACTOR DRAWING NO.							
SHEET TOTAL							
SUB-CONTRACTOR DRAWING NO.							
ZD6.5(Y95).00							
SHEET 1 TOTAL 1							
PROJECT: MKP Methanol Project							
UNIT: REFORMER							
PHASE: DETAIL_ENGINEERING							
OWNER DWG NO. MKP-VD-9000-306-007-A1							
SCALE 1:1 SHEET:1 TOT.:1 SIZE: A1							
Counter Signing	Sign	Date					



# Node 2008



## GENERAL NOTES

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

△	Issued For Review	15.2.2017	Han Yong	Zhang Siyuan	Qu Luon	00.10.0015	Tian Sheng
▲	Issued For Review	12.1.2017	Han Yong	Zhang Siyuan	Qu Luon	00.10.0015	Tian Sheng
REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

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OWNER:



Middle East  
Kimiyay Pars Company

CONTRACTOR:



CONTRACTOR DRAWING NO.  
MKP-11-DE-9000-MP86-REQ-008

VENDOR:



Shenyang Blower Works Group Co., LTD.

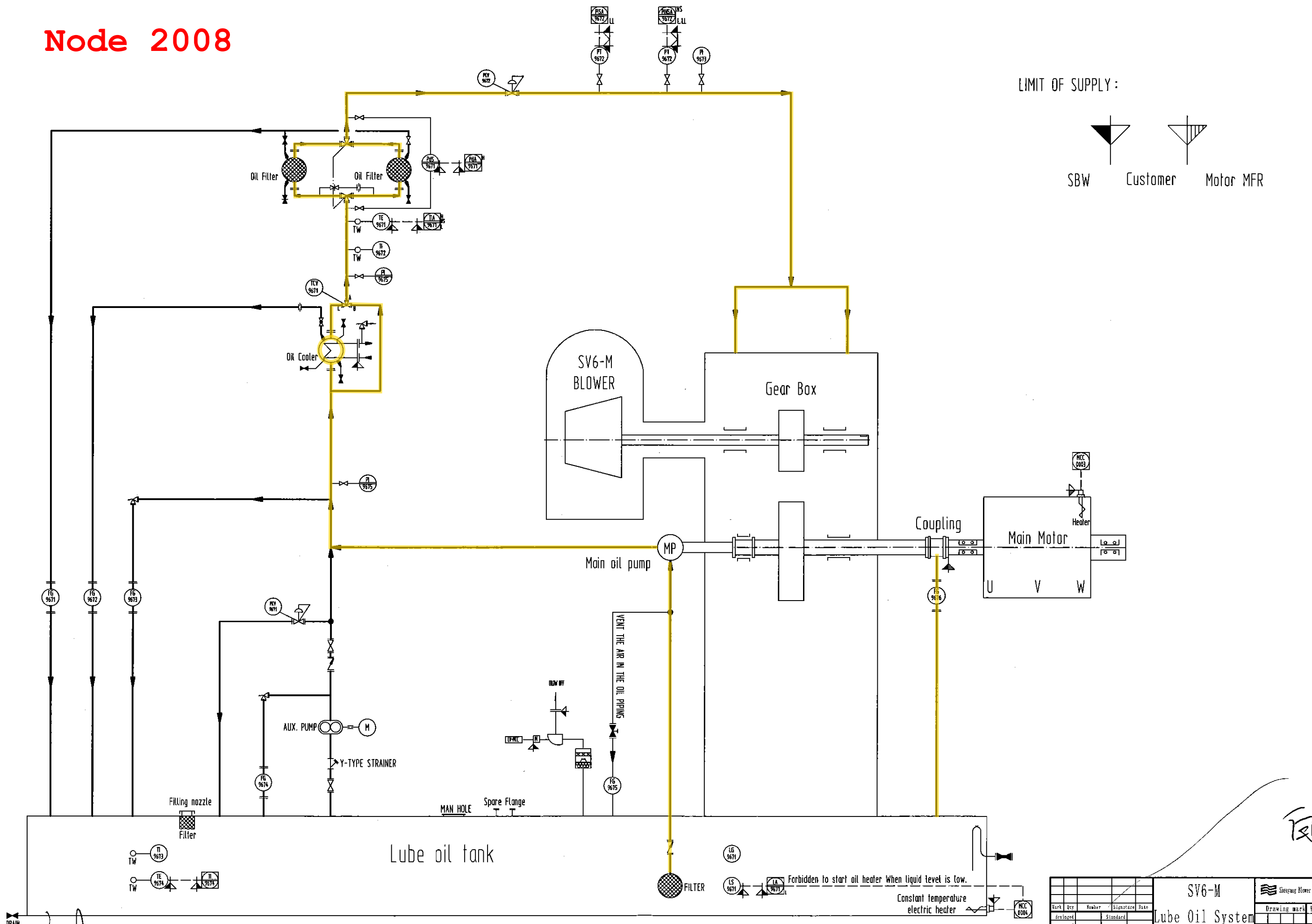
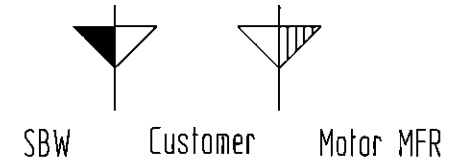
VENDOR DRAWING NO.  
MKP-VD-9000-308-060-A4

Item NO.:	C2001	PROJECT	MKP Methanol Project
Service:	Centrifugal Compressor	UNIT	General Technical
Document:	Gas system	PHASE	Detail Engineering
SCALE	SHEET	TOT.	SIZE
OWNER DWG NO.	MKP-11-DE-9000-RE-REQ-308		

Counter Signing	Spn	Date

# Node 2008

LIMIT OF SUPPLY :



Mark		Use	Number	Signature	Date
designed		Standard			
prepared		process			
reviewed		approved			
checked		Rev.			
revised					

SV6-M		Shenyang Blower Works Group Co., LTD.	
Lube Oil System		Drawing mark	Weight Scale
		Total 1 pages	1/1

Handwritten signature/initials.

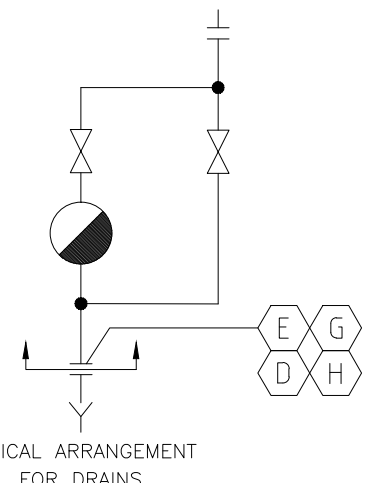
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# Node 2009

POS.	QTY.	DIMENSION	DESCRIPTION
A	1	DNL 6" RF ASME B16.5 600#	INLET STEAM
B	1	DNL 16" RF ASME B16.5 300#	EXHAUST STEAM
C	1	DNL 3" RF ASME B16.5 300#	DRAIN SHIRT ISOLATION
D	1	DNL 1" RF ASME B16.5 150#	CASING CONDENSATE DRAIN
E	1	DNL 1" RF ASME B16.5 150#	STEAM CHEST CONDENSATE DRAIN
F	1	DNL 1" RF ASME B16.5 150#	GOVERNOR VALVE AND TRIP VALVE STEAM DRAIN
G	1	DNL 1" RF ASME B16.5 150#	GOVERNOR VALVE BODY CONDENSATE DRAIN
H	1	DNL 1" RF ASME B16.5 150#	CASING CONDENSATE DRAIN
W	2	DNL HOLD 50 RF ASME B16.5 150#	OUTLET WATER COOLING
WT	2	DNL HOLD 50 RF ASME B16.5 150#	INLET WATER COOLING



## GENERAL NOTES

- 1 - VALVES SV-2801, SV-2802, SV-2803 AND SV-2804 FORM A SINGLE MANIFOLD BLOCK;
- 2 - VALVES HV-2803 AND SV-2805 FORM A SINGLE MANIFOLD BLOCK;
- 3 - CONNECTIONS D, E, G, H, SHOULD BE DRAINED TO AN ATMOSPHERIC COLLECTOR (PIPING) SUPPLIED BY CLIENT.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
Δ	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC

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OWNER:

Middle East  
Kimiaye Pars Company

CONTRACTOR:

TCC 中国天辰工程有限公司  
CHINA TIANCHEN ENGINEERING CORPORATION

CLIENT:

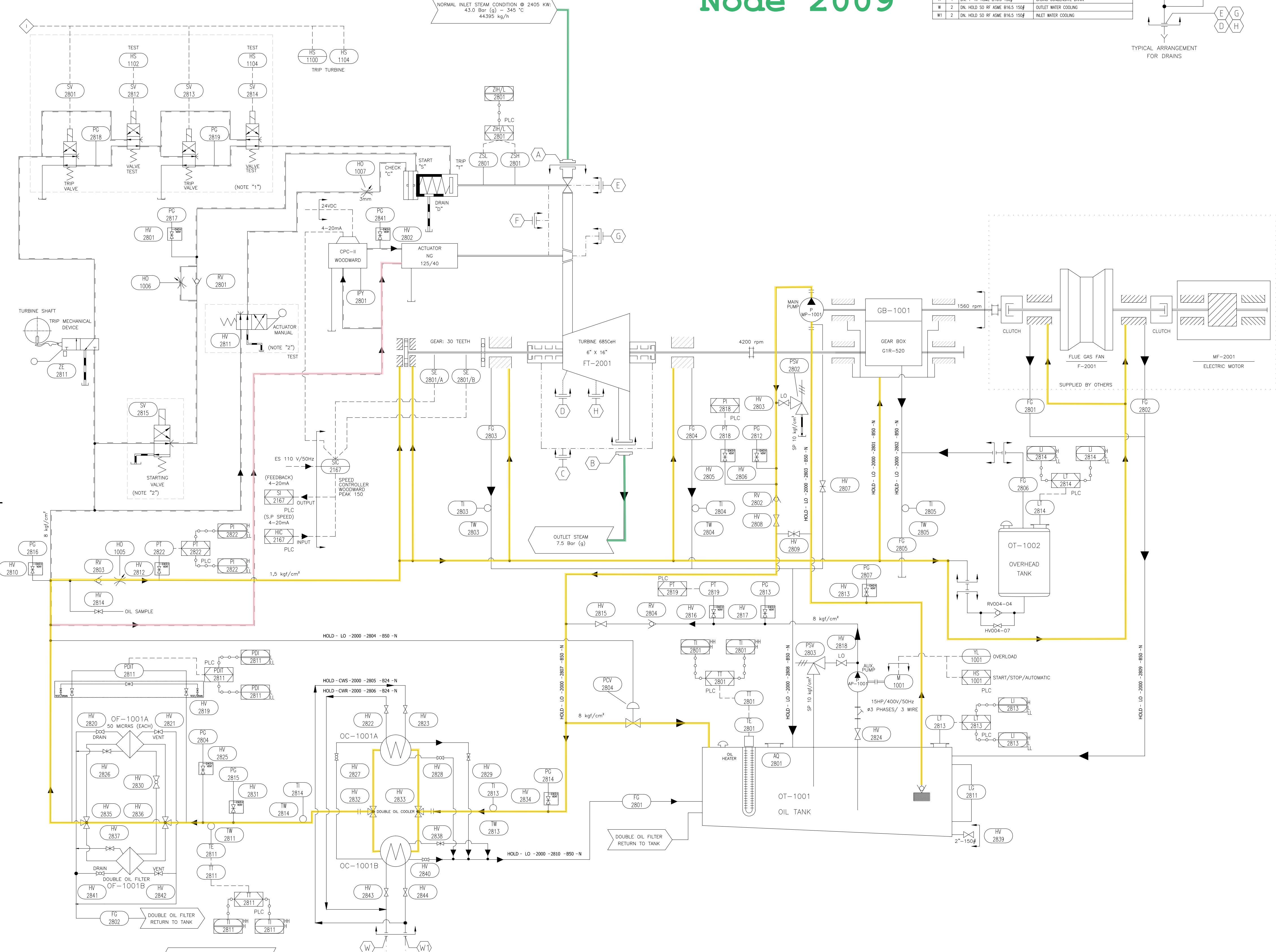
I.T.T. SpA - Milano - Italy

VENDOR DRAWING NO.  
15104B-VND-22-608\_16

PROCESS INSTRUMENTATION DIAGRAM  
TURBINE: 685 CcH  
TAG: FT-2001  
CUSTOMER: MKP - IRAN

PROJECT: MKP Methanol Project  
UNIT: PRIMARY REFORMER PACKAGE (H 2001)  
PHASE: DETAIL ENGINEERING  
OWNER DWG NO: MKP-VD-2000-351-145-A1

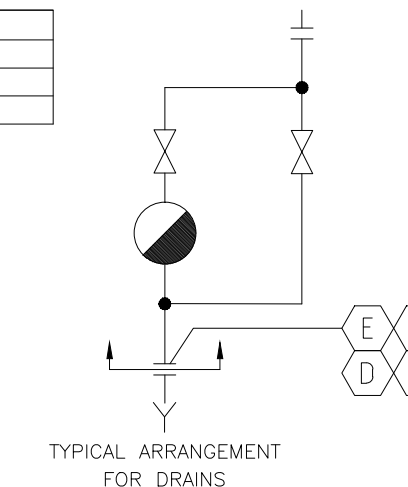
Counter Signing	Sign	Date
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DE-415671-004.00-REV.A - FL.0030.dwg

# Node 2009

POS.	QTY.	DIMENSION	DESCRIPTION
W3	1	DN. HOLD 50 RF ASME B16.5 150#	OUTLET WATER CONDENSER
W4	1	DN. HOLD 50 RF ASME B16.5 150#	INLET WATER CONDENSER



## GENERAL NOTES

1 - USV-2801 TO SUPPLIED BY ITT.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
1	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC

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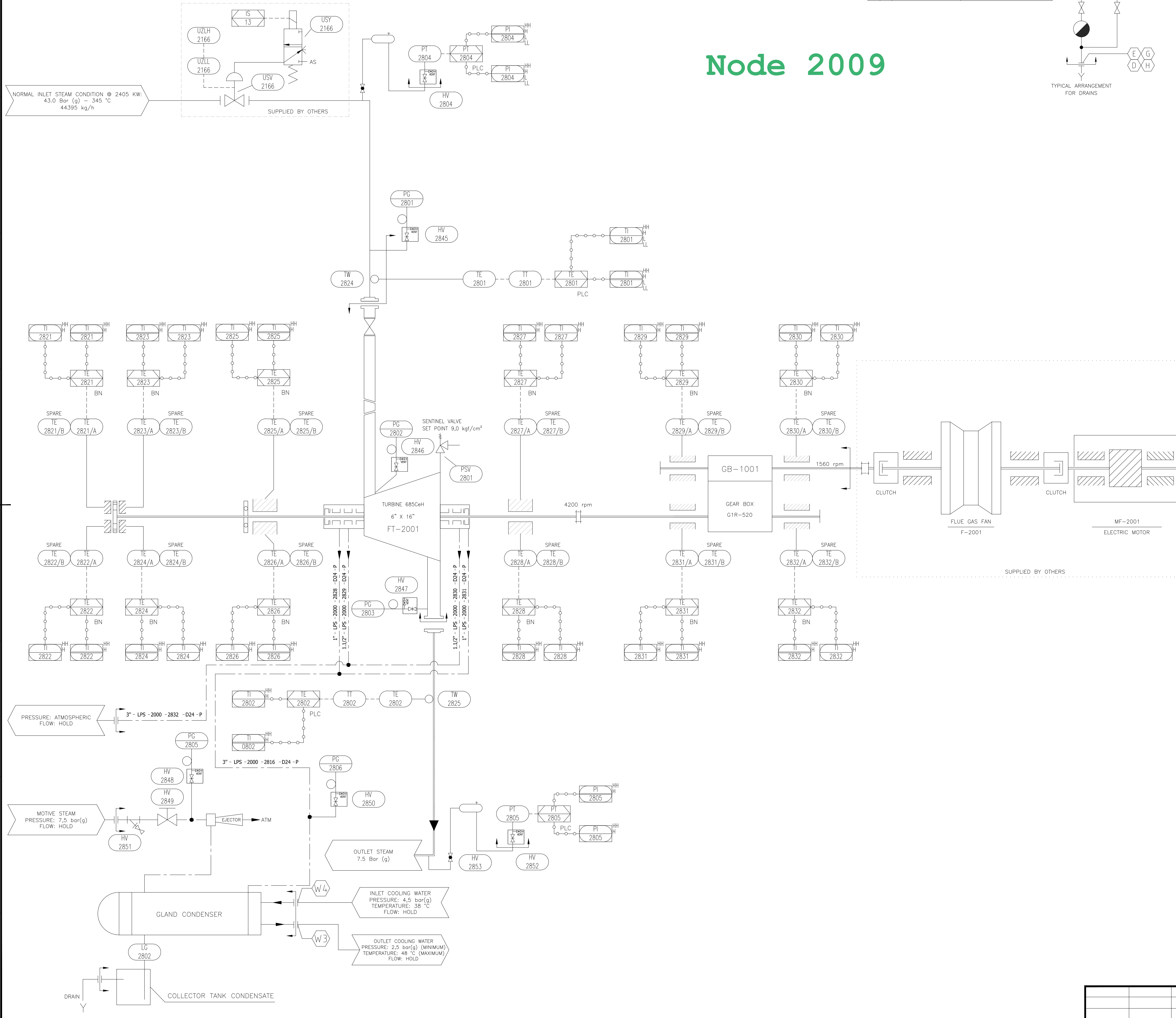
HALDOR TOPSØE A/S  
CORPORATION  
DENMARK

CONTRACTOR: **TCC** 中国天辰工程有限公司  
CHINA TIANCHEN ENGINEERING CORPORATION

I.T.T. SpA - Milano - Italy

VENDOR DRAWING NO.  
15104B-VND-22-608\_16

PROCESS INSTRUMENTATION DIAGRAM TURBINE: 685 CcH TAG: FT-2001 CUSTOMER: MKP - IRAN	PROJECT MKP Methanol Project
UNIT PRIMARY REFORMER PACKAGE (H 2001)	PHASE DETAIL ENGINEERING
SCALE N/S SHEET 04 TOT. 05 SIZE A1	OWNER MKP-VD-2000-351-145-A1

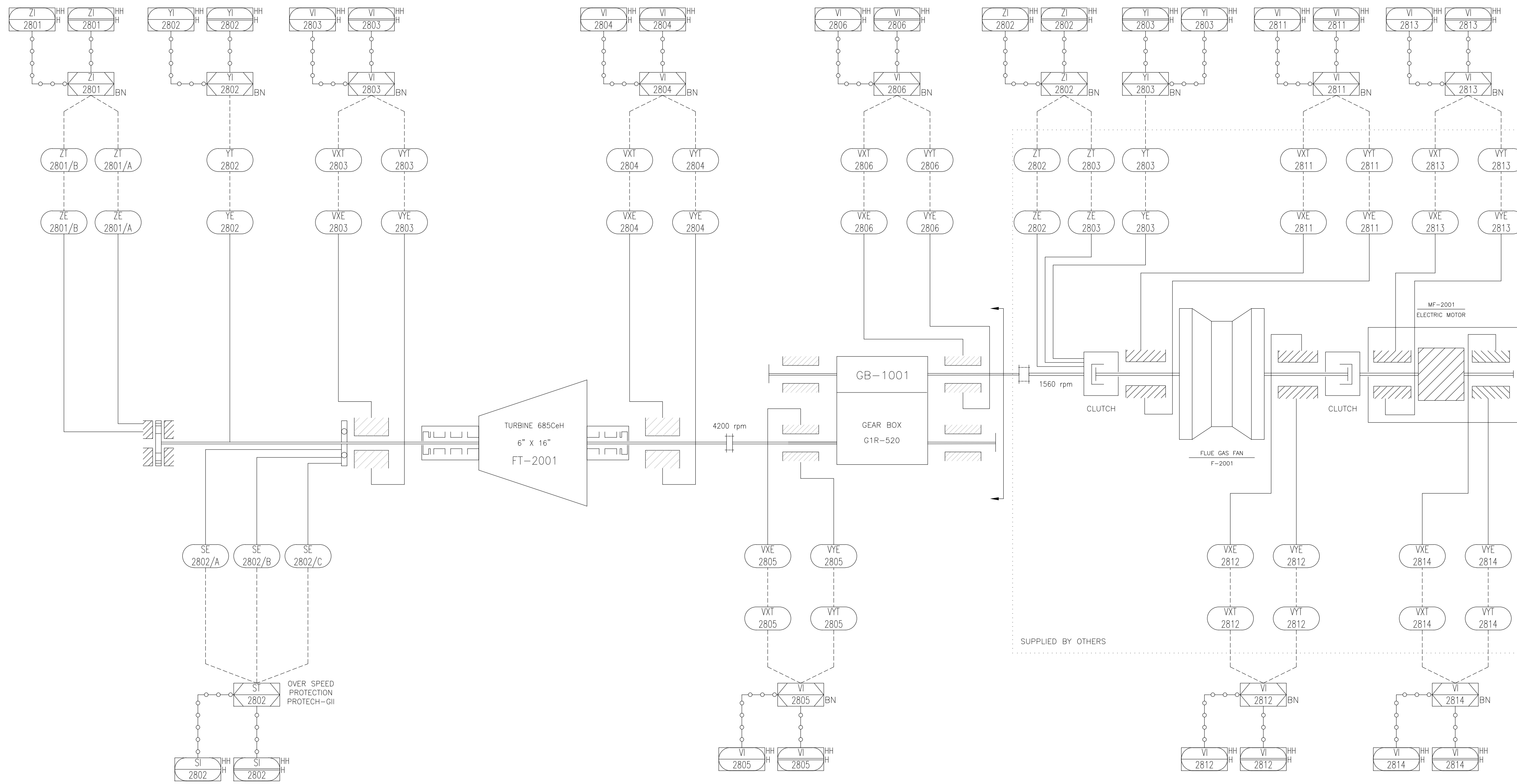


DE-415671-004.00-REV.A - FL.0040.dwg

Counter	Sign	Date



# Node 2009



## GENERAL NOTES

- 1 - FOR BENTLY NEVADA TAG USE BN-2816.
- 2 - FOR TRIP FAN TO PCS/ESD TAG USE USY-2802.
- 3 - FOR TRIP ELECTRIC MOTOR TO PCS/ESD TAG USE USY-2803.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
1	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC

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LICENSEE: HALDOR TOPSØE A/S

CONTRACTOR: **TCC** 中国天辰工程有限公司  
CHINA TIANCHEN ENGINEERING CORPORATION

I.T.T. SpA - Milano - Italy

VENDOR DRAWING NO.  
15104B-VND-22-608\_16

PROJECT	MKP Methanol Project
UNIT	PRIMARY REFORMER PACKAGE (H 2001)
PHASE	DETAIL ENGINEERING
OWNER DWG NO.	MKP-VD-2000-351-145-A1

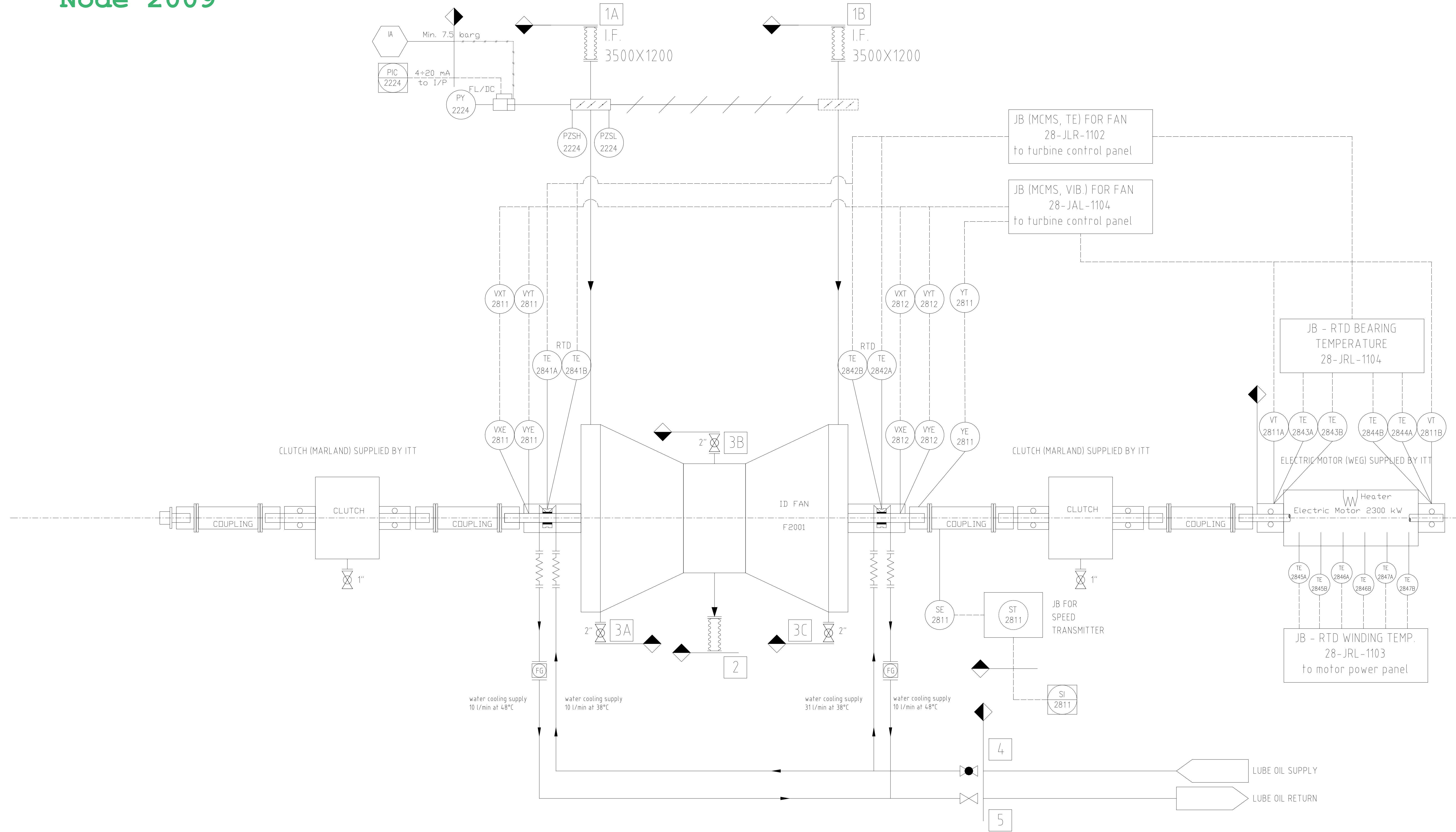
Counter	Sign	Date

SCALE	N/S	SHEET	05	TOT.	05	SIZE	A1
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DE-415671-004.00-REV.A - FL.0050.dwg

# Node 2009

## GENERAL NOTES

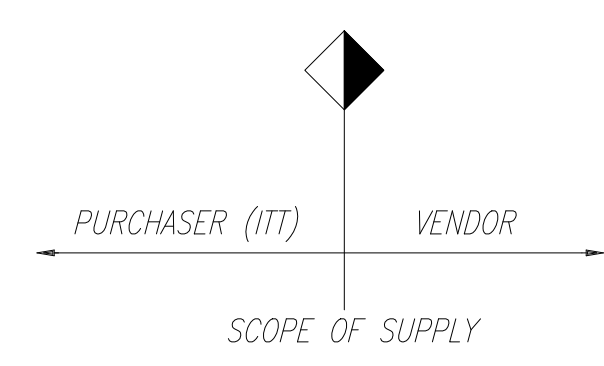


**LEGENDA**

	Mechanical Link		Flexible Pipe for Adjustments
	Water Cooling Line		Flow Glass
	Pneumatic Signal Line		Field Instrument
	Oil Piping		Main Control Room Instrument
	Steam Piping		Remote/Local Panel - Mounted Instrument
	Instrument Capillary Tubing		DCS by Customer
	Softwire Link		Interlock in Customer ESD
	Electrical Signal Lead		
	Ball Valve		
	Globe Valve		
	Gate Valve		
	Check Valve		
	Safety Valve		

A) ALL OIL PIPING STAINLESS STEEL AISI 316L 304/3040  
B) ALL TUBING AND FITTINGS STAINLESS STEEL AISI 317L

SE = SPEED PROBE  
VXE = VIBRATION SENSOR AXIS X  
VYE = VIBRATION SENSOR AXIS Y  
YE = KEY PHASOR SENSOR  
VT = VELOMITOR SENSOR



**LIST OF CONNECTION**

POS	SIZE	RATING	SERVICE
1A-1B	I.F. 3500 x 1200	-	INLET COUNTERFLANGE
2	I.F. 2078 x 2514	-	OUTLET COUNTERFLANGE
3A-3B-3C	2"	#150 RF	HOUSING DRAIN
4	1" 1/2	#150 RF	INLET WATER COOLED
5	1" 1/2	#150 RF	OUTLET WATER COOLED

REV.	Issued For Comments	26.07.2016	C.V.	C.V.	N.2	M.C.	G.F.A.
	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

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Kimiaye Pars Company

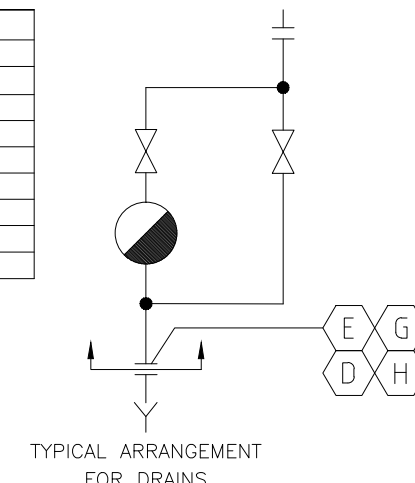
HALDOR TOPSØE A/S  
TCC 中国天辰工程有限公司  
I.T.T. SpA - Milano - Italy

PROJECT	MKF Methanol Project
UNIT	PRIMARY REFORMER
PHASE	DETAIL ENGINEERING
SCALE	1:50
SHEET	01
TOT.	01
SIZE	A0
OWNER DWG NO.	MKP-VD-2000-351-302-A0

Counter	Sign	Date
---------	------	------

# Node 2010

POS.	QTY.	DIMENSION	DESCRIPTION
A	1	DN 5" RTJ ASME B16.5 900F	INLET STEAM
B	1	DN 10" RTJ ASME B16.5 300F	EXHAUST STEAM
E	1	DN 1/2" RTJ ASME B16.5 150F	CONDENSATE CHEST DRAIN
F	1	DN 1" RTJ ASME B16.5 150F	INLET VALVE STEM DRAIN
G	1	DN 3/4" RTJ ASME B16.5 150F	CASING DRAIN
T	1	DN 1.5" RTJ ASME B16.5 300F	DRAIN SHUT SEALING
U	2	DN HOLD RTJ ASME B16.5 150F	OUTLET WATER COOLING
V	2	DN HOLD RTJ ASME B16.5 150F	INLET WATER COOLING



## GENERAL NOTES

1 - CONNECTIONS E, G, SHOULD BE DRAINED TO AN ATMOSPHERIC COLLECTOR (PIPING) SUPPLIED BY CLIENT.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
Δ	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC

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OWNER:

Middle East  
Kimiaye Pars Company

CONTRACTOR:

TCC 中国天辰工程有限公司  
CHINA TIANCHEN ENGINEERING CORPORATION

OWNER:

I.T.T. SpA - Milano - Italy

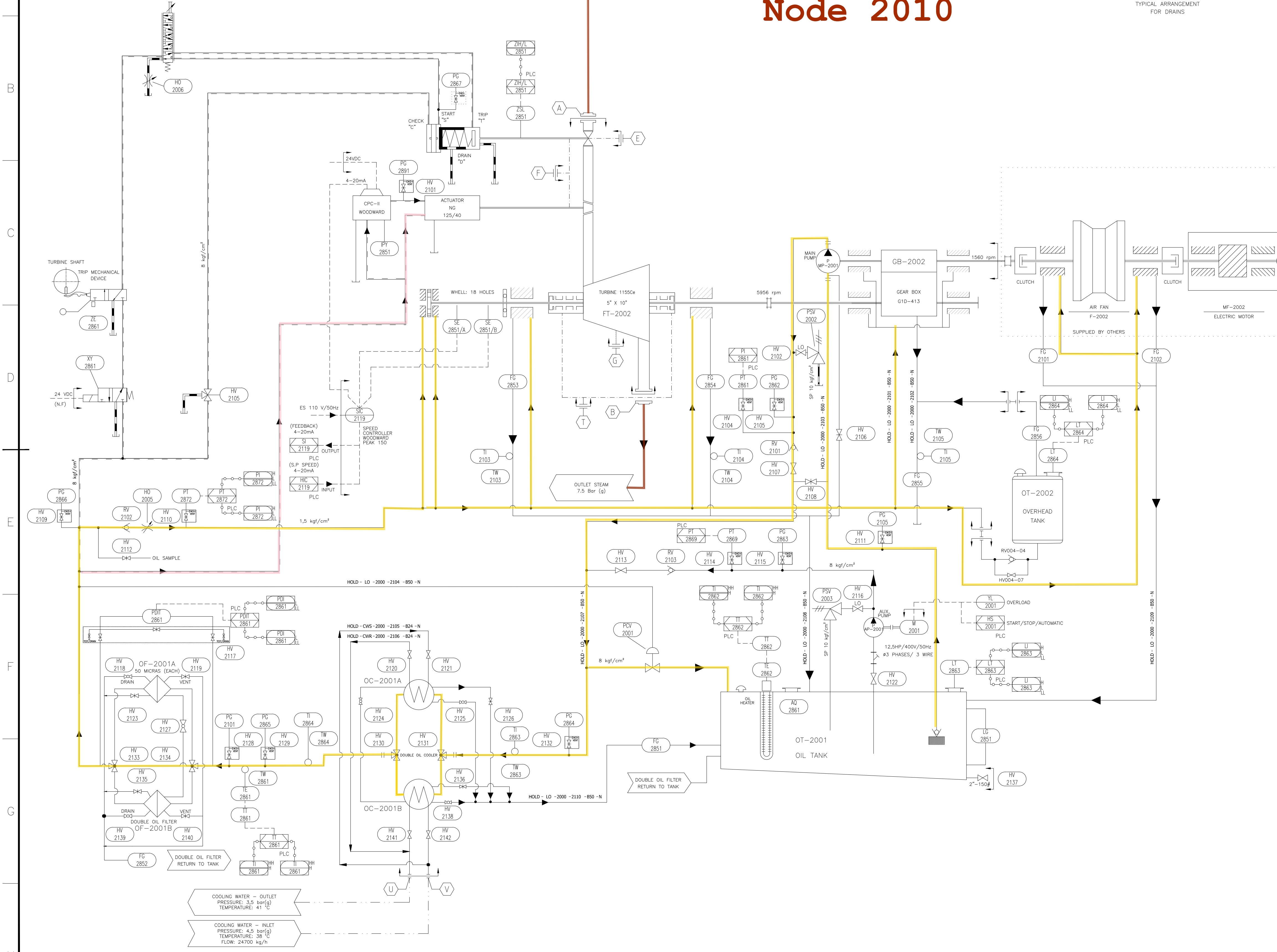
VENDOR DRAWING NO.  
15104B-VND-22-607\_16

PROCESS INSTRUMENTATION DIAGRAM  
TURBINE: 1155 Ce  
TAG: FT-2002  
CUSTOMER: MKP - IRAN

PROJECT: MKP Methanol Project  
UNIT: PRIMARY REFORMER PACKAGE (H 2001)  
PHASE: DETAIL ENGINEERING

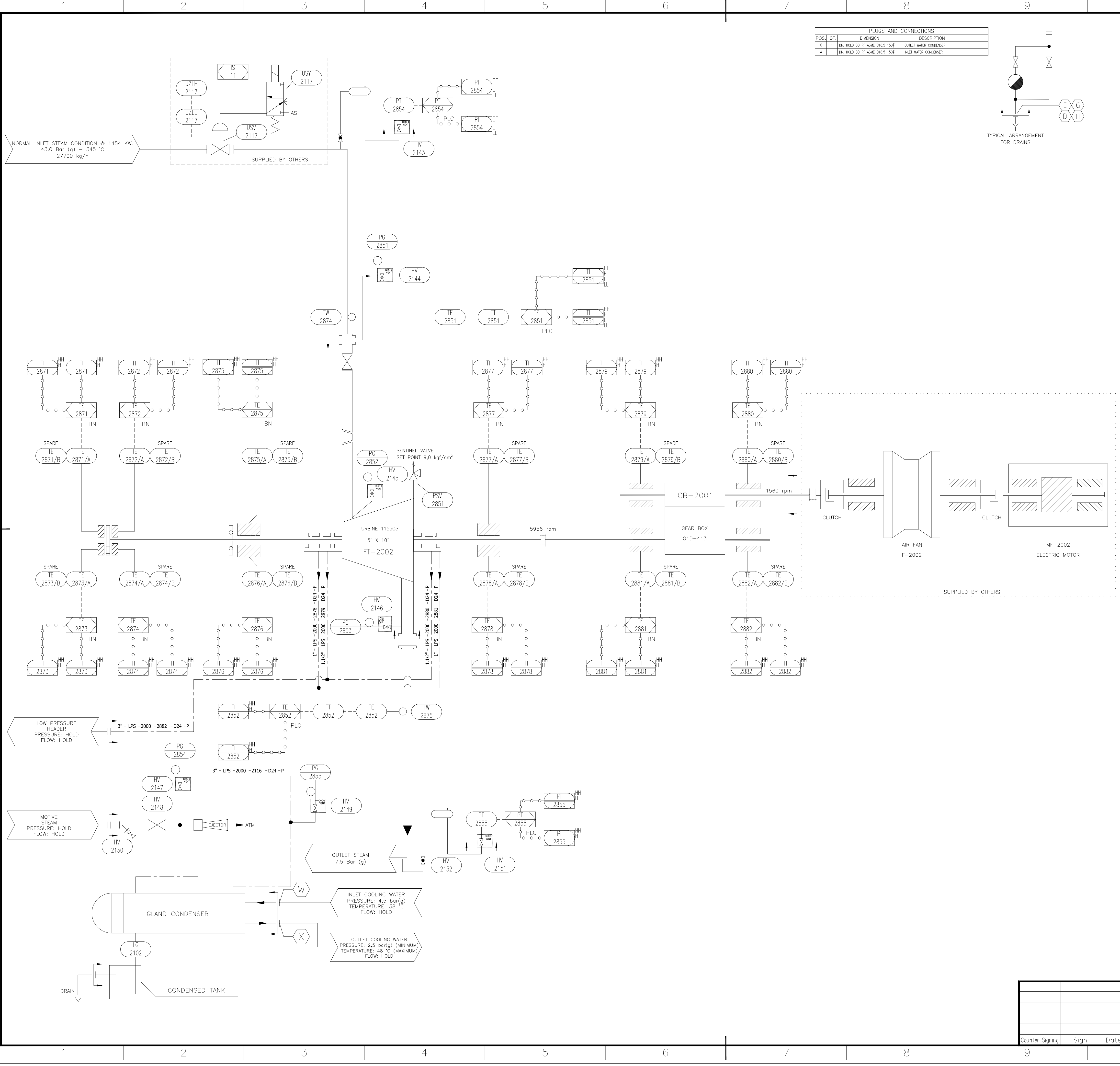
SCALE N/S SHEET 03 TOT. 05 SIZE A1  
COUNTER SIGNING Sign Date

OWNER DWG NO. MKP-VD-2000-351-120-A1

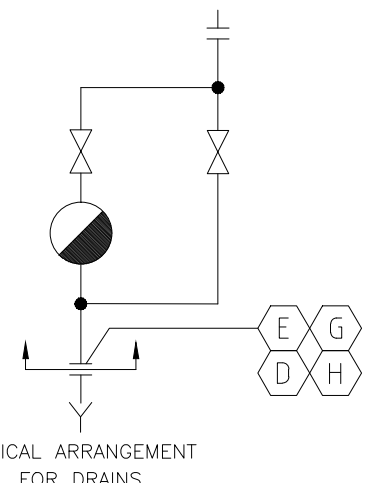


DE-415675-004.00-REV.A - FL0030.dwg





POS.	QTY.	DIMENSION	DESCRIPTION
X	1	DN. HOLD 50 RF ASME B16.5 150#	OUTLET WATER CONDENSER
W	1	DN. HOLD 50 RF ASME B16.5 150#	INLET WATER CONDENSER



**GENERAL NOTES**

1 - USV-2101 TO SUPPLIED BY ITT.

**REFERENCE DRAWINGS**

**SYMBOLS AND LEGENDS**

**KEY PLAN**

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
1	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC

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OWNER:  
**Middle East  
 Kimiaye Pars Company**

CONTRACTOR:  
**TCC 中国天辰工程有限公司  
 CHINA TIANCHEN ENGINEERING CORPORATION**

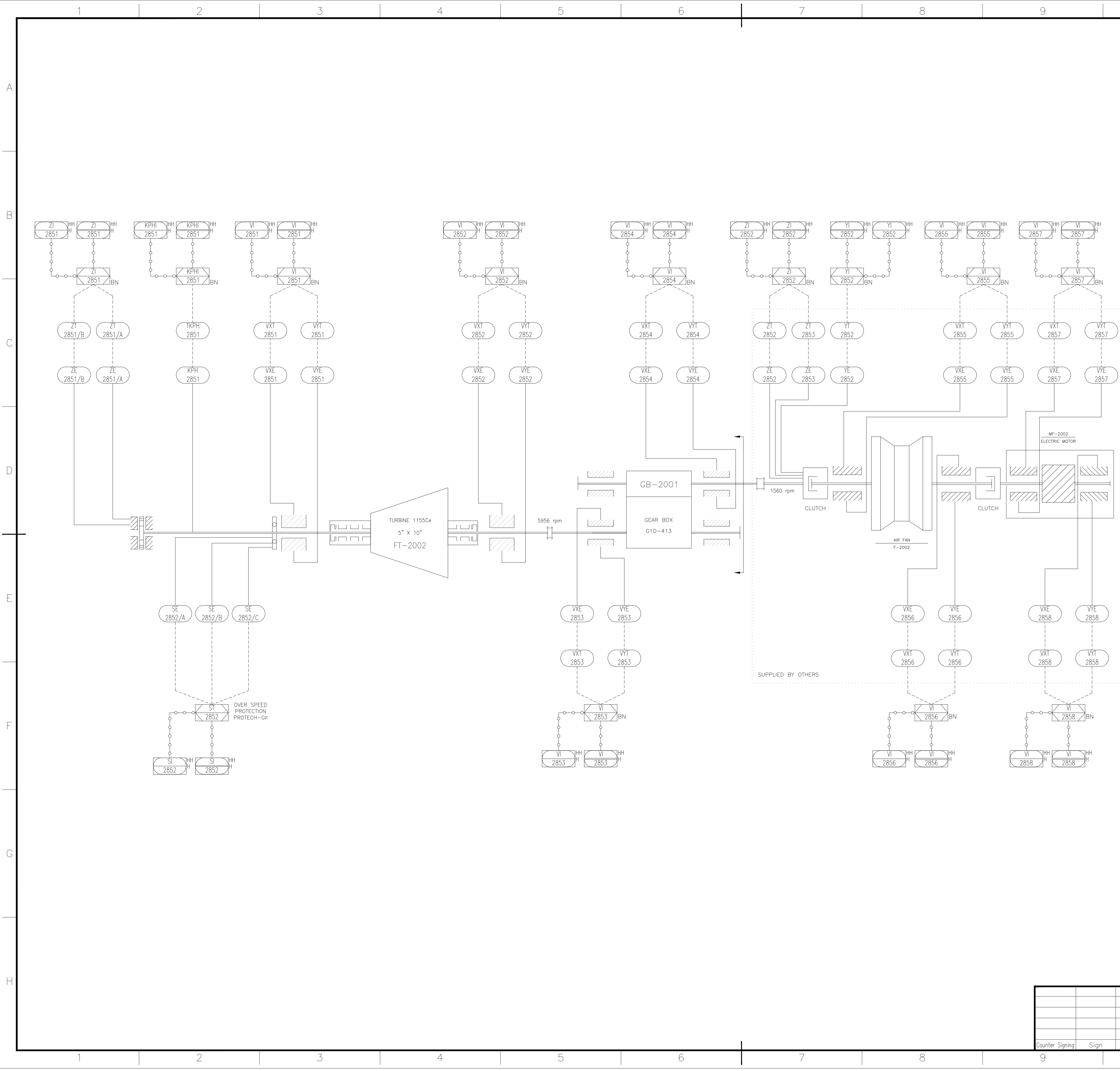
CLIENT:  
**I.T.T. SpA - Milano - Italy**

VENDOR DRAWING NO.  
 15104B-VND-22-607\_16

PROJECT	MKP Methanol Project
UNIT	PRIMARY REFORMER PACKAGE (H 2001)
PHASE	DETAIL ENGINEERING
OWNER DWG NO.	MKP-VD-2000-351-120-A1

SCALE	N/S
SHEET	04
TOT.	05
SIZE	A1

DE-415675-004.00-REV.A - FL.0040.dwg



**GENERAL NOTES**

- 1 - FOR BENTLY NEVADA TAG USE BN-2116.
- 2 - FOR TRIP FAN TO PCS/ESD TAG USE USY-2102.
- 3 - FOR TRIP ELECTRIC MOTOR TO PCS/ESD TAG USE USY-2103.

**REFERENCE DRAWINGS**


**SYMBOLS AND LEGENDS**

**KEY PLAN**

△	Issued For Comments	09.12.2016	ADTC	ADTC	ADCF	ADCF	HCC
REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

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OWNER:


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**Kimiaye Pars Company**


**HALDOR TOPSØE A/S**  
COPENHAGEN DENMARK


**TCC 中国天辰工程技术有限公司**  
CHINA TIANCHEN ENGINEERING CORPORATION

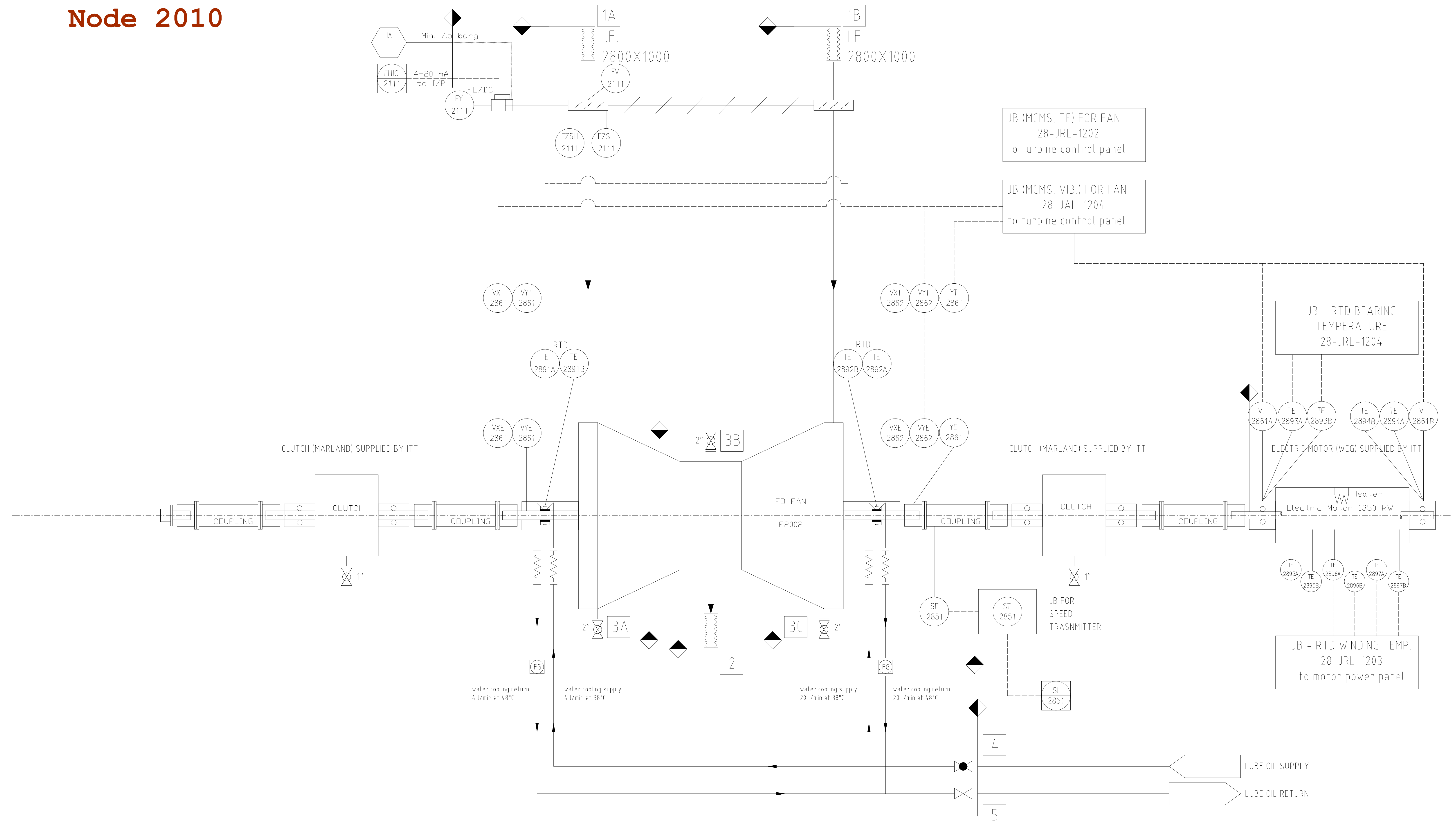

**I.T.T. SpA - Milano - Italy**

PROCESS INSTRUMENTATION DIAGRAM TURBINE: 1155 Ce TAG: FT-2002 CUSTOMER: MKP - IRAN		PROJECT MKP Methanol Project
UNIT PRIMARY REFORMER PACKAGE (H 2001)		PHASE DETAIL ENGINEERING
SCALE N/S SHEET 05 TOT. 05 SIZE A1	VENDOR DRAWING NO. 15104B-VND-22-607_16 OWNER MKP-VD-2000-351-120-A1	

DE-415675-004.00-REV.A - FL.0050.dwg



# Node 2010



## GENERAL NOTES

REV.	Issued For Comments	26.07.2016	C.V.	C.V.	N.2	M.C.	G.F.A.
	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

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OWNER: Middle East  
Kimiaye Pars Company

DESIGNER	HALDOR TOPSØE A/S		
OWNER	<b>TCC</b> 中国天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION		
DESIGNER	I.T.T. SpA - Milano - Italy	VENDOR DRAWING NO.	15104B-PID-002

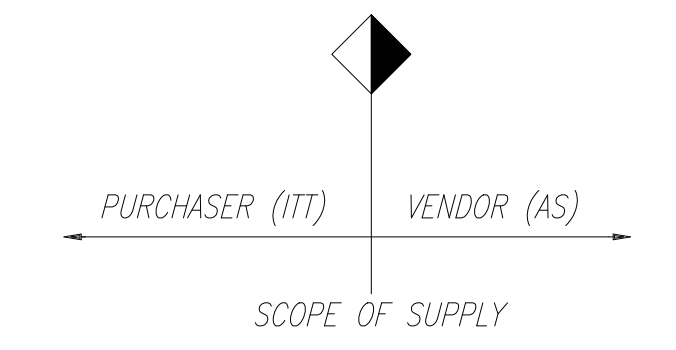
PROJECT	MIP Methanol Project
UNIT	PRIMARY_REFORMER
PHASE	DETAIL ENGINEERING
OWNER	MKP-V0-2000-351-303-A0

SCALE 1:50 SHEET 01 TOT. 01 SIZE A0

### LEGENDA

	MECHANICAL LINK		FLEXIBLE PIPE FOR ADJUSTMENTS
	WATER COOLING LINE		FLOW GLASS
	PNEUMATIC SIGNAL LINE		FIELD INSTRUMENT
	OIL PIPING		MAIN CONTROL ROOM INSTRUMENT
	STEAM PIPING		REMOTE/LOCAL PANEL - MOUNTED INSTRUMENT
	INSTRUMENT CAPILLARY TUBING		DCS BY CUSTOMER
	SOFTWARE LINK		INTERLOCK IN CUSTOMER ESD
	ELECTRICAL SIGNAL LEAD		

SE = SPEED PROBE  
VXE = VIBRATION SENSOR AXIS X  
VYE = VIBRATION SENSOR AXIS Y  
YE = KEY PHASOR SENSOR  
VT = VELOMITOR SENSOR



### LIST OF CONNECTION

POS	SIZE	RATING	SERVICE
1A-1B	I.F. 2800 x 1000	-	INLET COUNTERFLANGE
2	I.F. 2278 x 1878	-	OUTLET COUNTERFLANGE
3A-3B-3C	2"	#150 RF	HOUSING DRAIN
4	1" 1/2	#150 RF	INLET WATER COOLED
5	1" 1/2	#150 RF	OUTLET WATER COOLED

# Node 3006

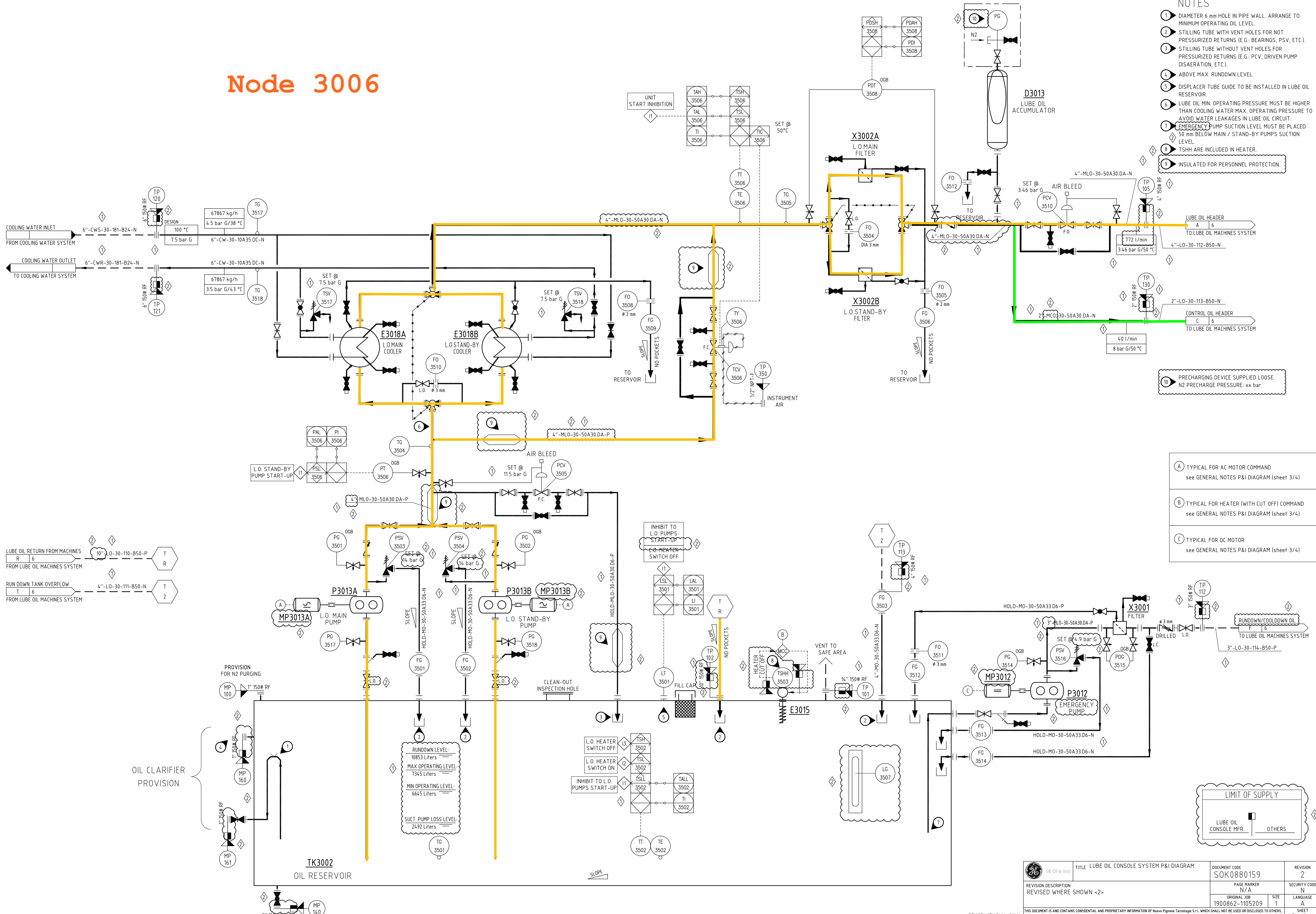
## NOTES

- 1 DIAMETER 6 mm HOLE IN PIPE WALL. ARRANGE TO MINIMUM OPERATING OIL LEVEL.
- 2 STILLING TUBE WITH VENT HOLES FOR NOT PRESSURIZED RETURNS (E.G.: BEARINGS, PSV, ETC.).
- 3 STILLING TUBE WITHOUT VENT HOLES FOR PRESSURIZED RETURNS (E.G.: PCV, DRIVEN PUMP DISAERATION, ETC.).
- 4 ABOVE MAX. RUNDOWN LEVEL.
- 5 DISPLACER TUBE GUIDE TO BE INSTALLED IN LUBE OIL RESERVOIR.
- 6 LUBE OIL MIN. OPERATING PRESSURE MUST BE HIGHER THAN COOLING WATER MAX. OPERATING PRESSURE TO AVOID WATER LEAKAGES IN LUBE OIL CIRCUIT.
- 7 EMERGENCY PUMP SUCTION LEVEL MUST BE PLACED 50 mm BELOW MAIN / STAND-BY PUMPS SUCTION LEVEL.
- 8 TSHH ARE INCLUDED IN HEATER.
- 9 INSULATED FOR PERSONNEL PROTECTION.

10 PRECHARGING DEVICE SUPPLIED LOOSE.  
N2 PRECHARGE PRESSURE: xx bar

- (A) TYPICAL FOR AC MOTOR COMMAND  
see GENERAL NOTES P&I DIAGRAM (sheet 3/4)
- (B) TYPICAL FOR HEATER (WITH CUT OFF) COMMAND  
see GENERAL NOTES P&I DIAGRAM (sheet 3/4)
- (C) TYPICAL FOR DC MOTOR  
see GENERAL NOTES P&I DIAGRAM (sheet 3/4)

LIMIT OF SUPPLY  
LUBE OIL \_\_\_\_\_  
CONSOLE MFR. \_\_\_\_\_ OTHERS \_\_\_\_\_



	TITLE	LUBE OIL CONSOLE SYSTEM P&I DIAGRAM	DOCUMENT CODE	SOK0880159	REVISION	2
	REVISION DESCRIPTION	REVISED WHERE SHOWN -2-	PAGE MARKER	N/A	SECURITY CODE	N
	ORIGINAL JOB	1900862-1105209	SIZE	1	LANGUAGE	A
					SHEET	5 of 14

REVISE WITH PIDX ONLY



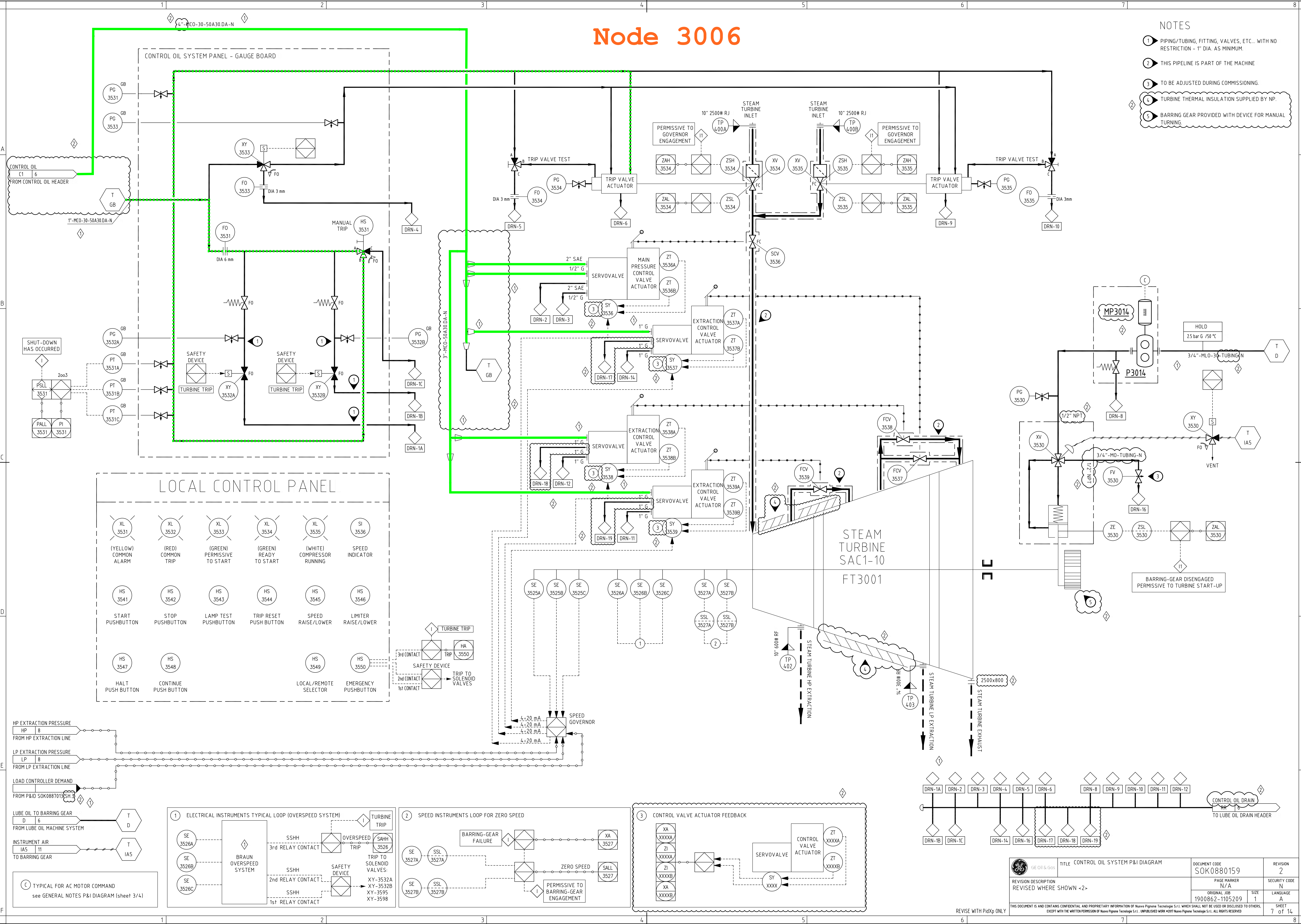




# Node 3006

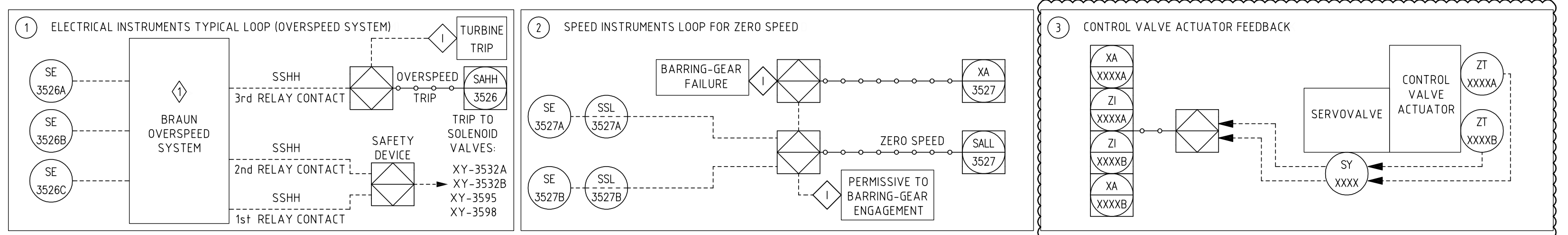
## NOTES

- 1 PIPING/TUBING, FITTING, VALVES, ETC... WITH NO RESTRICTION - 1" DIA. AS MINIMUM.
- 2 THIS PIPELINE IS PART OF THE MACHINE
- 3 TO BE ADJUSTED DURING COMMISSIONING.
- 4 TURBINE THERMAL INSULATION SUPPLIED BY NP.
- 5 BARRING GEAR PROVIDED WITH DEVICE FOR MANUAL TURNING.



### LOCAL CONTROL PANEL

XL 3531 (YELLOW) COMMON ALARM	XL 3532 (RED) COMMON TRIP	XL 3533 (GREEN) PERMISSIVE TO START	XL 3534 (GREEN) READY TO START	XL 3535 (WHITE) COMPRESSOR RUNNING	SI 3536 SPEED INDICATOR
HS 3541 START PUSHBUTTON	HS 3542 STOP PUSHBUTTON	HS 3543 LAMP TEST PUSHBUTTON	HS 3544 TRIP RESET PUSH BUTTON	HS 3545 SPEED RAISE/LOWER	HS 3546 LIMITER RAISE/LOWER
HS 3547 HALT PUSH BUTTON	HS 3548 CONTINUE PUSH BUTTON	HS 3549 LOCAL/REMOTE SELECTOR		HS 3550 EMERGENCY PUSHBUTTON	



	TITLE CONTROL OIL SYSTEM P&I DIAGRAM	DOCUMENT CODE SOK0880159	REVISION 2
REVISION DESCRIPTION	PAGE MARKER N/A	SECURITY CODE N	
REVISED WHERE SHOWN -2-	ORIGINAL JOB 1900862-1105209	SIZE 1	LANGUAGE A
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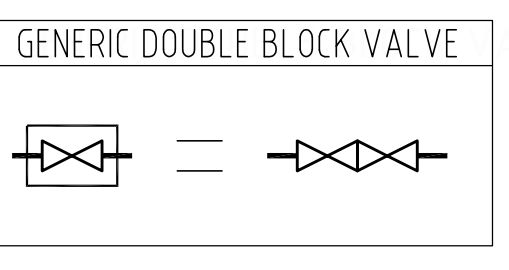
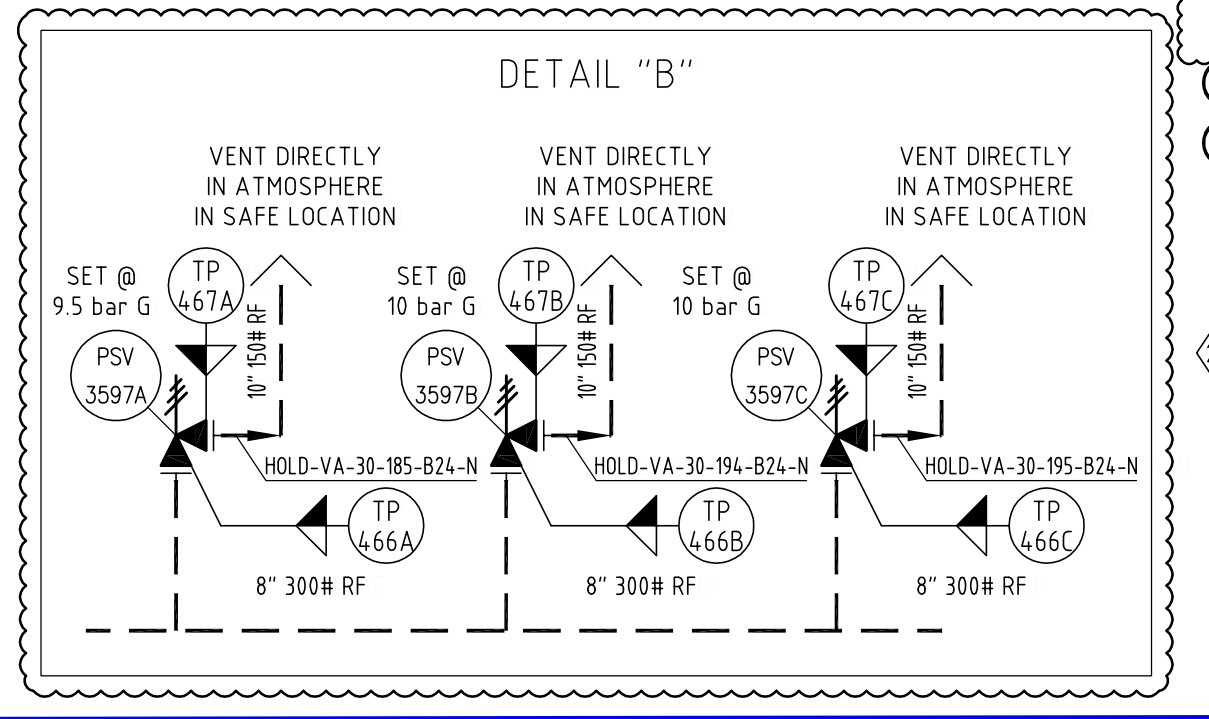
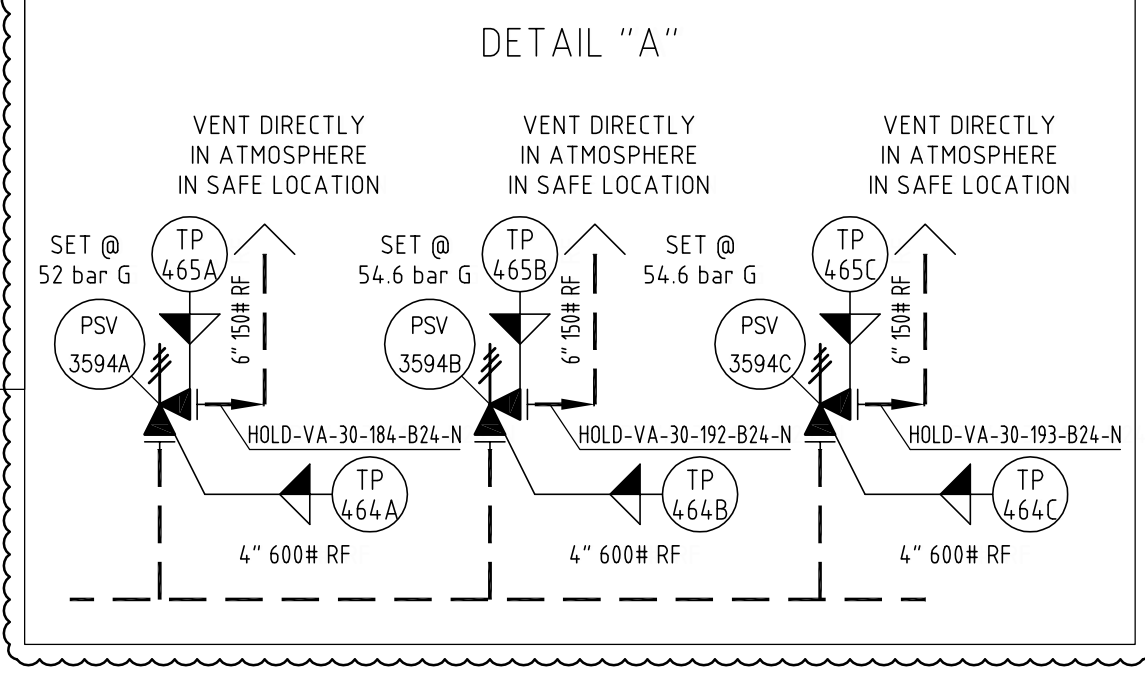
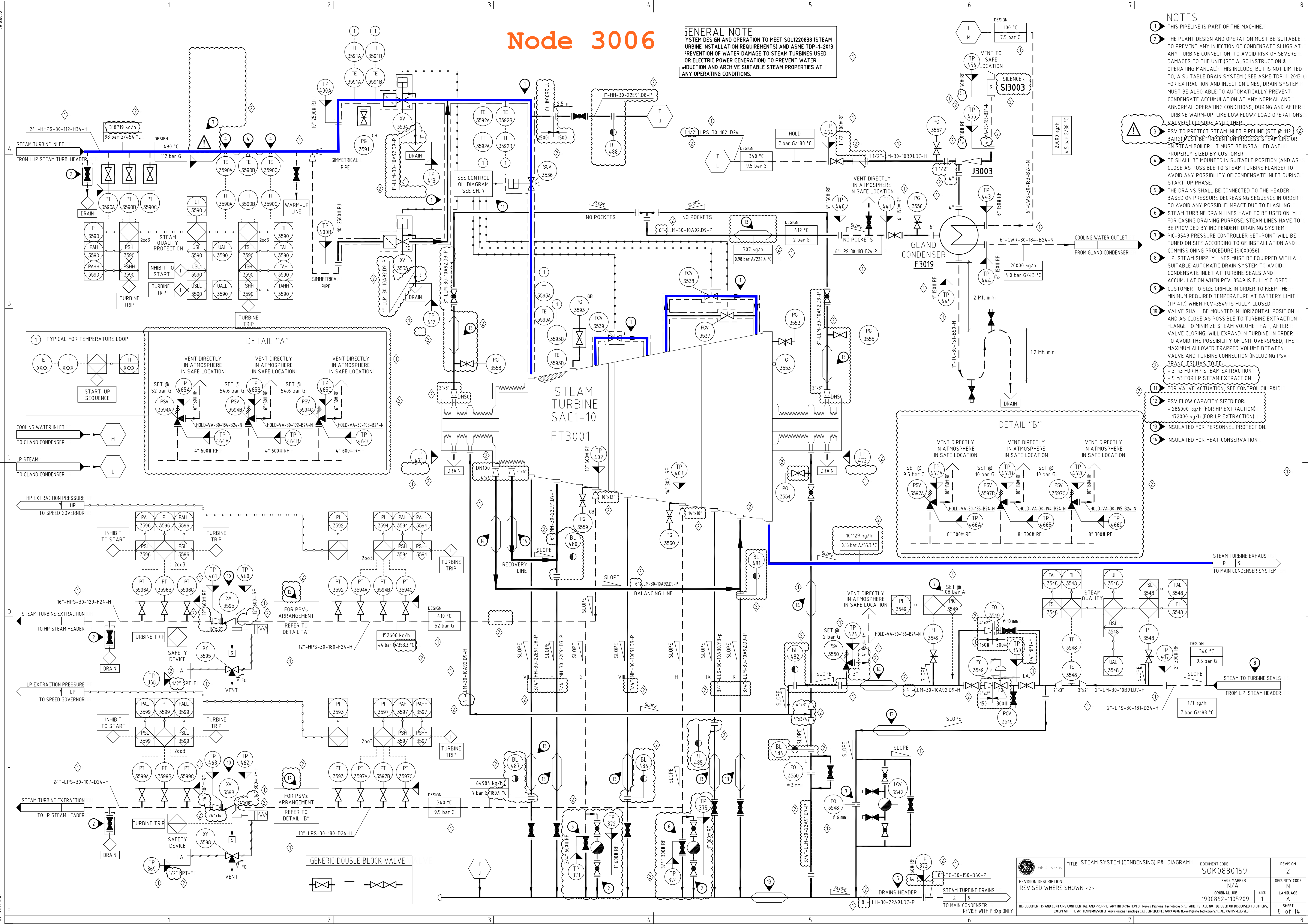


# Node 3006

**GENERAL NOTE**  
 SYSTEM DESIGN AND OPERATION TO MEET SOL1220838 (STEAM TURBINE INSTALLATION REQUIREMENTS) AND ASME TOP-1-2013 (PREVENTION OF WATER DAMAGE TO STEAM TURBINES USED FOR ELECTRIC POWER GENERATION TO PREVENT WATER INDUCTION AND ARCHIVE SUITABLE STEAM PROPERTIES AT ANY OPERATING CONDITIONS).

## NOTES

- THIS PIPELINE IS PART OF THE MACHINE.
- THE PLANT DESIGN AND OPERATION MUST BE SUITABLE TO PREVENT ANY INJECTION OF CONDENSATE SLUGS AT ANY TURBINE CONNECTION, TO AVOID RISK OF SEVERE DAMAGES TO THE UNIT (SEE ALSO INSTRUCTION & OPERATING MANUAL). THIS INCLUDE, BUT IS NOT LIMITED TO, A SUITABLE DRAIN SYSTEM (SEE ASME TOP-1-2013). FOR EXTRACTION AND INJECTION LINES, DRAIN SYSTEM MUST BE ALSO ABLE TO AUTOMATICALLY PREVENT CONDENSATE ACCUMULATION AT ANY NORMAL AND ABNORMAL OPERATING CONDITIONS, DURING AND AFTER TURBINE WARM-UP, LIKE LOW FLOW/ LOAD OPERATIONS, VALVES CLOSURE AND OTHERS.
- PSV TO PROTECT STEAM INLET PIPELINE (SET @ 112 BAR G) MUST BE PRESENT ON PROCESS STEAM LINE OR ON STEAM BOILER. IT MUST BE INSTALLED AND PROPERLY SIZED BY CUSTOMER.
- TE SHALL BE MOUNTED IN SUITABLE POSITION (AND AS CLOSE AS POSSIBLE TO STEAM TURBINE FLANGE) TO AVOID ANY POSSIBILITY OF CONDENSATE INLET DURING START-UP PHASE.
- THE DRAINS SHALL BE CONNECTED TO THE HEADER BASED ON PRESSURE DECREASING SEQUENCE IN ORDER TO AVOID ANY POSSIBLE IMPACT DUE TO FLASHING.
- STEAM TURBINE DRAIN LINES HAVE TO BE USED ONLY FOR CASING DRAINING PURPOSE. STEAM LINES HAVE TO BE PROVIDED BY INDEPENDENT DRAINING SYSTEM.
- PIC-3549 PRESSURE CONTROLLER SET-POINT WILL BE TUNED ON SITE ACCORDING TO GE INSTALLATION AND COMMISSIONING PROCEDURE (SIC00056).
- LP STEAM SUPPLY LINES MUST BE EQUIPPED WITH A SUITABLE AUTOMATIC DRAIN SYSTEM TO AVOID CONDENSATE INLET AT TURBINE SEALS AND ACCUMULATION WHEN PCV-3549 IS FULLY CLOSED.
- CUSTOMER TO SIZE ORIFICE IN ORDER TO KEEP THE MINIMUM REQUIRED TEMPERATURE AT BATTERY LIMIT (TP 471) WHEN PCV-3549 IS FULLY CLOSED.
- VALVE SHALL BE MOUNTED IN HORIZONTAL POSITION AND AS CLOSE AS POSSIBLE TO TURBINE EXTRACTION FLANGE TO MINIMIZE STEAM VOLUME THAT, AFTER VALVE CLOSING, WILL EXPAND IN TURBINE. IN ORDER TO AVOID THE POSSIBILITY OF UNIT OVERSPEED, THE MAXIMUM ALLOWED TRAPPED VOLUME BETWEEN VALVE AND TURBINE CONNECTION INCLUDING PSV BRANCHES HAS TO BE:
  - 3 m<sup>3</sup> FOR HP STEAM EXTRACTION
  - 5 m<sup>3</sup> FOR LP STEAM EXTRACTION
- FOR VALVE ACTUATION, SEE CONTROL OIL P&ID.
- PSV FLOW CAPACITY SIZED FOR:
  - 286000 kg/h (FOR HP EXTRACTION)
  - 172000 kg/h (FOR LP EXTRACTION)
- INSULATED FOR PERSONNEL PROTECTION.
- INSULATED FOR HEAT CONSERVATION.



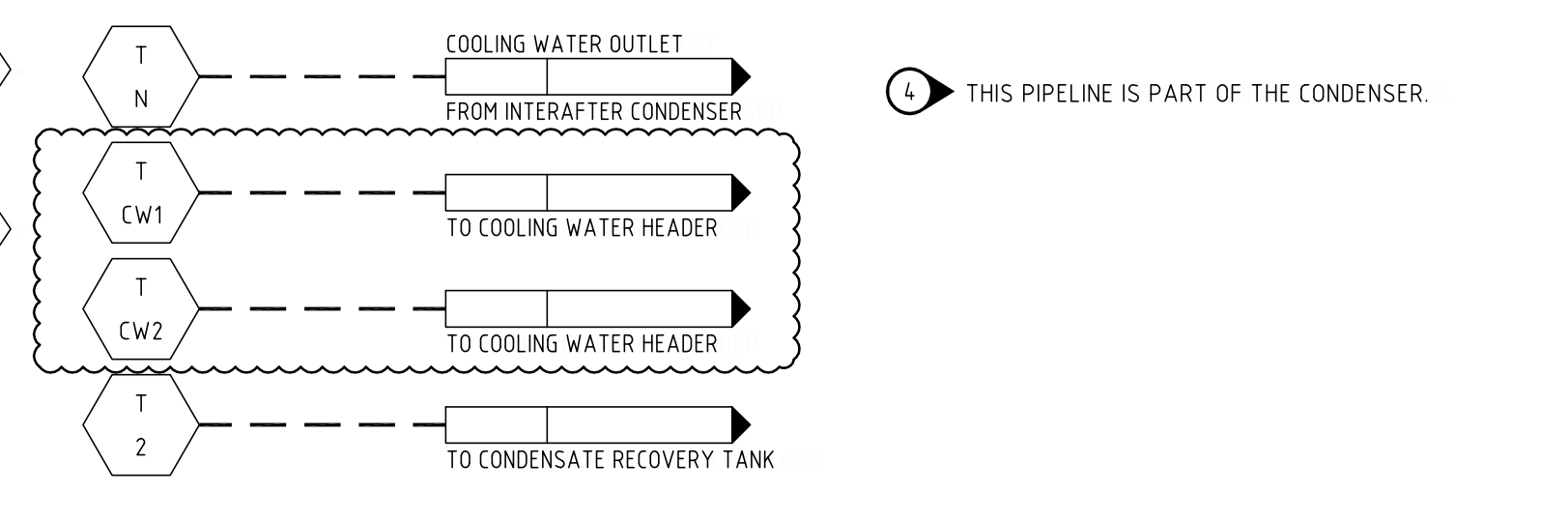
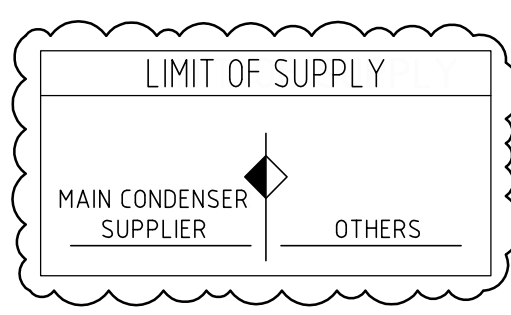
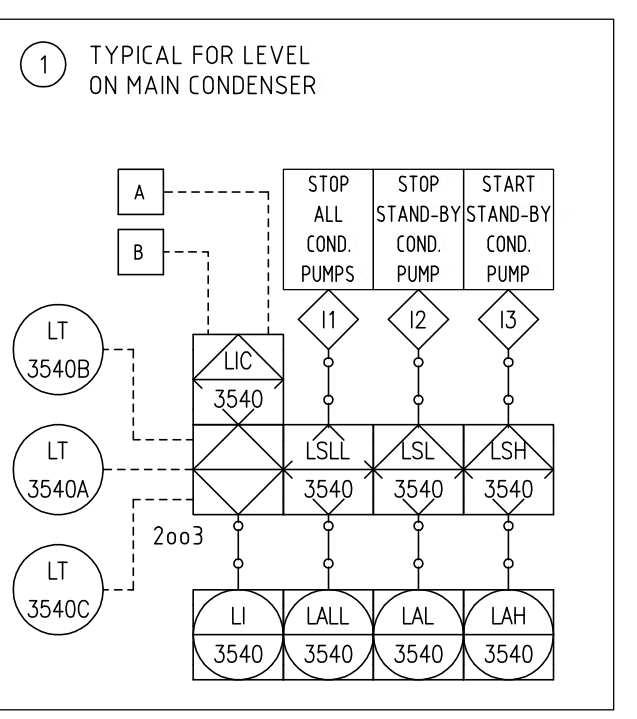
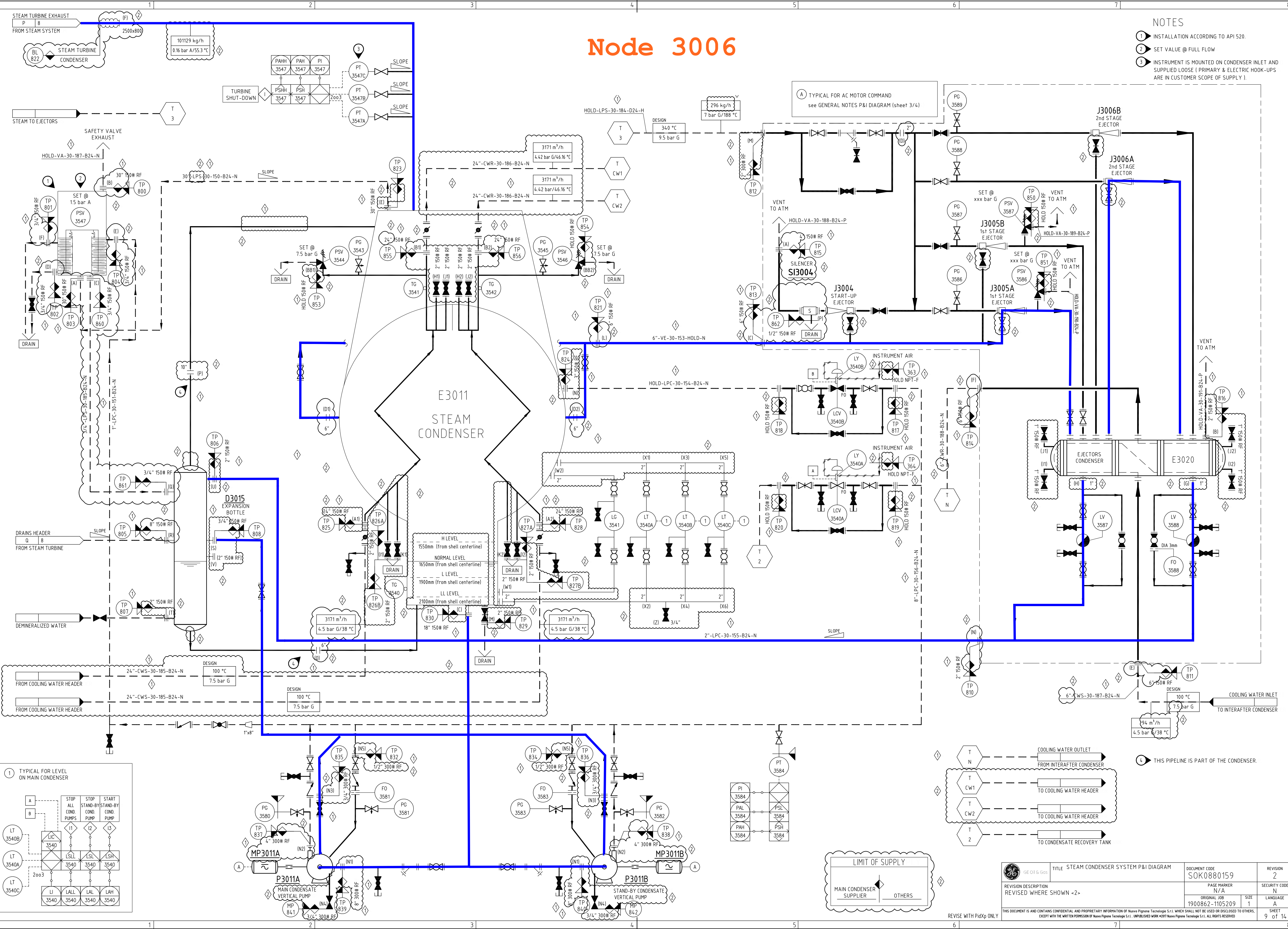
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	ORIGINAL JOB	1900862-1105209	SIZE	1	LANGUAGE	A
						SHEET
						8 of 14



# Node 3006

## NOTES

- 1 INSTALLATION ACCORDING TO API 520.
- 2 SET VALUE @ FULL FLOW
- 3 INSTRUMENT IS MOUNTED ON CONDENSER INLET AND SUPPLIED LOOSE (PRIMARY & ELECTRIC HOOK-UPS ARE IN CUSTOMER SCOPE OF SUPPLY).

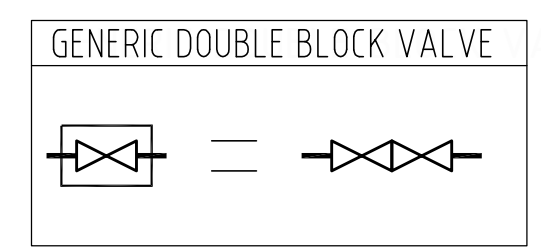
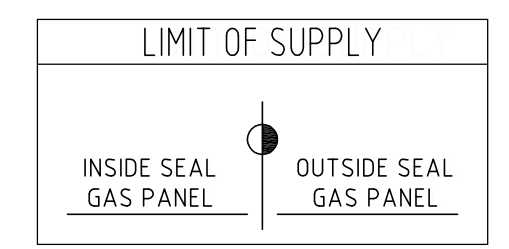
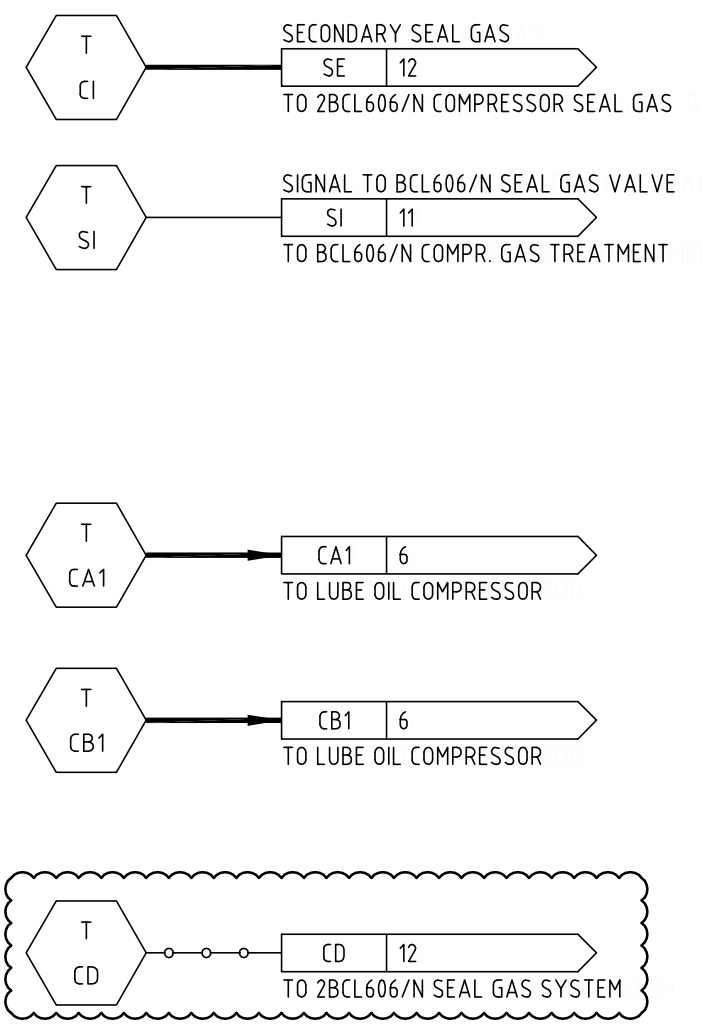
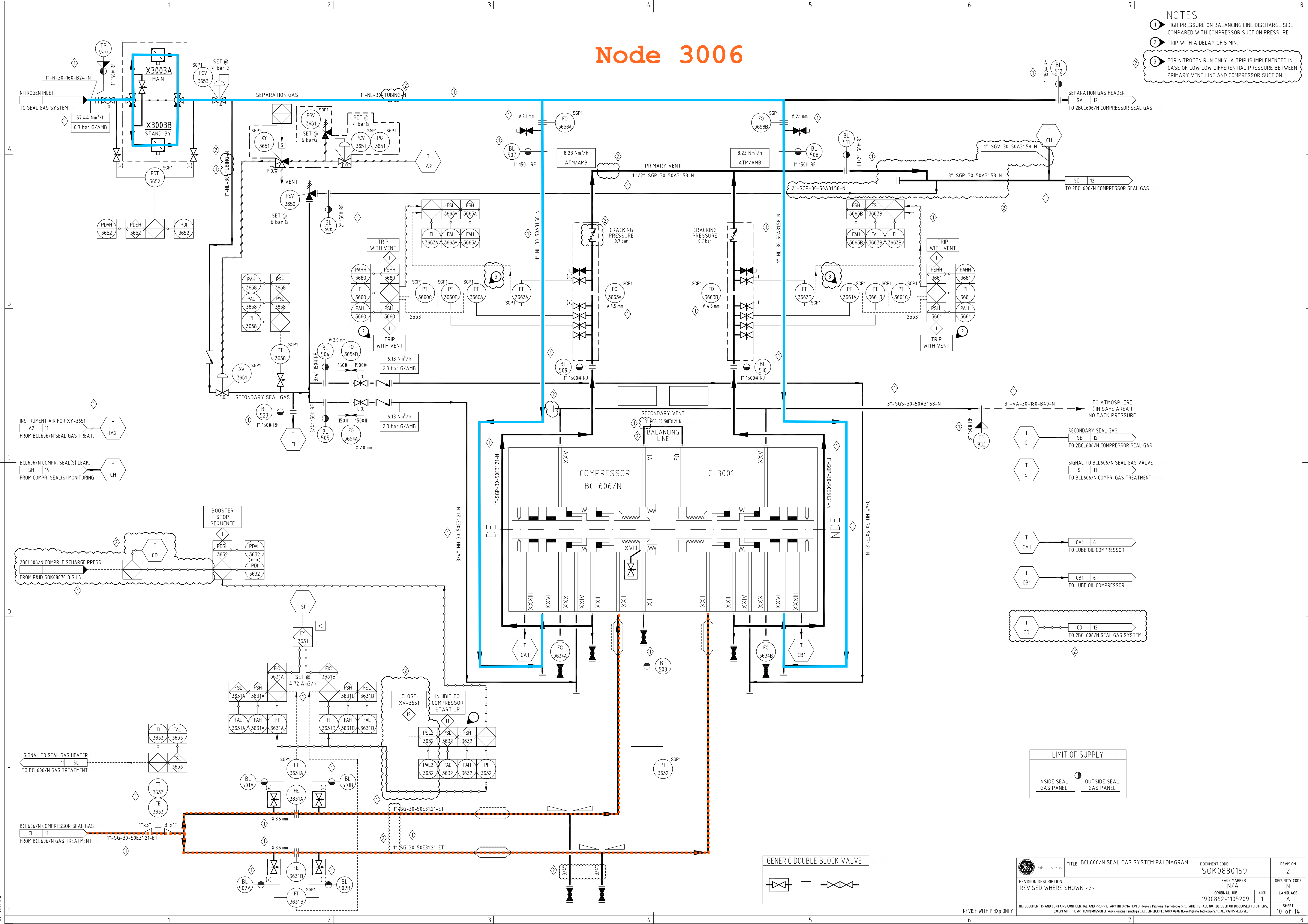


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# Node 3006

- NOTES**
- HIGH PRESSURE ON BALANCING LINE DISCHARGE SIDE COMPARED WITH COMPRESSOR SUCTION PRESSURE.
  - TRIP WITH A DELAY OF 5 MIN.
  - FOR NITROGEN RUN ONLY, A TRIP IS IMPLEMENTED IN CASE OF LOW LOW DIFFERENTIAL PRESSURE BETWEEN PRIMARY VENT LINE AND COMPRESSOR SUCTION.

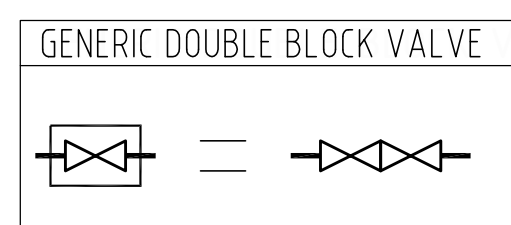
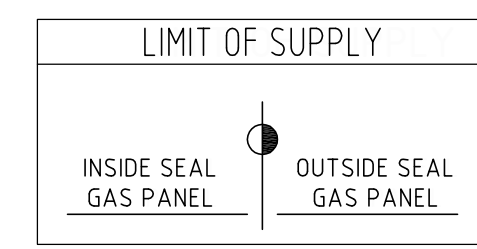
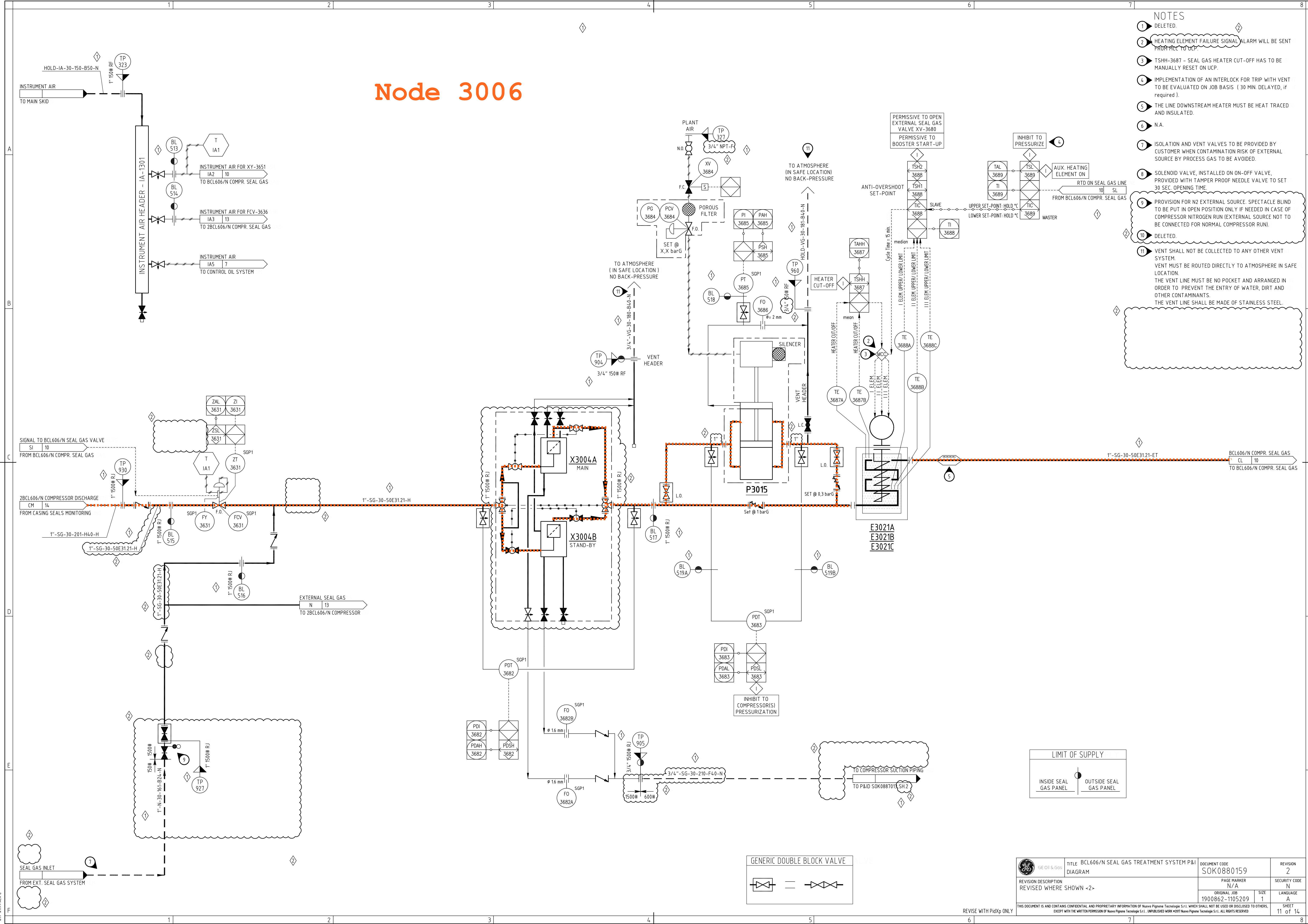


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# Node 3006

- ### NOTES
- DELETED.
  - HEATING ELEMENT FAILURE SIGNAL ALARM WILL BE SENT FROM MCC TO UCP.
  - TSHH-3687 - SEAL GAS HEATER CUT-OFF HAS TO BE MANUALLY RESET ON UCP.
  - IMPLEMENTATION OF AN INTERLOCK FOR TRIP WITH VENT TO BE EVALUATED ON JOB BASIS ( 30 MIN. DELAYED, if required ).
  - THE LINE DOWNSTREAM HEATER MUST BE HEAT TRACED AND INSULATED.
  - N.A.
  - ISOLATION AND VENT VALVES TO BE PROVIDED BY CUSTOMER WHEN CONTAMINATION RISK OF EXTERNAL SOURCE BY PROCESS GAS TO BE AVOIDED.
  - SOLENOID VALVE, INSTALLED ON ON-OFF VALVE, PROVIDED WITH TAMPER PROOF NEEDLE VALVE TO SET 30 SEC. OPENING TIME.
  - PROVISION FOR N2 EXTERNAL SOURCE. SPECTACLE BLIND TO BE PUT IN OPEN POSITION ONLY IF NEEDED IN CASE OF COMPRESSOR NITROGEN RUN (EXTERNAL SOURCE NOT TO BE CONNECTED FOR NORMAL COMPRESSOR RUN).
  - DELETED.
  - VENT SHALL NOT BE COLLECTED TO ANY OTHER VENT SYSTEM. VENT MUST BE ROUTED DIRECTLY TO ATMOSPHERE IN SAFE LOCATION. THE VENT LINE MUST BE NO POCKET AND ARRANGED IN ORDER TO PREVENT THE ENTRY OF WATER, DIRT AND OTHER CONTAMINANTS. THE VENT LINE SHALL BE MADE OF STAINLESS STEEL.



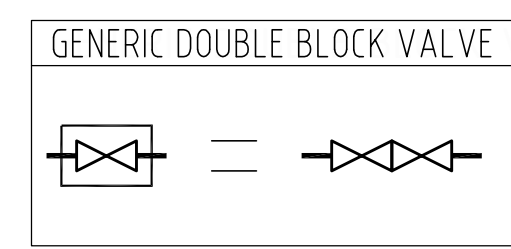
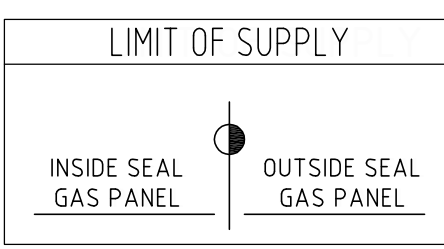
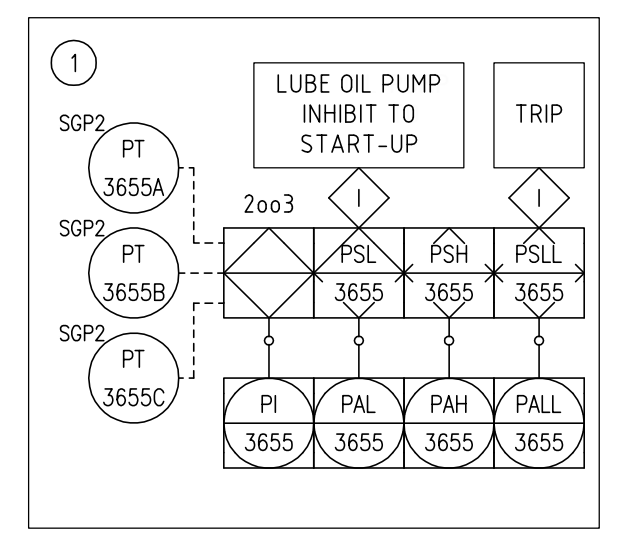
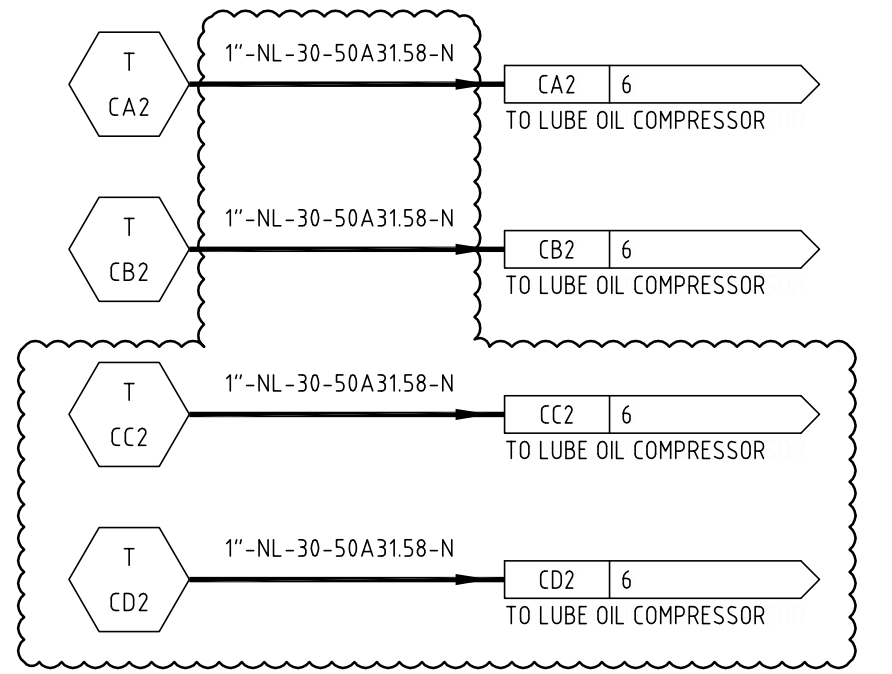
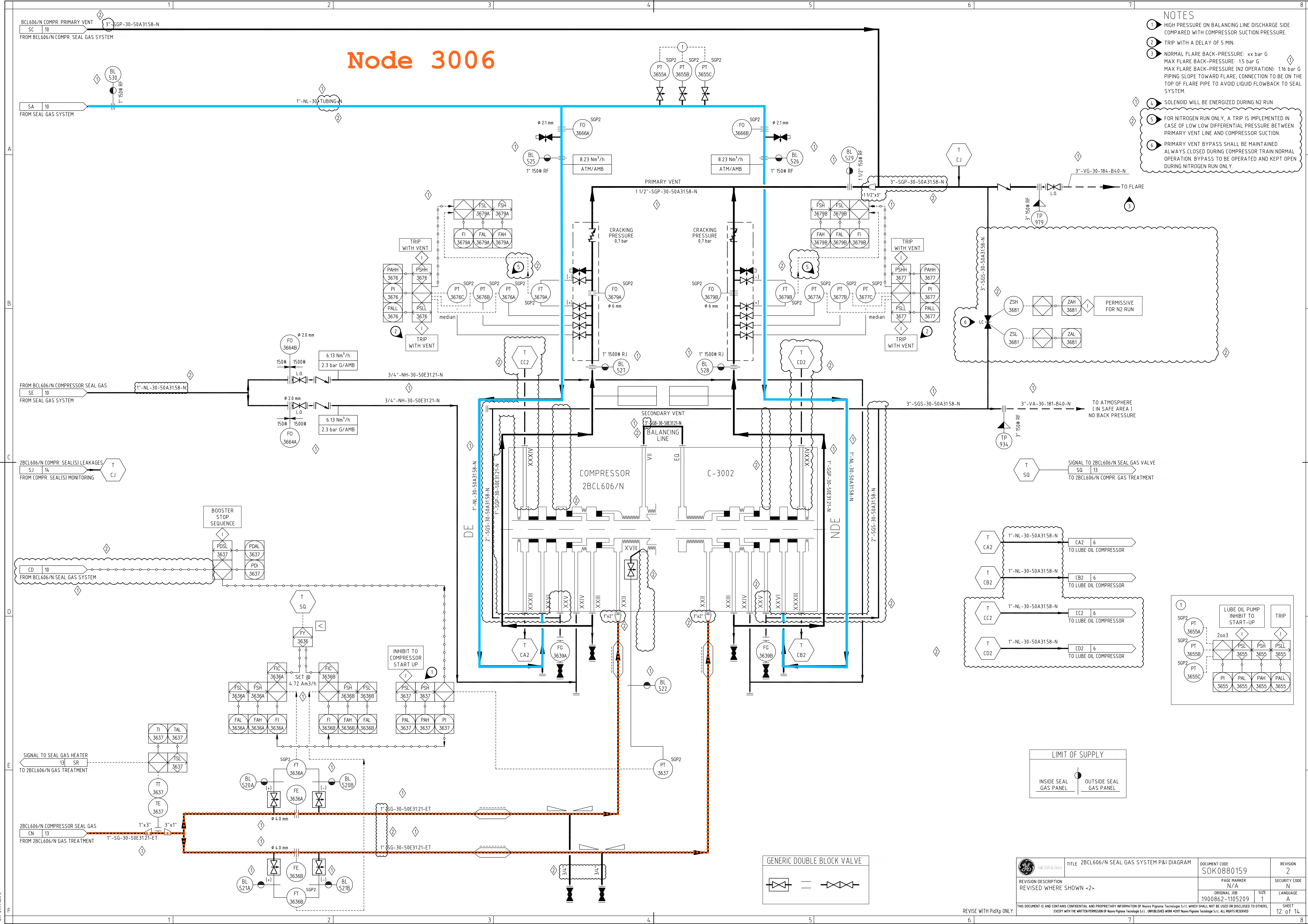
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	ORIGINAL JOB	1900862-1105209	SIZE	1	LANGUAGE	A
					SHEET	11 of 14

REVISE WITH PIDXp ONLY



# Node 3006

- NOTES**
- 1 HIGH PRESSURE ON BALANCING LINE DISCHARGE SIDE COMPARED WITH COMPRESSOR SUCTION PRESSURE.
  - 2 TRIP WITH A DELAY OF 5 MIN.
  - 3 NORMAL FLARE BACK-PRESSURE: xx bar G  
MAX FLARE BACK-PRESSURE: 15 bar G  
MAX FLARE BACK-PRESSURE (N2 OPERATION): 1.16 bar G  
PIPING SLOPE TOWARD FLARE, CONNECTION TO BE ON THE TOP OF FLARE PIPE TO AVOID LIQUID FLOWBACK TO SEAL SYSTEM.
  - 4 SOLENOID WILL BE ENERGIZED DURING N2 RUN.
  - 5 FOR NITROGEN RUN ONLY, A TRIP IS IMPLEMENTED IN CASE OF LOW LOW DIFFERENTIAL PRESSURE BETWEEN PRIMARY VENT LINE AND COMPRESSOR SUCTION.
  - 6 PRIMARY VENT BYPASS SHALL BE MAINTAINED ALWAYS CLOSED DURING COMPRESSOR TRAIN NORMAL OPERATION. BYPASS TO BE OPERATED AND KEPT OPEN DURING NITROGEN RUN ONLY.



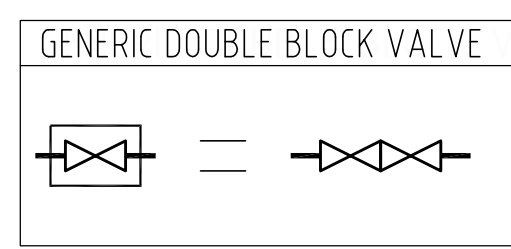
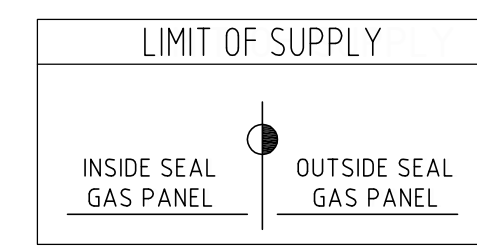
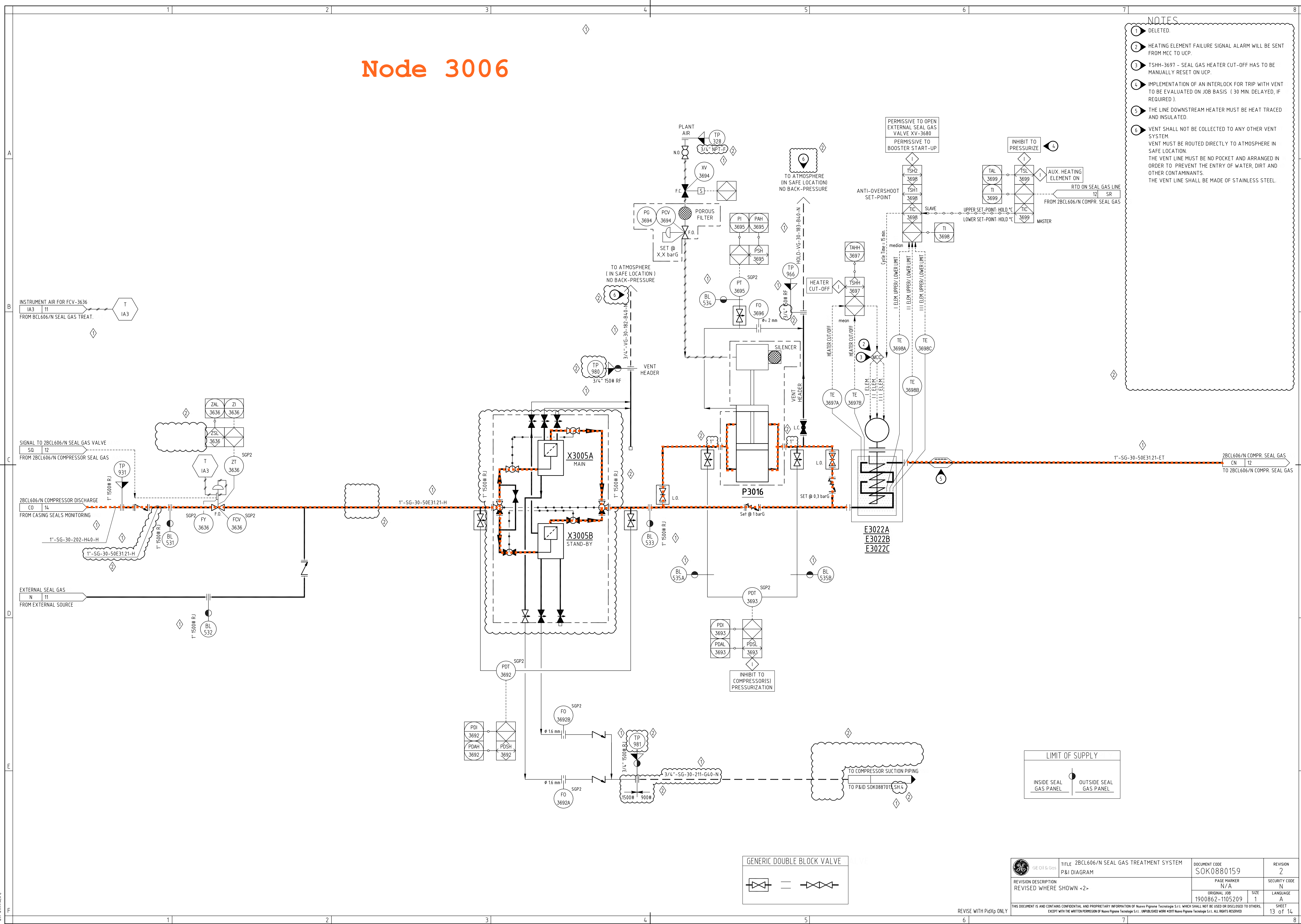
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# Node 3006

## NOTES

- 1 DELETED.
- 2 HEATING ELEMENT FAILURE SIGNAL ALARM WILL BE SENT FROM MCC TO UCP.
- 3 TSHH-3697 - SEAL GAS HEATER CUT-OFF HAS TO BE MANUALLY RESET ON UCP.
- 4 IMPLEMENTATION OF AN INTERLOCK FOR TRIP WITH VENT TO BE EVALUATED ON JOB BASIS ( 30 MIN. DELAYED, IF REQUIRED ).
- 5 THE LINE DOWNSTREAM HEATER MUST BE HEAT TRACED AND INSULATED.
- 6 VENT SHALL NOT BE COLLECTED TO ANY OTHER VENT SYSTEM. VENT MUST BE ROUTED DIRECTLY TO ATMOSPHERE IN SAFE LOCATION. THE VENT LINE MUST BE NO POCKET AND ARRANGED IN ORDER TO PREVENT THE ENTRY OF WATER, DIRT AND OTHER CONTAMINANTS. THE VENT LINE SHALL BE MADE OF STAINLESS STEEL.



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	P&I DIAGRAM					
REVISION DESCRIPTION	REVISED WHERE SHOWN -2-	PAGE MARKER	N/A	SECURITY CODE	N	
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SEAL GAS FROM 2BCL606/N DISCH.  
FROM P&ID SOK0887013 SH5

2"-SG-30-212-H4.0-P

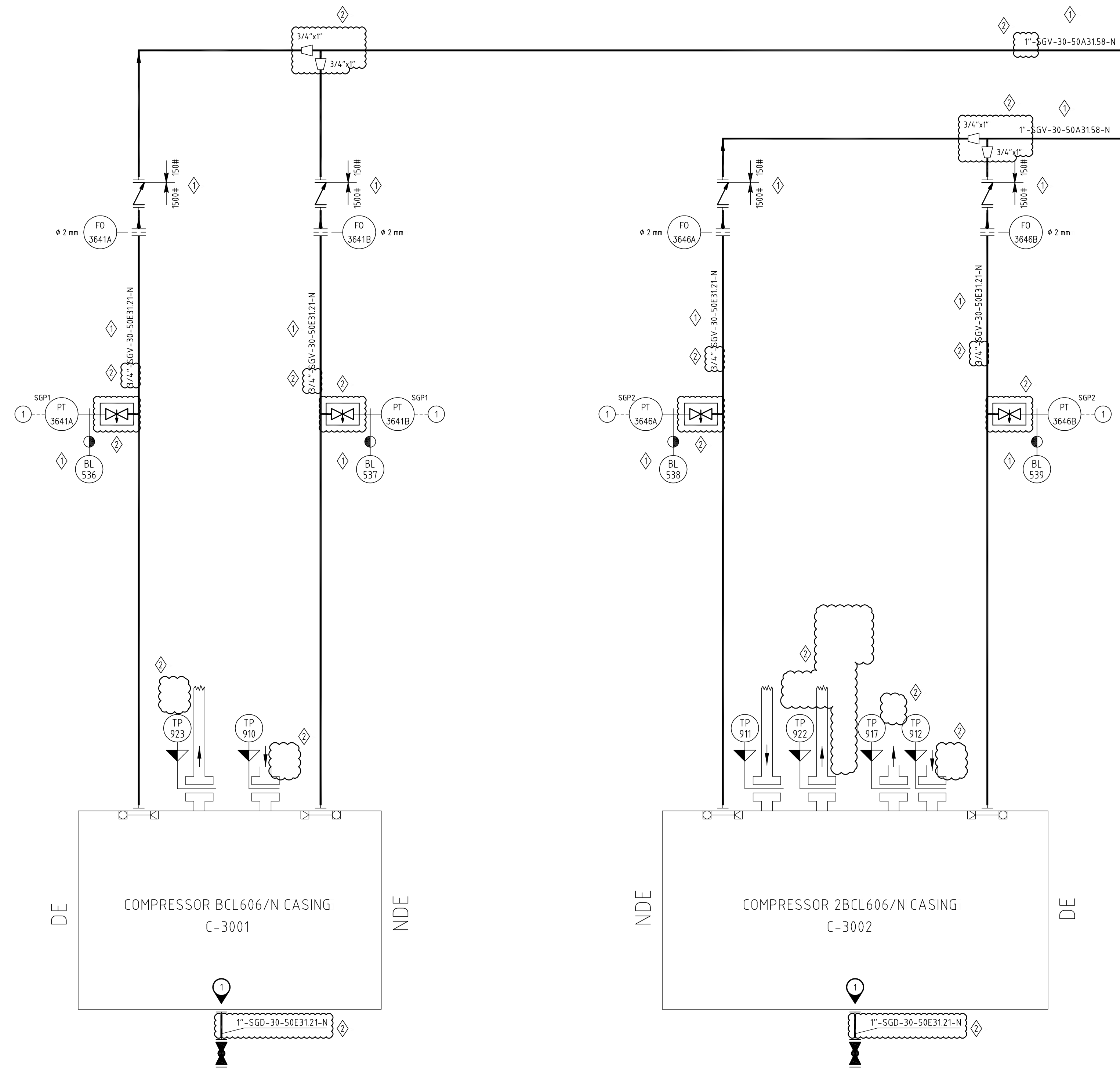
- NOTES**
- 1 ON BCL606/N, THE CASING DRAINS ARE N. 5.
  - ON 2BCL606/N, THE CASING DRAINS ARE N. 6.
  - 2 SEAL GAS SUPPLY FROM 2BCL606/N DISCHARGE DOWNSTREAM TP922 (SEE SOK0887013 SHEET 5).

2BCL606/N COMPRESSOR DISCHARGE  
CO 13  
TO 2BCL606/N COMPR. SEAL GAS SYS

2BCL606/N COMPRESSOR DISCHARGE  
CM 11  
TO BCL606/N COMPR. SEAL GAS SYS

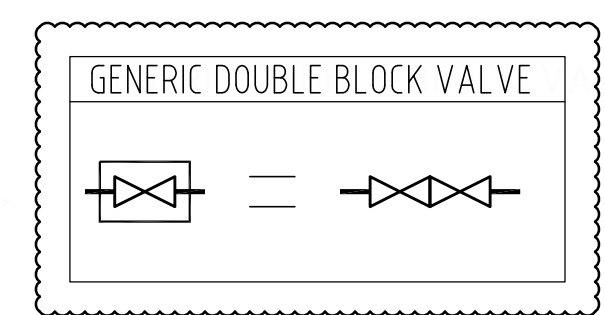
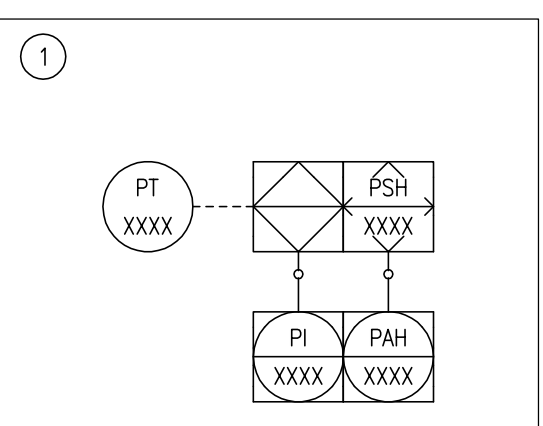
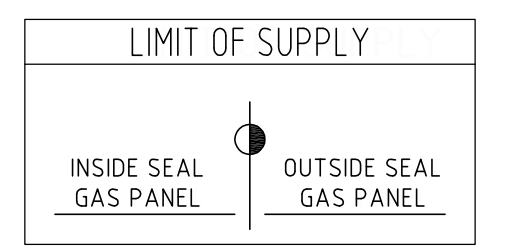
BCL606/N COMPR. SEAL(S) LEAKAGES  
SH 10  
TO BCL606/N COMPRESSOR SEAL GAS

2BCL606/N COMPR. SEAL(S) LEAKAGES  
SJ 12  
TO 2BCL606/N COMPRESSOR SEAL GAS



DE COMPRESSOR BCL606/N CASING C-3001 NDE

NDE COMPRESSOR 2BCL606/N CASING C-3002 DE



	TITLE	CASING SEALS MONITORING SYSTEM P&ID DIAGRAM	DOCUMENT CODE	SOK0880159	REVISION	2
	REVISION DESCRIPTION	REVISED WHERE SHOWN ~2~	PAGE MARKER	N/A	SECURITY CODE	N
	ORIGINAL JOB	1900862-1105209	SIZE	1	LANGUAGE	A
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CUSTOMER : MIDDLE EAST KIMIAYE PARS COMPANY  
 PUMP MODEL : DST 200x150-11S  
 ITEM NO. : P 7001C  
 SERVICE : BFW PUMP  
 SITE : ASSLUYEH, IRAN

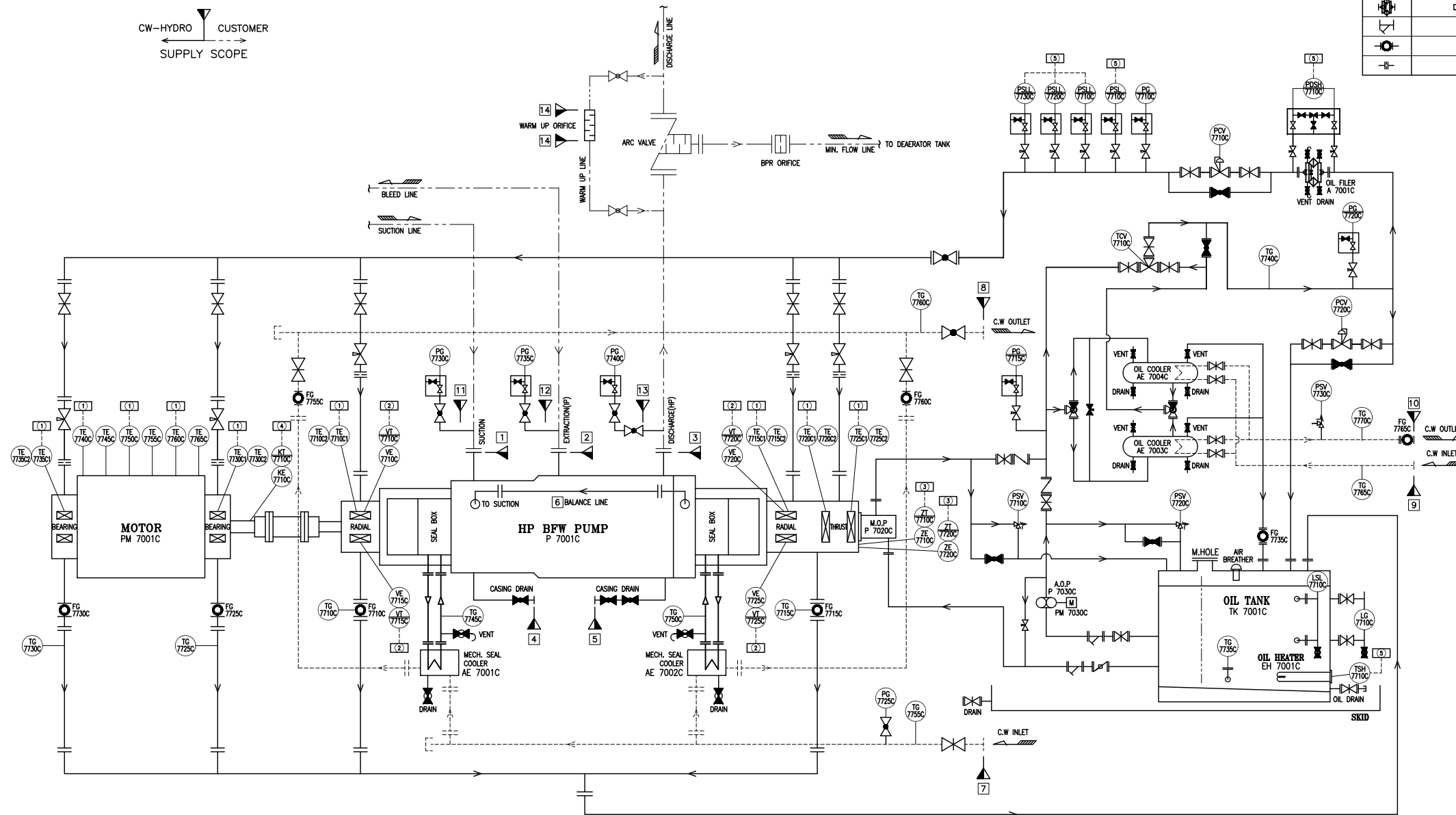
# Node 7007

INSTRUMENTS		
MEASURING ITEM 1ST LETTER	SERVICE 2ND LETTER	SERVICE 3RD LETTER
P PRESSURE	C CONTROL	H HIGH
PD DIFF. PRESSURE	E ELEMENT	HH HIGH HIGH
T TEMPERATURE	G GAUGE	L LOW
L LEVEL	S SWITCH	LL LOW LOW
F FLOW	T TRANSMITTER	
V VIBRATION	P PROXIMITOR	
K KEY PHASER	A ACCELEROMETER	
S SPEED / SATFTY	V VALVE	
Z POSITION		

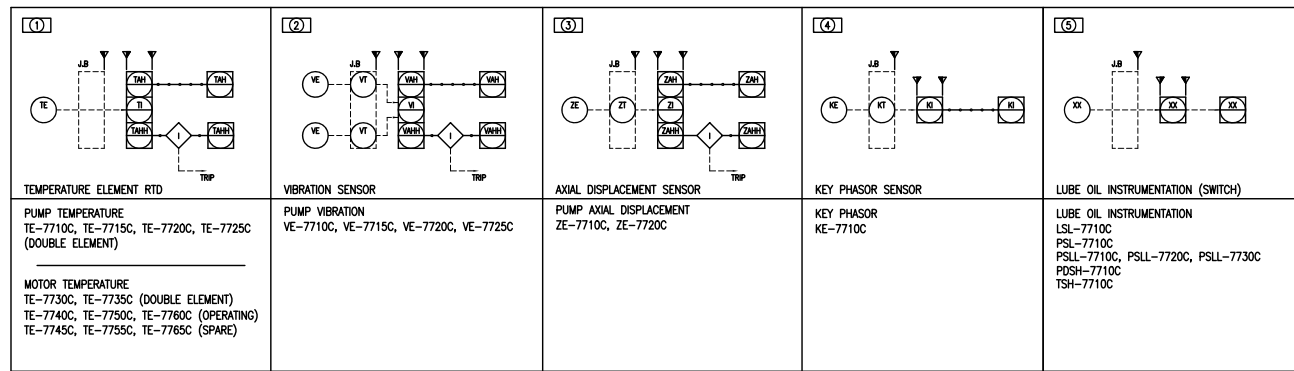
SYMBOL	DESCRIPTION	SYMBOL	DESCRIPTION
	LOCAL FIELD MOUNTED INSTRUMENT		GATE VALVE
	LOCAL PANEL MOUNTED INSTRUMENT		GLOBE VALVE
	FIELD -> DCS		BALL VALVE
	INTERLOCK		NEEDLE VALVE
	SEALING WATER LINE		CHECK VALVE
	LUB. OIL RECIRCULATION LINE		SCREW DOWN CHECK VALVE
	COOLING WATER LINE		3-WAY BALL VALVE
	ELECTRIC SIGNAL		TEMPERATURE CONTROL VALVE(TCV)
			PRESSURE REDUCING VALVE(PCV)
			PRESSURE REGULATING VALVE(PRV)
			SAFETY RELIEF VALVE
			2-WAY MANIFOLD VALVE
			5-WAY MANIFOLD VALVE
			DUPLEX FILTER
			Y-STRAINER
			SIGHT GLASS
			ORIFICE

GENERAL NOTES	
1.	
REFERENCE DRAWINGS	
SYMBOLS AND LEGENDS	
KEY PLAN	

CW-HYDRO CUSTOMER  
 SUPPLY SCOPE



TERMINAL POINTS		
NO.	DESCRIPTION	RATING & SIZE
1	PUMP SUCTION	DN200 ASME 150LB RF
2	PUMP EXTRACTION	DN50 ASME 600LB WN RF
3	PUMP DISCHARGE	DN150 ASME 1500LB RJT
4	CASING DRAIN(SUCTION SIDE)	DN25 ASME 300LB SW RF
5	CASING DRAIN(DISCHARGE SIDE)	DN25 ASME 1500LB SW RF
6	BALANCE LINE	DN40 ASME 300LB SW RF
7	C.W. INLET FOR M/S COOLER	DN40 ASME 150LB SW RF
8	C.W. OUTLET FOR M/S COOLER	DN40 ASME 150LB SW RF
9	C.W. INLET FOR LUBE. OIL COOLER	DN40 ASME 150LB SW RF
10	C.W. OUTLET FOR LUBE. OIL COOLER	DN40 ASME 150LB SW RF
11	SUCTION PRESSURE GAUGE	DN15 600LB SW
12	EXTRACTION PRESSURE GAUGE	DN15 600LB SW
13	DISCHARGE PRESSURE GAUGE	DN15 1500LB SW
14	WARM UP LINE ORIFICE	DN20 ASME 1500LB SW RF



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 REV. PURPOSE OF ISSUE DATE DESIGN DRAW CHECK REVIEW APPROVE  
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OWNER:  
 Middle East Kimiaye Pars Company

CONTRACTOR	HALDOR TOPSØE A/S	CONTRACTOR DRAWING NO.	MKP-VD-9000-303-155-A3
CONTRACTOR	TCC 中國天辰工程有限 CHINA TIANGHEN ENGINEERING CORPORATION	SHEET	03 TOTAL 03
VENDOR	CW-Hydro, Inc.	VENDOR DRAWING NO.	-
		SHEET	03 TOTAL 03
		PROJECT	MKP Methanol Project
		UNIT	General Technical
		PHASE	Detail Engineering
SCALE 1:1	SHEET 03	TOT. 03	SIZE A3
OWNER	MKP-VD-9000-303-155-A3		

Counter Sign Sign Date



CUSTOMER : MIDDLE EAST KIMIAYE PARS COMPANY  
 PUMP MODEL : DST 200x150-11S  
 ITEM NO. : P 7001A/B  
 SERVICE : BFW PUMP  
 SITE : ASSLUYEH, IRAN

TERMINAL POINTS for Pump		
NO.	DESCRIPTION	RATING & SIZE
1	PUMP SUCTION	DN200 ASME 150LB RF
2	PUMP EXTRACTION	DN50 ASME 600LB WN RF
3	PUMP DISCHARGE	DN150 ASME 1500LB RJT
4	CASING DRAIN(SUCTION SIDE)	DN25 ASME 300LB SW RF
5	CASING DRAIN(DISCHARGE SIDE)	DN25 ASME 1500LB SW RF
6	BALANCE LINE	DN40 ASME 300LB SW RF
7	C.W. INLET FOR M/S COOLER	DN40 ASME 150LB SW RF
8	C.W. OUTLET FOR M/S COOLER	DN40 ASME 150LB SW RF
9	C.W. INLET FOR LUBE. OIL COOLER	DN40 ASME 150LB SW RF
10	C.W. OUTLET FOR LUBE. OIL COOLER	DN40 ASME 150LB SW RF
11	SUCTION PRESSURE GAUGE	DN15 600LB SW
12	EXTRACTION PRESSURE GAUGE	DN15 600LB SW
13	DISCHARGE PRESSURE GAUGE	DN15 1500LB SW
14	WARM UP LINE ORIFICE	DN20 ASME 1500LB SW RF

INSTRUMENTS		
MEASURING ITEM 1ST LETTER	SERVICE 2ND LETTER	SERVICE 3RD LETTER
P	C	H
PD	E	HH
T	G	L
L	S	LL
F	T	
V	P	
K	A	
S	V	
Z		

SYMBOL	DESCRIPTION	SYMBOL	DESCRIPTION
	LOCAL FIELD MOUNTED INSTRUMENT		GATE VALVE
	LOCAL PANEL MOUNTED INSTRUMENT		GLOBE VALVE
	FIELD -> DCS		BALL VALVE
	INTERLOCK		NEEDLE VALVE
	SEALING WATER LINE		CHECK VALVE
	LUB. OIL RECIRCULATION LINE		SCREW DOWN CHECK VALVE
	COOLING WATER LINE		3-WAY BALL VALVE
	STEAM LINE		TEMPERATURE CONTROL VALVE(TCV)
	INSTRUMENT AIR		PRESSURE REDUCING VALVE(PCV)
	MECHANICAL LINK		PRESSURE REGULATING VALVE(PRV)
	ELECTRIC SIGNAL		SAFETY RELIEF VALVE

GENERAL NOTES

1.

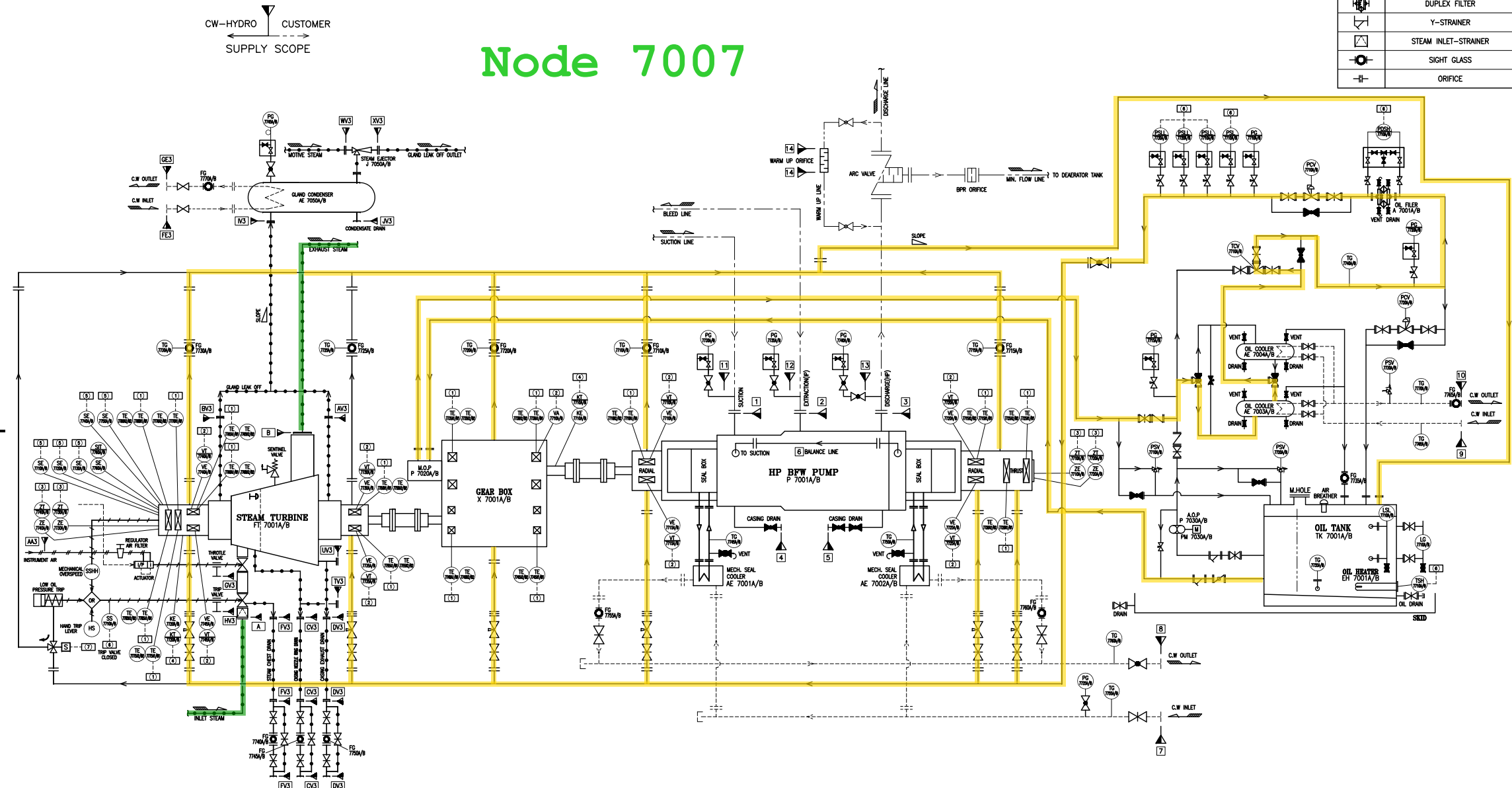
REFERENCE DRAWINGS

SYMBOLS AND LEGENDS

1. MECHANICAL ACTION ON TRIP VALVE CAN OCCUR FROM ANY OF THE 3 CONDITIONS HAND TRIP LEVER, MECHANICAL OVERSPEED OR LOFT

KEY PLAN

# Node 7007



TERMINAL POINTS for TURBINE		
NO.	DESCRIPTION	RATING & SIZE
A	STEAM TURBINE INLET	DN150 ASME 600LB RF
B	STEAM TURBINE EXHAUST	DN300 ASME 150LB RF
AV3	PACKING CASE LEAK OFF	LATER
BV3	PACKING CASE LEAK OFF	LATER
CV3	STEAM TURBINE CASE NOZZLE RING DRAIN	DN20 ASME 600LB RF
DV3	STEAM TURBINE CASING EXHAUST	DN20 ASME 150LB RF
FV3	STEAM CHEST DRAIN	DN20 ASME 600LB RF
GV3	STEAM CHEST COVER LEAK OFF - GOVERNOR V/V	DN15 ASME 150LB SW RF
HV3	STEAM CHEST COVER LEAK OFF - TRIP V/V	DN20 ASME 150LB SW RF
IV3	GLAND CONDENSOR - STEAM INLET	LATER
JV3	GLAND CONDENSOR - CONDENSATE OUTLET	LATER
TV3	PROVISION FOR 1ST STAGE PRESS. MEASUREMENT	DN20 ASME 600LB RF
UV3	PROVISION FOR EXHAUST PRESS. MEASUREMENT	DN20 ASME 150LB RF
XV3	STEAM EJECTOR - OUTLET	LATER
WV3	STEAM EJECTOR - INLET MOTIVE STEAM	LATER
FE3	C.W. INLET FOR STEAM GLAND	LATER
GE3	C.W. OUTLET FOR STEAM GLAND	LATER
AA3	ACTUATOR AIR INLET	1/4" NPT F

 TEMPERATURE ELEMENT RTD PUMP TEMPERATURE TE-7710A/B, TE-7715A/B, VE-7720A/B, TE-7725A/B (DOUBLE ELEMENT) GEAR BOX TEMPERATURE TE-7730A/B, TE-7735A/B, TE-7740A/B, TE-7745A/B (DOUBLE ELEMENT) STEAM TURBINE TEMPERATURE TE-7750A/B, TE-7755A/B, TE-7760A/B, TE-7765A/B TE-7770A/B, TE-7775A/B, TE-7780A/B, TE-7785A/B (DOUBLE ELEMENT)	 VIBRATION SENSOR PUMP VIBRATION VE-7710A/B, VE-7715A/B, VE-7720A/B, VE-7725A/B GEAR BOX VIBRATION VA-7710A/B STEAM TURBINE VIBRATION VE-7730A/B, VE-7735A/B, VE-7740A/B, VE-7745A/B	 AXIAL DISPLACEMENT SENSOR PUMP AXIAL DISPLACEMENT ZE-7710A/B, ZE-7720A/B STEAM TURBINE AXIAL DISPLACEMENT ZE-7730A/B, ZE-7740A/B	 KEY PHASOR SENSOR KEY PHASOR KE-7710A/B, KE-7720A/B	 SPEED SENSOR STEAM TURBINE OVERSPEED PROTECTION SE-7710A/B, SE-7720A/B, SE-7730A/B STEAM TURBINE GOVERNOR SE-7740A/B, SE-7750A/B	 SWITCH LUBE OIL INSTRUMENTATION LSL-7710A/B PSL-7710A/B PSL-7710A/B, PSL-7720A/B, PSL-7730A/B PSDH-7710A/B TSH-7710A/B STEAM TURBINE LIMIT SWITCH SS-7710A/B
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HALDOR TOPSØE A/S  中國天辰工程有限 CHINA TIANGHEN ENGINEERING CORPORATION  CW-Hydro, Inc.	CONTRACTOR DRAWING NO. MKP-VD-9000-303-150-A3 SHEET 03 TOTAL 03 VENDOR DRAWING NO. SHEET 03 TOTAL 03
P7001AB_BFW_PUMP P&ID_WITH_SUPPLY_LIMIT_&_CONNECTION SCALE 1:1 SHEET 03 TOT. 03 SIZE A3 Counter Signng Sign Date	PROJECT MKP Methanol Project UNIT General Technical PHASE Detail Engineering OWNER DWG NO. MKP-VD-9000-303-150-A3

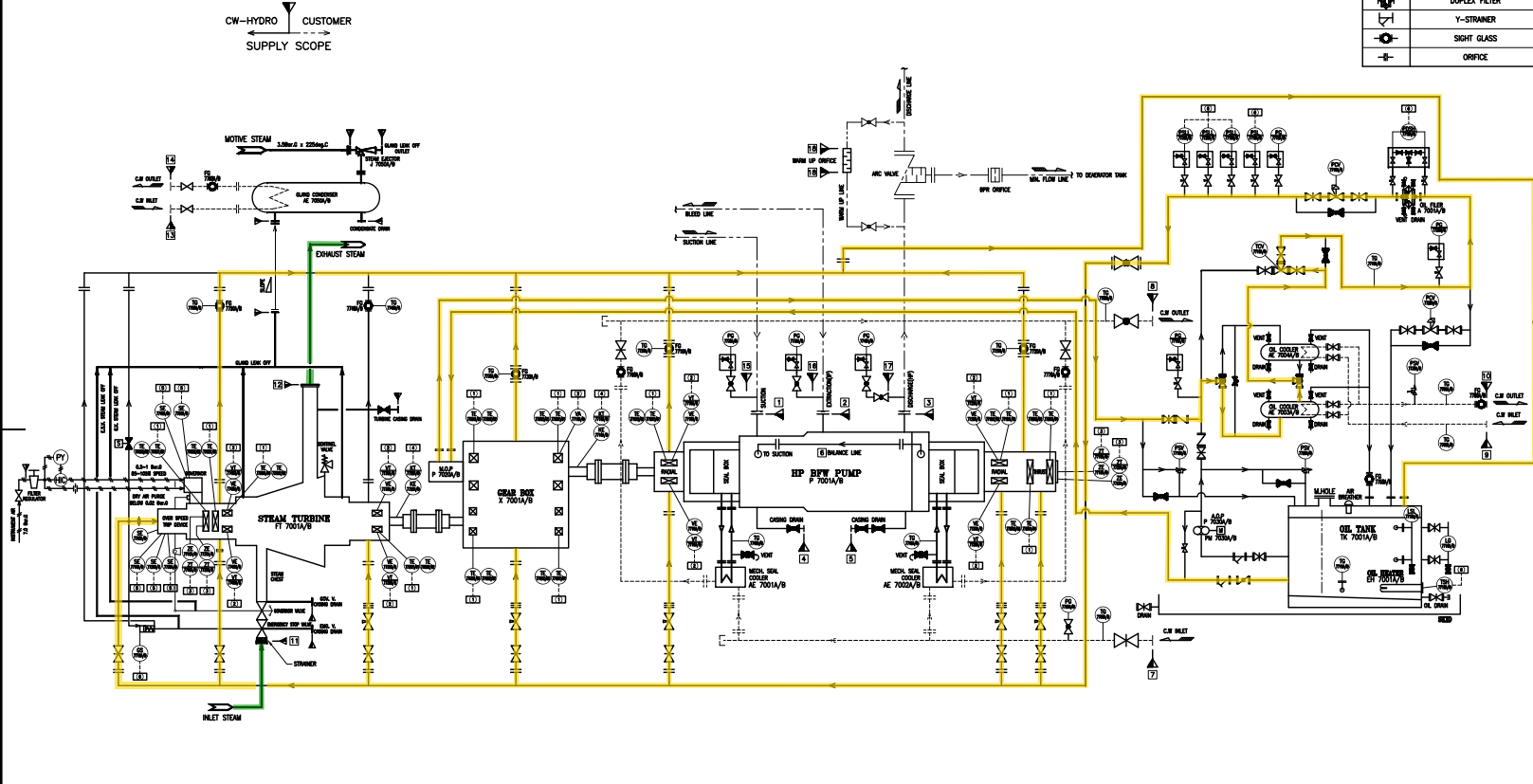
CUSTOMER : MIDDLE EAST KIMIYE PARS COMPANY  
 PUMP MODEL : DST 200x150-11S  
 ITEM NO. : P 7001A/B  
 SERVICE : BFW PUMP  
 SITE : ASSLUYEH, IRAN

# Node 7007

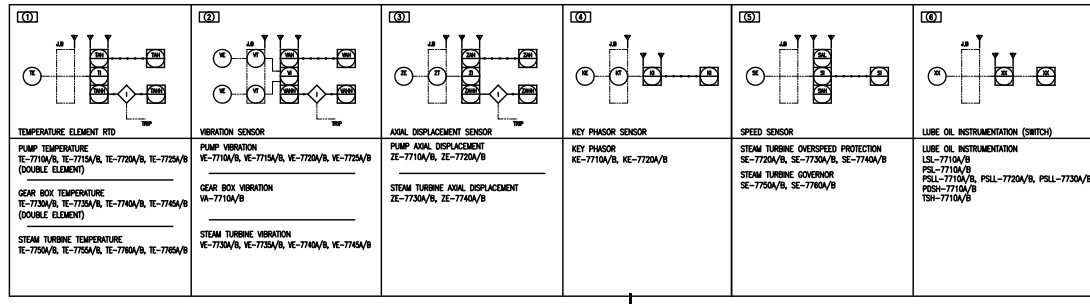
MEASURING ITEM 1ST LETTER	SERVICE 2ND LETTER	SERVICE 3RD LETTER
P PRESSURE	C CONTROL	H HIGH
PD DIFT. PRESSURE	E ELEMENT	HH HIGH HIGH
T TEMPERATURE	G GAUGE	L LOW
L LEVEL	S SWITCH	LL LOW LOW
F FLOW	T TRANSMITTER	
V VIBRATION	P PROXIMATOR	
K KEY PHASER	A ACCELEROMETER	
S SAFETY	V VALVE	
G LIMIT		

SYMBOL	DESCRIPTION	SYMBOL	DESCRIPTION
○	LOCAL FIELD MOUNTED INSTRUMENT	⊗	2-WAY MANIFOLD VALVE
○	LOCAL PANEL MOUNTED INSTRUMENT	⊗	5-WAY MANIFOLD VALVE
◇	FIELD → DCS	⊗	DUPLEX FILTER
◇	INTERLOCK	⊗	Y-STRAINER
—	SEALING WATER LINE	⊗	SIGHT GLASS
—	LUB. OIL RECIRCULATION LINE	⊗	ORFICE
—	COOLING WATER LINE		
—	STEAM LINE		
—	INSTRUMENT AIR		
—	DATALINE OR SOFTWARE		
—	ELECTRIC SIGNAL		

GENERAL NOTES	
1.	
REFERENCE DRAWINGS	
SYMBOLS AND LEGENDS	
KEY PLAN	



TERMINAL POINTS		
NO.	DESCRIPTION	RATING & SIZE
1	PUMP SUCTION	DN200 ASME 150LB RF
2	PUMP EXTRACTION	DN50 ASME 600LB WN RF
3	PUMP DISCHARGE	DN150 ASME 1500LB RJT
4	CASING DRAIN(SUCTION SIDE)	DN25 ASME 300LB SW RF
5	CASING DRAIN(DISCHARGE SIDE)	DN25 ASME 1500LB SW RF
6	BALANCE LINE	DN40 ASME 300LB SW RF
7	C.W. INLET FOR M/S COOLER	DN40 ASME 150LB SW RF
8	C.W. INLET FOR LUBE COOLER	DN40 ASME 150LB SW RF
9	C.W. INLET FOR LUBE OIL COOLER	DN40 ASME 150LB SW RF
10	C.W. OUTLET FOR LUBE OIL COOLER	DN40 ASME 150LB SW RF
11	STEAM TURBINE INLET	DN150 ASME 600LB RF
12	STEAM TURBINE EXHAUST	DN300 ASME 150LB RF
13	C.W. INLET FOR STEAM GLAND	DN65 ASME 150LB SW RF
14	C.W. INLET FOR STEAM GLAND	DN65 ASME 150LB SW RF
15	SUCTION PRESSURE GAUGE	DN15 600LB SW
16	EXTRACTION PRESSURE GAUGE	DN15 600LB SW
17	DISCHARGE PRESSURE GAUGE	DN15 1500LB SW
18	WARM UP LINE ORFICE	DN20 ASME 1500LB SW RF



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 OWNER: Middle East Kimiye Pars Company  
 TCC 中環天機工程顧問有限公司  
 CONTRACTOR DRAWING NO. MWP-VD-9000-303-150-A3  
 SHEET 03 TOTAL 03  
 VENDOR DRAWING NO. -  
 SHEET 03 TOTAL 03  
 PROJECT: MWP Midland Project  
 UNIT: General Technical  
 PHASE: Detail Engineering  
 OWNER DWG NO. MWP-VD-9000-303-150-A3  
 SCALE: 1:1 SHEET 03 TOT. 03 SIZE A3  
 Counter Sign Date

CUSTOMER : MIDDLE EAST KIMIAYE PARS COMPANY  
 PUMP MODEL : DS 700x600-8G  
 ITEM NO. : P 0501 1/2  
 SERVICE : TURBINE DRIVEN COOLING WATER PUMP  
 SITE : ASSLUYEH, IRAN

TERMINAL POINTS for PUMP		
NO.	DESCRIPTION	RATING & SIZE
1	PUMP SUCTION	DN700 ASME 150LB RF
2	PUMP DISCHARGE	DN600 ASME 150LB RF
3	SUCTION PRESSURE GAUGE	DN15 150LB SW
4	DISCHARGE PRESSURE GAUGE	DN15 150LB SW
5	C.W. INLET FOR LUBE. OIL COOLER	DN40 150LB SW
6	C.W. OUTLET FOR LUBE. OIL COOLER	DN40 150LB SW

INSTRUMENTS		
MEASURING ITEM 1ST LETTER	SERVICE 2ND LETTER	SERVICE 3RD LETTER
P PRESSURE	C CONTROL	H HIGH
PD DIFF. PRESSURE	E ELEMENT	HH HIGH HIGH
T TEMPERATURE	G GAUGE	L LOW
L LEVEL	S SWITCH	LL LOW LOW
F FLOW	T TRANSMITTER	
V VIBRATION	P PROXIMITOR	
K KEY PHASER	A ACCELEROMETER	
S SPEED / SAFETY	V VALVE	
Z POSITION		

SYMBOL	DESCRIPTION	SYMBOL	DESCRIPTION
	LOCAL FIELD MOUNTED INSTRUMENT		NORMAL OPEN GATE VALVE
	LOCAL PANEL MOUNTED INSTRUMENT		NORMAL CLOSE GLOBE VALVE
	FIELD -> DCS		NORMAL OPEN BALL VALVE
	INTERLOCK		NORMAL OPEN NEEDLE VALVE
	SEALING WATER LINE		CHECK VALVE
	LUB. OIL RECIRCULATION LINE		SCREW DOWN CHECK VALVE
	COOLING WATER LINE		3-WAY BALL VALVE
	STEAM LINE		TEMPERATURE CONTROL VALVE(TCV)
	INSTRUMENT AIR		PRESSURE REDUCING VALVE(PCV)
	MECHANICAL LINK		PRESSURE REGULATING VALVE(PRV)
	ELECTRIC SIGNAL		SAFETY RELIEF VALVE
			2-WAY MANIFOLD VALVE
			5-WAY MANIFOLD VALVE
			DUPLEX FILTER
			Y-STRAINER
			STEAM INLET-STRAINER
			SIGHT GLASS
			ORIFICE

GENERAL NOTES

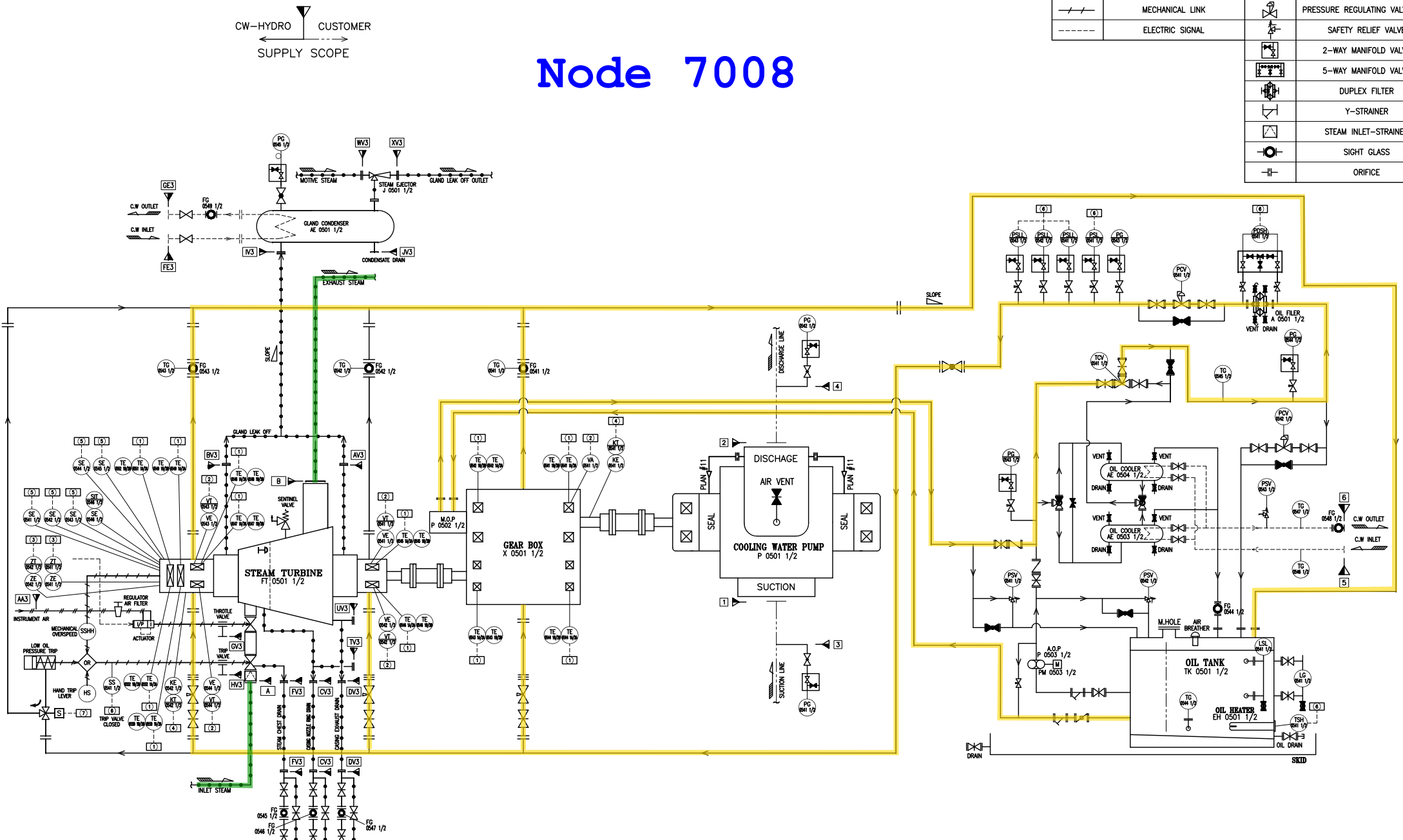
1. MECHANICAL ACTION ON TRIP VALVE CAN OCCURE FROM ANY OF THE 3 CONDITIONS HAND TRIP LEVER, MECHANICAL OVERSPEED OR LOFT

REFERENCE DRAWINGS

SYMBOLS AND LEGENDS

KEY PLAN

# Node 7008



TERMINAL POINTS for TURBINE		
NO.	DESCRIPTION	RATING & SIZE
A	STEAM TURBINE INLET	DN100 ASME 600LB RF
B	STEAM TURBINE EXHAUST	DN200 ASME 150LB RF
AV3	PACKING CASE LEAK OFF	LATER
BV3	PACKING CASE LEAK OFF	LATER
CV3	STEAM TURBINE CASE NOZZLE RING DRAIN	DN20 ASME 600LB RF
DV3	STEAM TURBINE CASING EXHAUST	DN20 ASME 150LB RF
FV3	STEAM CHEST DRAIN	DN20 ASME 600LB RF
GV3	STEAM CHEST COVER LEAK OFF - GOVERNOR V/V	DN15 ASME 150LB SW RF
HV3	STEAM CHEST COVER LEAK OFF - TRIP V/V	DN20 ASME 150LB SW RF
JV3	GLAND CONDENSOR - STEAM INLET	LATER
JV3	GLAND CONDENSOR - CONDENSATE OUTLET	LATER
TV3	PROVISION FOR 1ST STAGE PRESS. MEASUREMENT	DN20 ASME 600LB RF
UV3	PROVISION FOR EXHAUST PRESS. MEASUREMENT	DN20 ASME 150LB RF
XV3	STEAM EJECTOR - OUTLET	LATER
WV3	STEAM EJECTOR - INLET MOTIVE STEAM	LATER
FE3	C.W. INLET FOR STEAM GLAND	LATER
GE3	C.W. OUTLET FOR STEAM GLAND	LATER
AA3	ACTUATOR AIR INLET	1/4" NPT F

 TEMPERATURE ELEMENT RTD GEAR BOX TEMPERATURE TE-0541 1/2, TE-0542 1/2, TE-0543 1/2 TE-0544 1/2(DOUBLE ELEMENT) STEAM TURBINE TEMPERATURE TE-0545 1/2, TE-0546 1/2, TE-0547 1/2 TE-0548 1/2, TE-0549 1/2, TE-0550 1/2 TE-0551 1/2, TE-0552 1/2(DOUBLE ELEMENT)	 VIBRATION SENSOR GEAR BOX VIBRATION VA-0541 1/2 STEAM TURBINE VIBRATION VE-0541 1/2, VE-0542 1/2 VE-0543 1/2, VE-0544 1/2	 AXIAL DISPLACEMENT SENSOR STEAM TURBINE AXIAL DISPLACEMENT ZE-0541 1/2, ZE-0542 1/2	 KEY PHASOR SENSOR KEY PHASOR KE-0541 1/2, KE-0542 1/2	 SPEED SENSOR STEAM TURBINE OVERSPEED PROTECTION SE-0541 1/2, SE-0542 1/2, SE-0543 1/2 STEAM TURBINE GOVERNOR SE-0544 1/2, SE-0545 1/2	 SWITCH LUBE OIL INSTRUMENTATION LSL-0541 1/2 PSL-0541 1/2 PSL-0541 1/2, PSL-0542 1/2, P566-0543 1/2 PDSH-0541 1/2 TSH-0541 1/2 STEAM TURBINE LIMIT SWITCH SS-0541 1/2
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Issued For Approval	21.02.2017	Y.S. HAN	Y.S. HAN	G.M. KANG	M.Y. LEE	M.Y. LEE
REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW / APPROVE

Middle East  
Kimiaye Pars Company

 中國天辰工程有限 CHINA TIANGHEN ENGINEERING CORPORATION	CONTRACTOR DRAWING NO. MKP-VD-9000-311-200-A3 SHEET 03 TOTAL 03 VENDOR DRAWING NO. SHEET 03 TOTAL 03
 CW-Hydro, Inc.	PROJECT MKP Methanol Project UNIT General Technical PHASE Detail Engineering OWNER DWG NO. MKP-VD-9000-311-200-A3

Counter	Sign	Date

SCALE 1:1 SHEET 03 TOT. 03 SIZE A3

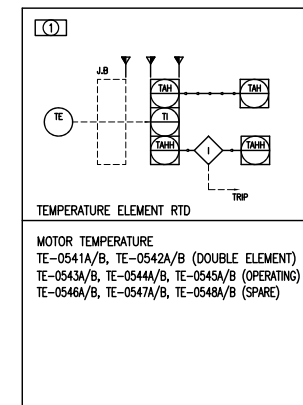
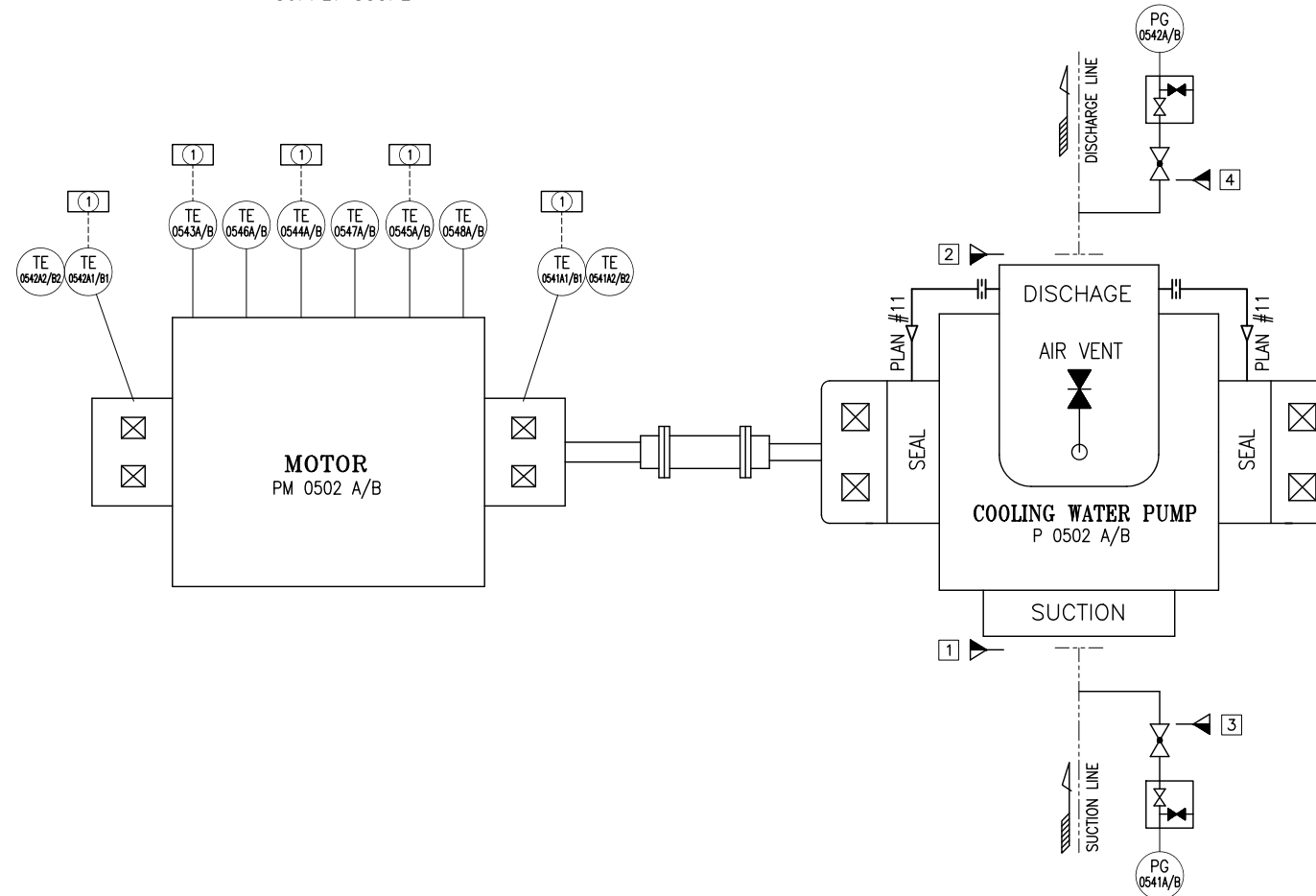
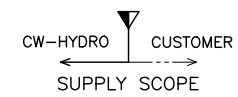
CUSTOMER : MIDDLE EAST KIMIAYE PARS COMPANY  
 PUMP MODEL : DS 700x600-8G  
 ITEM NO. : P 0502 A/B  
 SERVICE : MOTOR DRIVEN COOLING WATER PUMP  
 SITE : ASSLUYEH, IRAN

# Node 7008

INSTRUMENTS	
MEASURING ITEM 1ST LETTER	SERVICE 2ND LETTER
P PRESSURE	E ELEMENT
T TEMPERATURE	G GAUGE

SYMBOL	DESCRIPTION
	GATE VALVE
	GLOBE VALVE
	2-WAY MANIFOLD VALVE
	ORIFICE
	LOCAL FIELD MOUNTED INSTRUMENT
	FIELD -> DCS
	INTERLOCK
	SEALING WATER LINE

TERMINAL POINTS		
NO.	DESCRIPTION	RATING & SIZE
1	PUMP SUCTION	DN700 ASME 150LB RF
2	PUMP DISCHARGE	DN600 ASME 150LB RF
3	SUCTION PRESSURE GAUGE	DN15 150LB SW
4	DISCHARGE PRESSURE GAUGE	DN15 150LB SW



Issued For Approval	20.02.2017	Y.S. HAN	Y.S. HAN	G.M. KANG	M.Y. LEE	M.Y. LEE
REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW / APPROVE

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Middle East  
 Kimiaye Pars Company

CONTRACTOR	HALDOR TOPSØE A/S	CONTRACTOR DRAWING NO.	MKP-VD-9000-311-205-A3
CONTRACTOR	TCC 中國天辰工程有限有限公司 CHINA TIANGHEN ENGINEERING CORPORATION	SHEET	03 TOTAL 03
VENDOR	CW-Hydro, Inc.	VENDOR DRAWING NO.	-
		SHEET	03 TOTAL 03

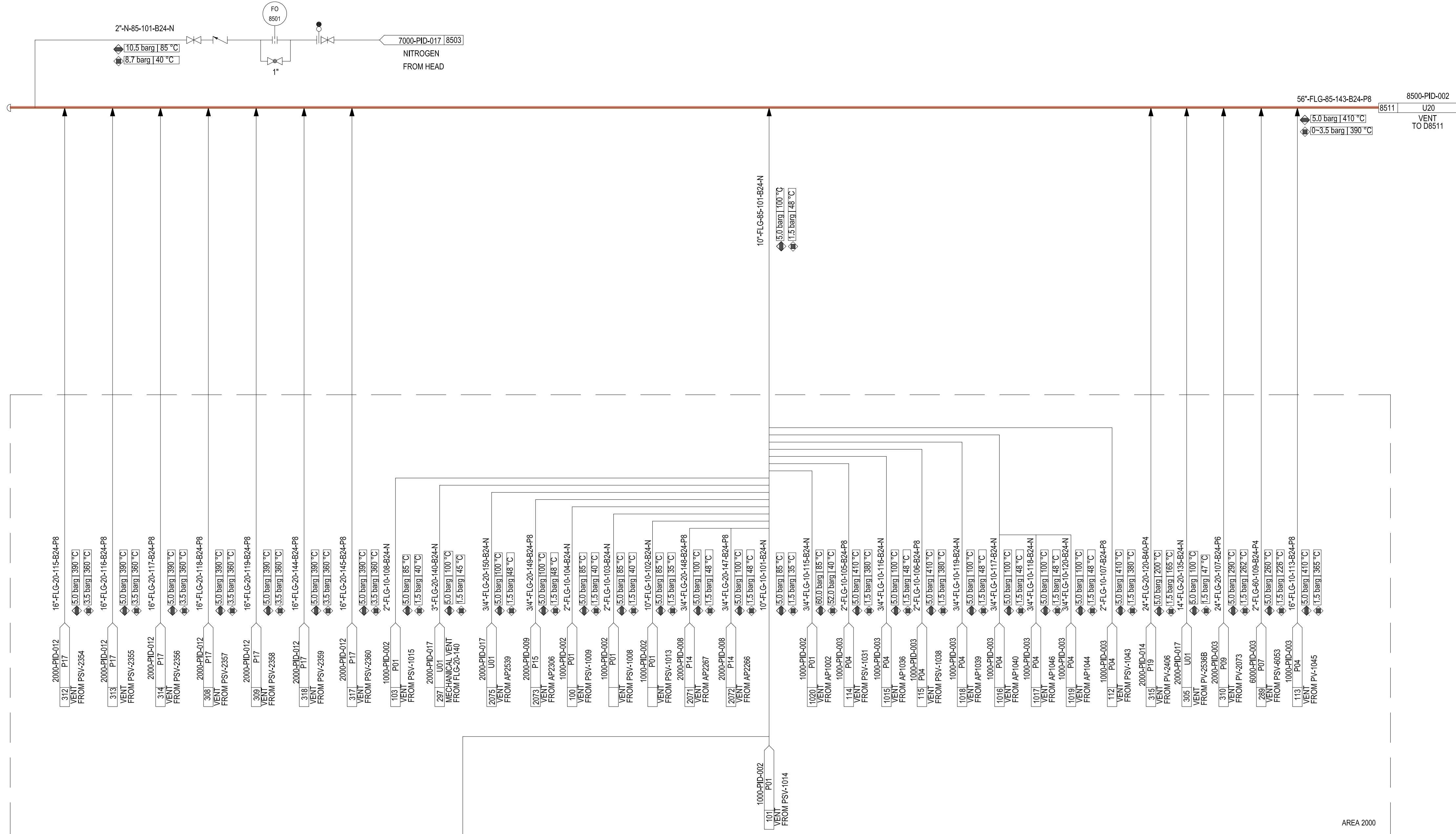
PROJECT	MKP Methanol Project
UNIT	General Technical
PHASE	Detail Engineering
OWNER DWG NO.	MKP-VD-9000-311-205-A3

SCALE	1:1
SHEET	03
TOT.	03
SIZE	A3

Counter Sign Sign Date



# Node 7009



### GENERAL NOTES

- GENERAL NOTE:**  
LOW POINT DRAINS AND HIGH POINT VENT MUST BE ADDED.
- NOTE:**  
1) THE DIRECT ROUTING DISTANCE BETWEEN THE TIE-IN POINT LOCATION OF THE METHANOL PLANT AND THE ACTUAL FLARE SITE IS ABOUT 1600 M.  
2) FOR THE FLARE PIPING ROUTING, ONE STRESS EXPANSION LOOP IS SET AT ABOUT EVERY 60M DISTANCE.

### REFERENCE DRAWINGS

### SYMBOLS AND LEGENDS

### KEY PLAN

REV.	DESCRIPTION	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
△	Approved For Construction	20.12.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Approval	12.10.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Review	31.8.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Comments	29.4.2016	Chen Tao		Xu Hang	Shi Jing	

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OWNER: Middle East Kimiaye Pars Company

LICENSOR <b>T</b> HALDOR TOPSØE A/S CORPORATION	DOCUMENT NAME: FLARE HEADER I UTILITY DIAGRAM	JOB NO. S-02115	DWG. NO. 1341775	DWG. GRP. U19	REV. 3
	CONTRACTOR <b>TCC</b> 中国天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION	CONTRACTOR DRAWING NO. MKP-11-DE-8500-PS09-PID-001 SHEET 01 TOTAL 01			
DESIGNER	SUB-CONTRACTOR DRAWING NO. -				
CHECKER	SHEET - TOTAL -				

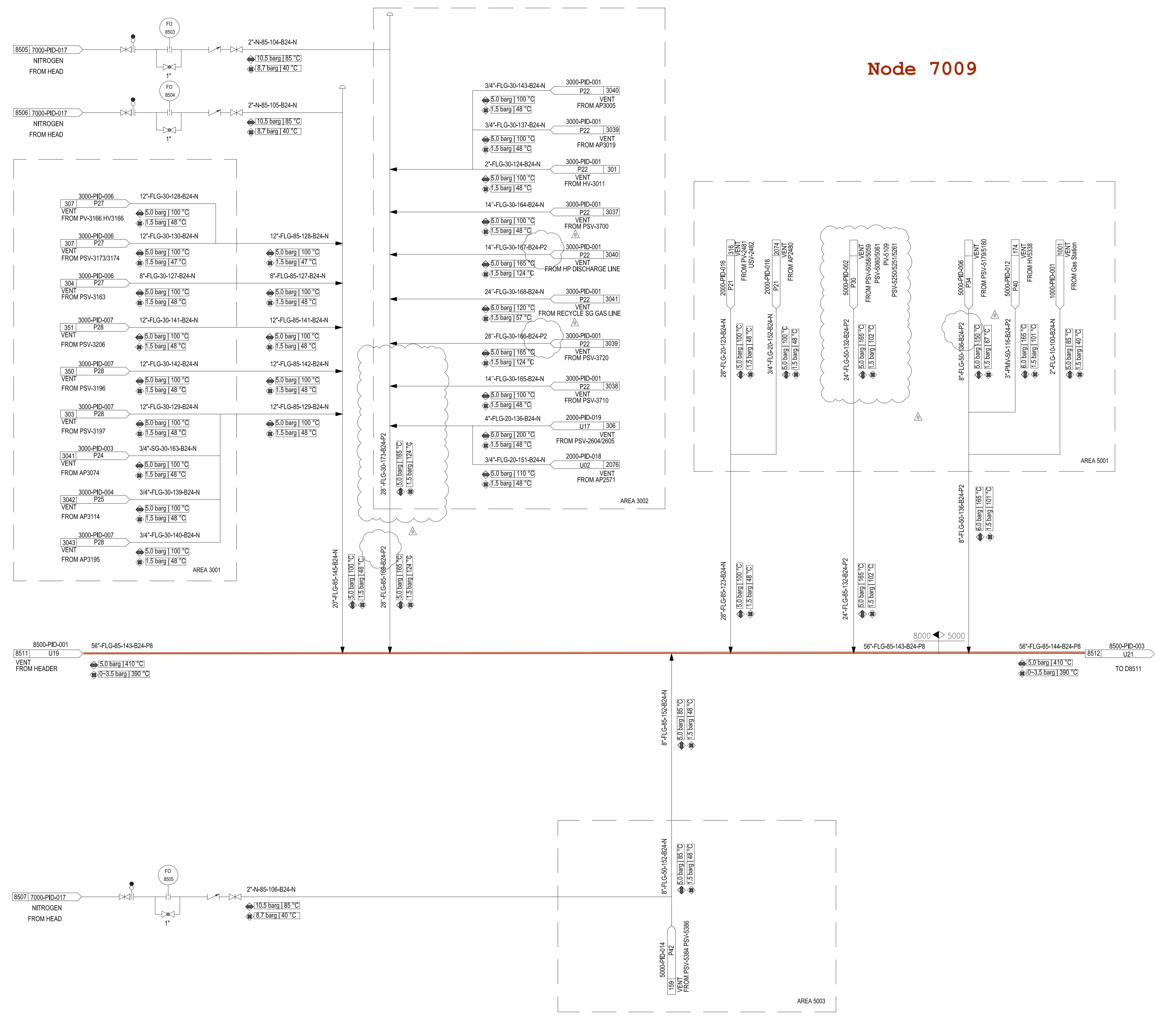
UTILITY DISTRIBUTION DIAGRAM FLARE HEADER I	PROJECT	MKP Methanol Project
	UNIT	Flare
	PHASE	Detail Engineering
SCALE: -	SHEET: 1	TOT.: 1
OWNER DWG. NO.	MKP-11-DE-8500-PR-PID-001	

Counter	Sign	Date

GENERAL NOTES

- † GENERAL NOTE:  
LOW POINT DRAINS AND HIGH POINT VENT MUST BE ADDED.
- † NOTE:  
1) THE DIRECT ROUTING DISTANCE BETWEEN THE TIE-IN POINT LOCATION OF THE METHANOL PLANT AND THE ACTUAL FLARE SITE IS ABOUT 1600 M.  
2) FOR THE FLARE PIPING ROUTING, ONE STRESS EXPANSION LOOP IS SET AT ABOUT EVERY 60M DISTANCE.

Node 7009



REFERENCE DRAWINGS

SYMBOLS AND LEGENDS

KEY PLAN

△	Approved For Construction	20.12.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Approval	12.10.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Review	31.8.2016	Chen Tao		Xu Hang	Shi Jing	
△	Issued For Comments	29.4.2016	Chen Tao		Xu Hang	Shi Jing	

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OWNER: Middle East Kimiaye Pars Company

LICENSOR HALDOR TOPSØE A/S	DOCUMENT NAME: FLARE HEADER II UTILITY DIAGRAM	JOB NO. S-02115	DWG. NO. 1341776	DOC. GRP. 42	U20	REV. 1
	CONTRACTOR DRAWING NO. MKP-11-DE-8500-PS09-PID-002					
SHEET 01 TOTAL 01						
SUB-CONTRACTOR DRAWING NO.						
SHEET - TOTAL -						

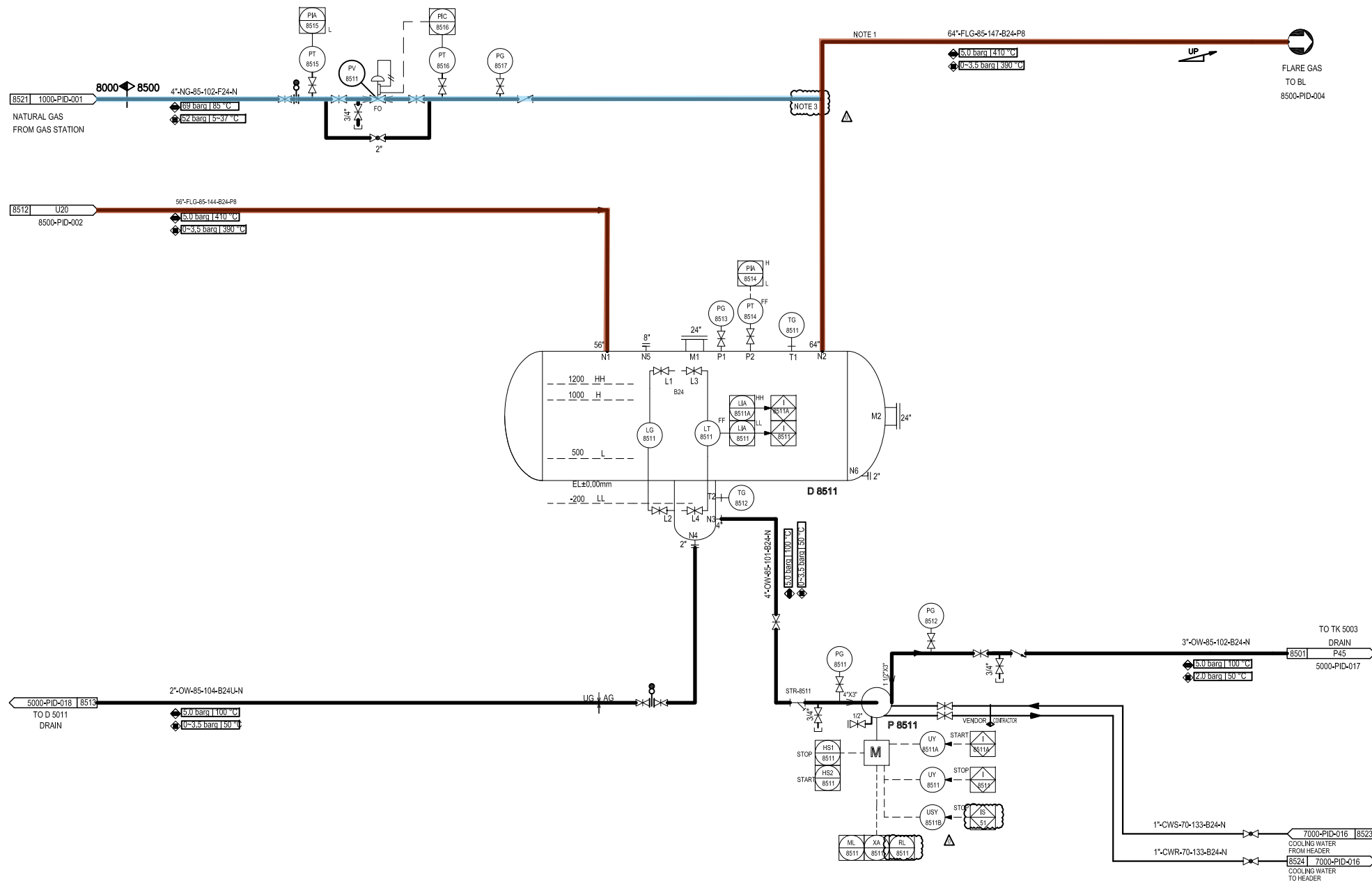
UTILITY DISTRIBUTION DIAGRAM FLARE HEADER II		PROJECT MKP Methanol Project
		UNIT Flare
		PHASE Detail Engineering
OWNER DWC NO.		MKP-11-DE-8500-PR-PID-002

Counter	Sign	Date

P 8511	KNOCK-OUT DRUM PUMP
CAPACITY	30 m <sup>3</sup> /h
HEAD	22 m
DENSITY@OT	990 kg/m <sup>3</sup>
INSULATION/TRACING	NONE
AUXILIARY PIPING	By Vendor
ELEV. of FOUNDATION	EL+101.600m

D 8511	FLARE KNOCK OUT DRUM
ID x LENGTH(T)	5000 x 11000 mm
DESIGN PRESS.	5.5 barg
DESIGN TEMP.	410 °C
INSULATION	YES
CLADDING/LINING	NONE
ELEV. of FOUNDATION	EL+101.600m

# Node 7009



### GENERAL NOTES

- GENERAL NOTE:
- 1) LOW POINT DRAINS AND HIGH POINT VENT MUST BE ADDED.
  - 2) FLARE LINE WITH AN UPWARD SLOPE SHALL ADD LOW POINT DRAINS.
- NOTE:
- 1) THE DIRECT ROUTING DISTANCE BETWEEN THE TIE-IN POINT LOCATION OF THE METHANOL PLANT AND THE ACTUAL FLARE SITE IS ABOUT 1600 M.
  - 2) FOR THE FLARE PIPING ROUTING, ONE STRESS EXPANSION LOOP IS SET AT ABOUT EVERY 60M DISTANCE.
  - 3) THIS CONNECTION POINT IS NEAR TO K.O.D INSIDE OF PLANT B.L.

### REFERENCE DRAWINGS

### SYMBOLS AND LEGENDS

### KEY PLAN

Approved For Construction	20.1.2017	Chen Tao	Xu Hang	Shi Jina
Issued For Approval	20.12.2016	Chen Tao	Xu Hang	Shi Jina
Issued For Approval	12.10.2016	Chen Tao	Xu Hang	Shi Jina
Issued For Review	31.8.2016	Chen Tao	Xu Hang	Shi Jina
Issued For Comments	29.4.2016	Chen Tao	Xu Hang	Shi Jina

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OWNER: **Middle East Kimiaye Pars Company**

HALDOR TOPSØE A/S	DOCUMENT NAME: FLARE STACK UTILITY DIAGRAM	JOB NO. S-02116	SOC. NO. 42	REV. 1
1344813		1344813	DIAGRAM U21	

CONTRACTOR: <b>TCC 中國天辰工程有限公司</b>	
CONTRACTOR DRAWING NO. MKP-11-DE-8500-PS09-PID-003	
SHEET 01	TOTAL 01
SUB-CONTRACTOR DRAWING NO.	
SHEET - TOTAL -	

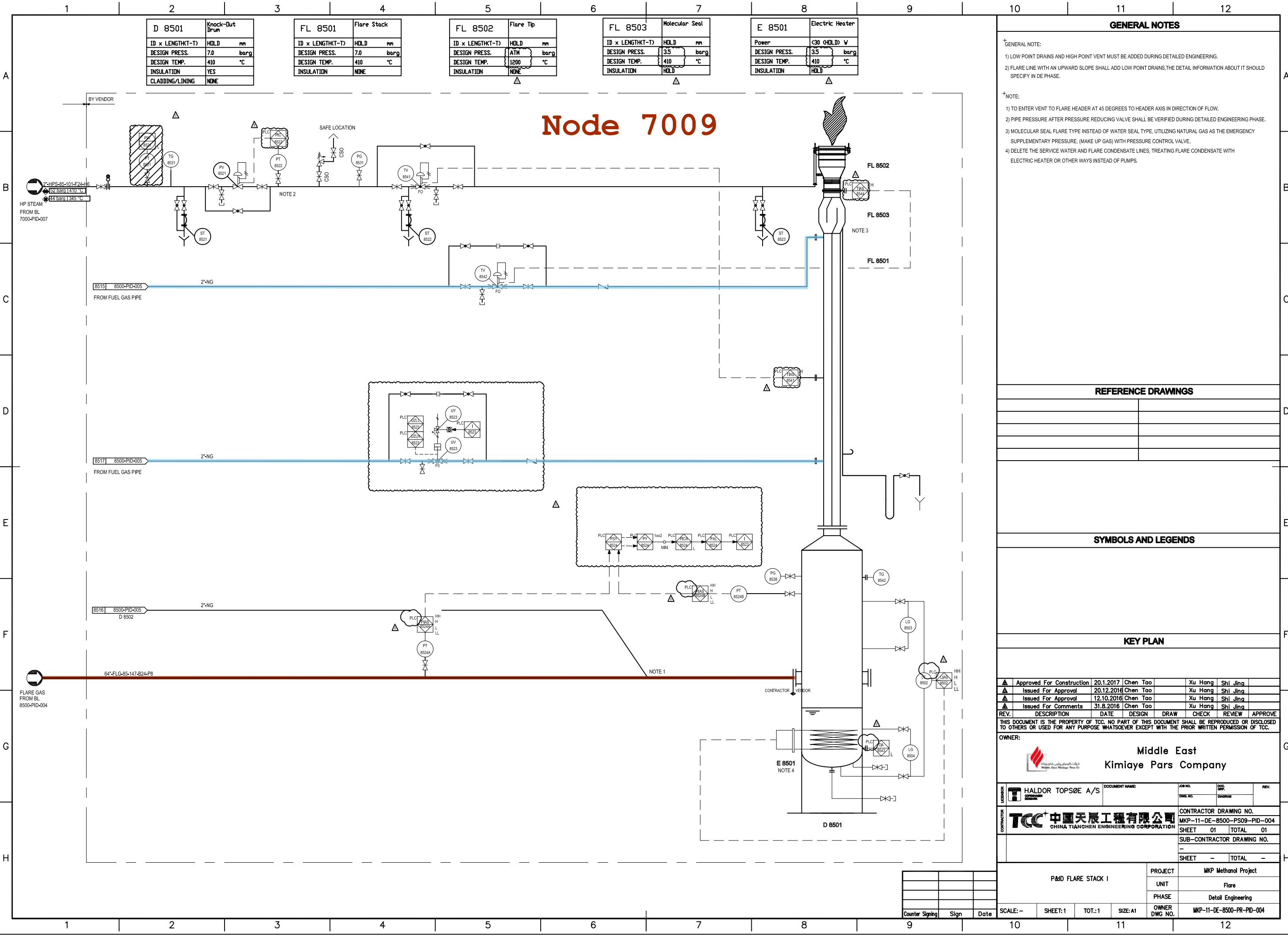
PROJECT: MKP Methanol Project	
UNIT: Flare	
PHASE: Detail Engineering	

P&ID FLARE K.O DRUM		SCALE: -	SHEET: 1	TOT.: 1	SIZE: A1	OWNER DWG NO. MKP-11-DE-8500-PR-PID-003
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Counter Signing	Sign	Date
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# Node 7009



D 8501		Knock-Out Drum	
ID x LENGTH-T	HOLD mm		
DESIGN PRESS.	7.0 barg		
DESIGN TEMP.	410 °C		
INSULATION	YES		
CLADDING/LINING	NONE		

FL 8501		Flare Stack	
ID x LENGTH-T	HOLD mm		
DESIGN PRESS.	7.0 barg		
DESIGN TEMP.	410 °C		
INSULATION	NONE		

FL 8502		Flare Tip	
ID x LENGTH-T	HOLD mm		
DESIGN PRESS.	ATM barg		
DESIGN TEMP.	1200 °C		
INSULATION	NONE		

FL 8503		Molecular Seal	
ID x LENGTH-T	HOLD mm		
DESIGN PRESS.	3.5 barg		
DESIGN TEMP.	410 °C		
INSULATION	HOLD		

E 8501		Electric Heater	
Power	<30 (HOLD) W		
DESIGN PRESS.	3.5 barg		
DESIGN TEMP.	410 °C		
INSULATION	HOLD		

### GENERAL NOTES

- GENERAL NOTE:**
- 1) LOW POINT DRAINS AND HIGH POINT VENT MUST BE ADDED DURING DETAILED ENGINEERING.
  - 2) FLARE LINE WITH AN UPWARD SLOPE SHALL ADD LOW POINT DRAINS, THE DETAIL INFORMATION ABOUT IT SHOULD SPECIFY IN DE PHASE.
- NOTE:**
- 1) TO ENTER VENT TO FLARE HEADER AT 45 DEGREES TO HEADER AXIS IN DIRECTION OF FLOW.
  - 2) PIPE PRESSURE AFTER PRESSURE REDUCING VALVE SHALL BE VERIFIED DURING DETAILED ENGINEERING PHASE.
  - 3) MOLECULAR SEAL FLARE TYPE INSTEAD OF WATER SEAL TYPE, UTILIZING NATURAL GAS AS THE EMERGENCY SUPPLEMENTARY PRESSURE, (MAKE UP GAS) WITH PRESSURE CONTROL VALVE.
  - 4) DELETE THE SERVICE WATER AND FLARE CONDENSATE LINES, TREATING FLARE CONDENSATE WITH ELECTRIC HEATER OR OTHER WAYS INSTEAD OF PUMPS.

### REFERENCE DRAWINGS

### SYMBOLS AND LEGENDS

### KEY PLAN

▲	Approved For Construction	20.1.2017	Chen Tao		Xu Hang	Shi Jina
▲	Issued For Approval	20.12.2016	Chen Tao		Xu Hang	Shi Jina
▲	Issued For Approval	12.10.2016	Chen Tao		Xu Hang	Shi Jina
▲	Issued For Comments	31.8.2016	Chen Tao		Xu Hang	Shi Jina

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OWNER:



**Middle East  
Kimiaye Pars Company**

LICENSING	HALDOR TOPSØE A/S	DOCUMENT NAME	JOB NO.	SOC. NO.	REV.
CONTRACTOR	TCC 中國天辰工程有限公司	CONTRACTOR DRAWING NO.			

MKP-11-DE-8500-PS09-PID-004	SHEET 01	TOTAL 01
SUB-CONTRACTOR DRAWING NO.		
SHEET -		TOTAL -

P&ID FLARE STACK I		PROJECT	MKP Methanol Project
		UNIT	Flare
		PHASE	Detail Engineering
SCALE: -	SHEET: 1	TOT.: 1	SIZE: A1
OWNER DWG NO.	MKP-11-DE-8500-PR-PID-004		

Counter	Sign	Date

# Node 7009

D 8502	Fuel Gas Buffer Drum
ID x LENGTH(T)	600x1500 mm
DESIGN PRESS.	10 barg
DESIGN TEMP.	85 °C
INSULATION	NONE
CLADDING/LINING	NONE

X 8501	Flare Front Generator

PIL 8501A~D	Pilot (with FFG & HED)

## GENERAL NOTES

- GENERAL NOTE:
- 1) LOW POINT DRAINS AND HIGH POINT VENT MUST BE ADDED DURING DETAILED ENGINEERING.
  - 2) FLARE LINE WITH AN UPWARD SLOPE SHALL ADD LOW POINT DRAINS, THE DETAIL INFORMATION ABOUT IT SHOULD SPECIFY IN DE PHASE.
- NOTE:
- 1) XL-01-04: PILOT CONDITION INDICATION LAMP, WHEN PIL-8501A/B/C/D ARE IN NORMAL CONDITION, THE RELEVANT LAMP IS ON.
  - 2) TAL-01-04: PILOT TEMPERATURE LOW ALARM LAMP, WHEN THE TEMPERATURE OF ANY ONE IN PIL-8501A/B/C/D IS LOWER THAN 150 °C, THE RELEVANT LAMP IS ON.
  - 3) PIPE PRESSURE AFTER PRESSURE REDUCING VALVE SHALL BE VERIFIED DURING DETAILED ENGINEERING PHASE.
  - 4) THERMOCOUPLE IS THE K TYPE DUAL SHEATHE THERMOCOUPLE, ONE IS DUTY, ANOTHER ONE IS SPARE.
  - 5) FFG WILL BE SUPPLIED AS THE COMPLETE SUPPLY SET BY VENDOR.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

▲	Approved For Construction	20.1.2017	Chen Tao		Xu Hang	Shi Jing
▲	Approved For Construction	20.12.2016	Chen Tao		Xu Hang	Shi Jing
▲	Approved For Construction	12.10.2016	Chen Tao		Xu Hang	Shi Jing
▲	Issued For Comments	31.8.2016	Chen Tao		Xu Hang	Shi Jing

REV.	DESCRIPTION	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE

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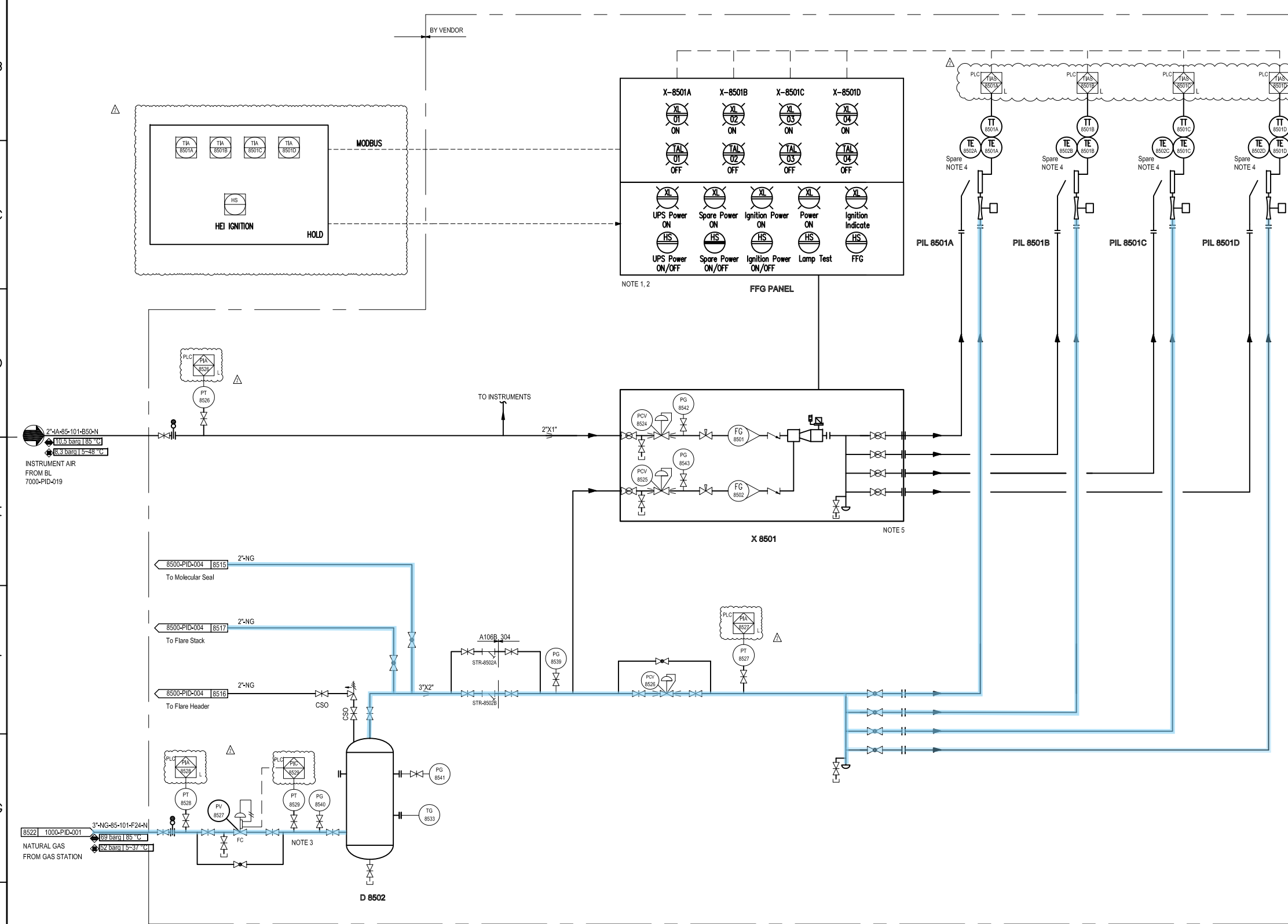
OWNER:

**Middle East  
Kimiya Pars Company**

LICENSING	HALDOR TOPSØE A/S	DOCUMENT NAME	JOB NO.	SOC. OFF.	REV.

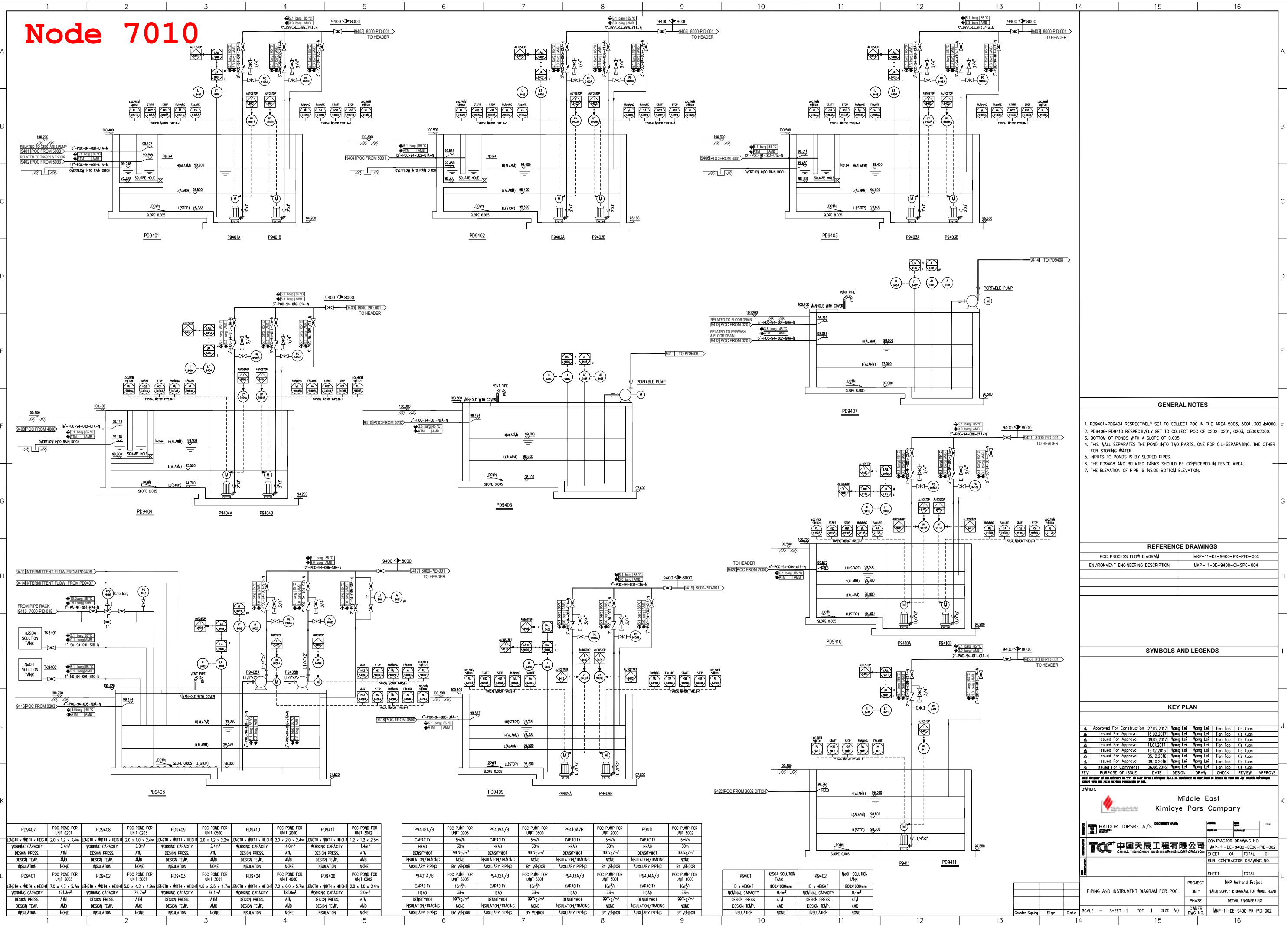
CONTRACTOR	TCC 中國天辰工程有限公司 CHINA TIANGHEN ENGINEERING CORPORATION	CONTRACTOR DRAWING NO.	MKP-11-DE-8500-PS09-PID-005
		SHEET	01 TOTAL 01
		SUB-CONTRACTOR DRAWING NO.	
		SHEET	- TOTAL -

P&ID FLARE STACK II		PROJECT	MKP Methanol Project
		UNIT	Flare
		PHASE	Detail Engineering
SCALE: -	SHEET: 1	TOT.: 1	SIZE: A1
OWNER DWG NO.	MKP-11-DE-8500-PR-PID-005		



Counter	Sign	Date

# Node 7010



### GENERAL NOTES

1. PD9401-PD9404 RESPECTIVELY SET TO COLLECT POC IN THE AREA 5003, 5001, 3001&4000.
2. PD9406-PD9410 RESPECTIVELY SET TO COLLECT POC OF 0202, 0201, 0203, 0500&2000.
3. BOTTOM OF PONDS WITH A SLOPE OF 0.005.
4. THIS WALL SEPARATES THE POND INTO TWO PARTS, ONE FOR OIL-SEPARATING, THE OTHER FOR STORING WATER.
5. INPUTS TO PONDS IS BY SLOPED PIPES.
6. THE PD9408 AND RELATED TANKS SHOULD BE CONSIDERED IN FENCE AREA.
7. THE ELEVATION OF PIPE IS INSIDE BOTTOM ELEVATION.

### REFERENCE DRAWINGS

POC PROCESS FLOW DIAGRAM	MKP-11-DE-9400-PR-PD-005
ENVIRONMENT ENGINEERING DESCRIPTION	MKP-11-DE-9400-CI-SPC-004

### SYMBOLS AND LEGENDS

### KEY PLAN

Approved For Construction	27.02.2017	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	16.02.2017	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	09.02.2017	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	11.01.2017	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	19.12.2016	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	05.12.2016	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Approval	09.10.2016	Wang Lei	Wang Lei	Tian Tao	Xie Xuan
Issued For Comments	06.06.2016	Wang Lei	Wang Lei	Tian Tao	Xie Xuan

OWNER: Middle East  
Kimiaye Pars Company

HALDOR TOPSOE A/S	CONTRACTOR DRAWING NO.	MKP-11-DE-9400-EC08-PD-002
TCC 中國天辰工程有限有限公司	CONTRACTOR DRAWING NO.	MKP-11-DE-9400-EC08-PD-002
	SHEET	01 TOTAL 01
	SUB-CONTRACTOR DRAWING NO.	

PROJECT	MKP Methanol Project
UNIT	WATER SUPPLY & DRAINAGE FOR WHOLE PLANT
PHASE	DETAIL ENGINEERING
OWNER	MKP-11-DE-9400-PR-PD-002
DWG NO.	

POD	POC POND FOR UNIT	LENGTH x WIDTH x HEIGHT	WORKING CAPACITY	DESIGN PRESS.	DESIGN TEMP.	INSULATION
PD9407	POC POND FOR UNIT 0201	2.0 x 1.2 x 3.4m	2.4m³	ATM	AMB	NONE
PD9408	POC POND FOR UNIT 0203	2.0 x 1.0 x 2.4m	2.0m³	ATM	AMB	NONE
PD9409	POC POND FOR UNIT 0500	2.0 x 1.2 x 2.2m	2.4m³	ATM	AMB	NONE
PD9410	POC POND FOR UNIT 2000	2.0 x 2.0 x 2.4m	4.0m³	ATM	AMB	NONE
PD9411	POC POND FOR UNIT 3002	1.2 x 1.2 x 2.5m	1.4m³	ATM	AMB	NONE
PD9401	POC POND FOR UNIT 5003	7.0 x 4.3 x 5.7m	131.5m³	ATM	AMB	NONE
PD9402	POC POND FOR UNIT 5001	5.0 x 4.2 x 4.9m	72.7m³	ATM	AMB	NONE
PD9403	POC POND FOR UNIT 3001	4.5 x 2.5 x 4.7m	36.1m³	ATM	AMB	NONE
PD9404	POC POND FOR UNIT 4000	7.0 x 6.0 x 5.7m	181.0m³	ATM	AMB	NONE
PD9406	POC POND FOR UNIT 0202	2.0 x 1.0 x 2.4m	2.0m³	ATM	AMB	NONE

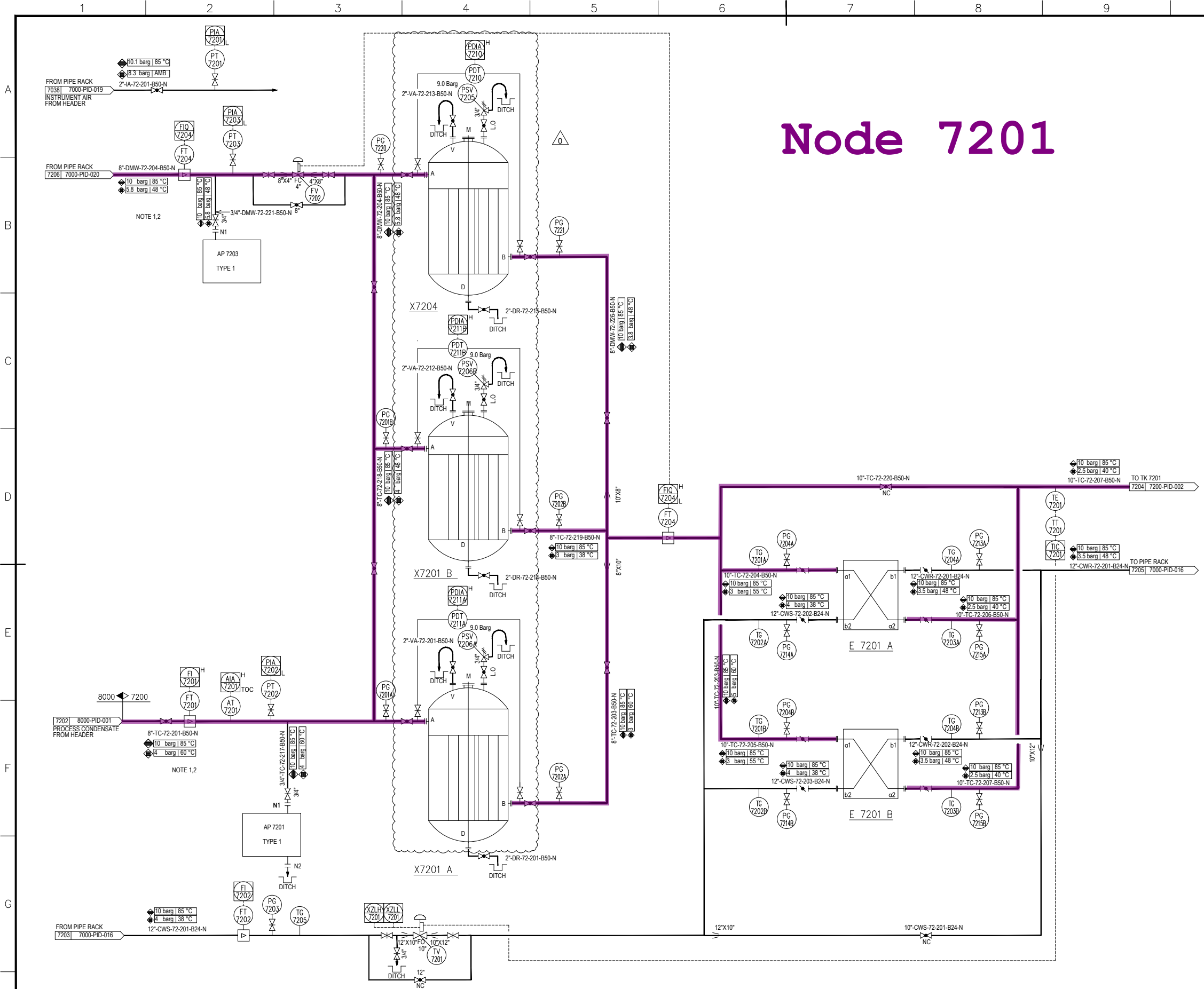
POD	POC PUMP FOR UNIT	CAPACITY	HEAD	DENSITY/WT	INSULATION/TRACING	AUXILIARY PIPING
P9408A/B	POC PUMP FOR UNIT 0203	5m³/h	30m	997kg/m³	NONE	BY VENDOR
P9409A/B	POC PUMP FOR UNIT 0500	5m³/h	30m	997kg/m³	NONE	BY VENDOR
P9410A/B	POC PUMP FOR UNIT 2000	12m³/h	30m	997kg/m³	NONE	BY VENDOR
P9411	POC PUMP FOR UNIT 3002	5m³/h	30m	997kg/m³	NONE	BY VENDOR
P9401A/B	POC PUMP FOR UNIT 5003	10m³/h	35m	997kg/m³	NONE	BY VENDOR
P9402A/B	POC PUMP FOR UNIT 5001	10m³/h	35m	997kg/m³	NONE	BY VENDOR
P9403A/B	POC PUMP FOR UNIT 3001	2.0m³/h	35m	997kg/m³	NONE	BY VENDOR
P9404A/B	POC PUMP FOR UNIT 4000	10m³/h	35m	997kg/m³	NONE	BY VENDOR

TK9401	H2SO4 SOLUTION TANK	TK9402	NaOH SOLUTION TANK
ID x HEIGHT	800x1000mm	ID x HEIGHT	800x1000mm
NOMINAL CAPACITY	0.4m³	NOMINAL CAPACITY	0.4m³
DESIGN PRESS.	ATM	DESIGN PRESS.	ATM
DESIGN TEMP.	AMB	DESIGN TEMP.	AMB
INSULATION	NONE	INSULATION	NONE

Counter Sign Sign Date

SCALE - SHEET 1 TOT. 1 SIZE A0

# Node 7201



## GENERAL NOTES

- NOTE 1: POLISHING UNIT IS GENERALLY REVISED BECAUSE DMW WATER FROM DAMAVAND NEEDS TO BE POLISHED, THE CAPACITY OF POLISHING UNIT WAS REVISED FROM 126 M3/H TO 250 M3/H. THE DRAWING IS ONLY FOR REFERENCE, VENDOR SHALL FINISH THE DETAILED DESIGN OF THIS DRAWING AND APPROVED BY TCC.
- NOTE 2: POLISHING UNIT SHOULD BE PACKAGE SUPPLIED, INCLUDING ALL THE EQUIPMENT, PLC, INSTRUMENT, CONTROL VALVE SHOWN IN P&ID, MOTORS AND PUMPS. THE MAIN PROCESS P7002 AB, MP 7002 AB, TK 7201 AND TK7001 1/2 WITH LEVEL TRANSMITTER AND GAUGE SHALL BE IN TCC'S WORKING SCOPE.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
△	Approved for Construction	23.01.2017	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Approval	05.01.2017	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Approval	12.12.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Approval	10.10.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Approval	27.07.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Review	05.07.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
△	Issued For Comments	06.06.2016	Liang Zhipeng	Tian Tao	Xie Xuan		

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OWNER: Middle East Kimiaye Pars Company

HALDOR TOPSØE A/S DOCUMENT NAME: \_\_\_\_\_ JOB NO. \_\_\_\_\_ DOC. GRP. \_\_\_\_\_ REV. \_\_\_\_\_

**TCC 中國天辰工程有限有限公司** CONTRACTOR DRAWING NO. MKP-11-DE-7200-EE06-PID-001

SHEET 01 TOTAL 01 SUB-CONTRACTOR DRAWING NO. \_\_\_\_\_

SHEET \_\_\_\_\_ TOTAL \_\_\_\_\_ PROJECT MKP Methanol Project UNIT POLISHING UNIT PHASE DETAIL ENGINEERING

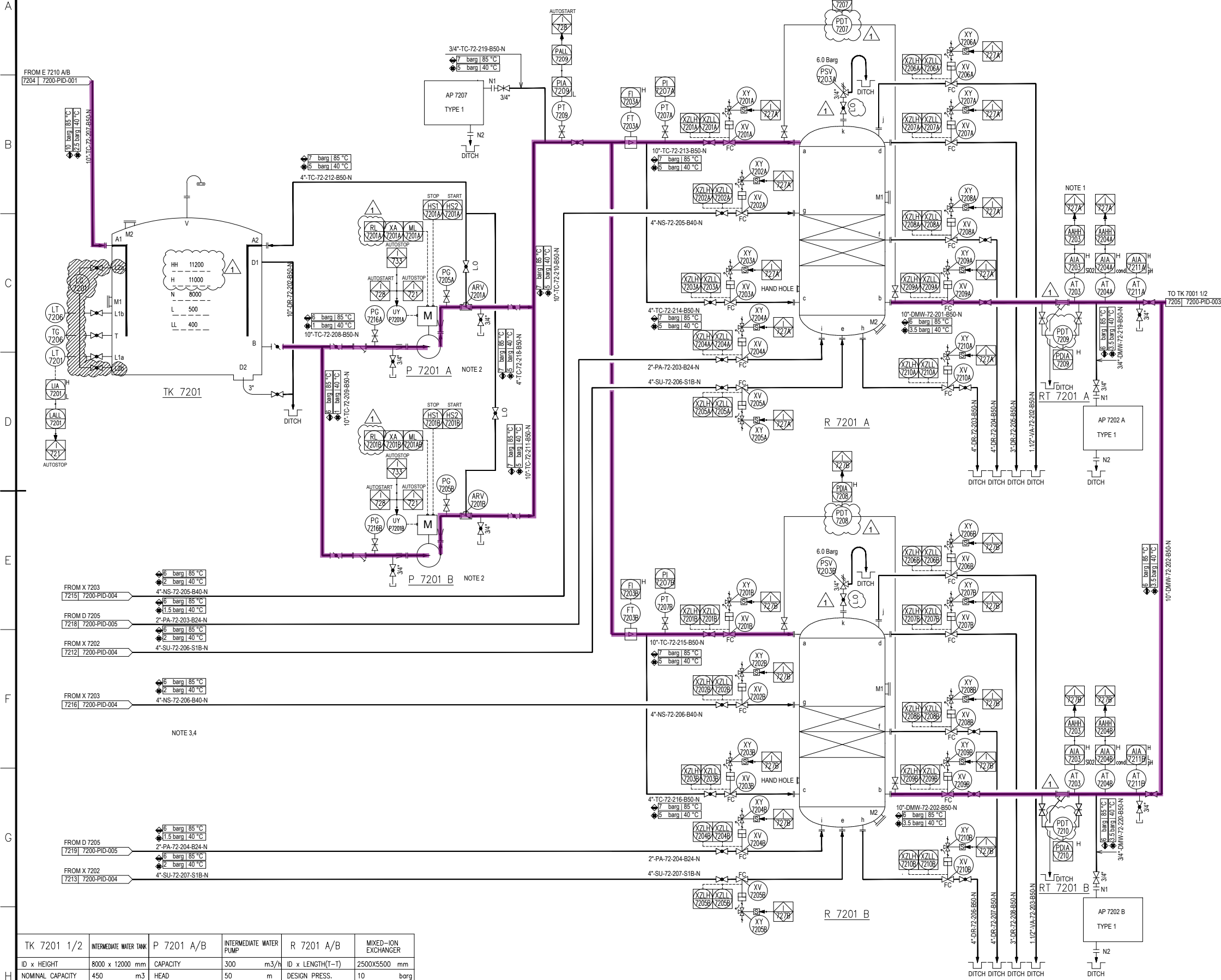
SCALE - SHEET 1 TOT. 1 SIZE A1 OWNER DWG. NO. MKP-11-DE-7200-PR-PID-001

	E 7201 A/B	PLATE HEAT EXCHANGER	X 7201 A	CARTRIDGE FILTER	X 7201 B	CARTRIDGE FILTER	X 7204	CARTRIDGE FILTER
EXCHANGE AREA	280	m <sup>2</sup>	CAPACITY	150	m <sup>3</sup> /h	CAPACITY	150	m <sup>3</sup> /h
DESIGN PRESS.	10	barg	ID x HEIGHT	1000 x 1500 mm	ID x HEIGHT	1000 x 1500 mm	ID x HEIGHT	1000 x 1500 mm
DESIGN TEMP.	85	°C	DESIGN PRESS.	10	barg	DESIGN PRESS.	10	barg
TYPE	PLATE	DESIGN TEMP.	85	°C	DESIGN TEMP.	85	°C	DESIGN TEMP.
MATERIAL	SS304	MATERIAL CASING	C.S+R.L	MATERIAL CASING	C.S+R.L	MATERIAL CASING	C.S+R.L	MATERIAL CASING
INSULATION	NONE	MATERIAL FILTER ELEMENT	PP	MATERIAL FILTER ELEMENT	PP	MATERIAL FILTER ELEMENT	PP	MATERIAL FILTER ELEMENT
ELEV. OF FOUNDATION	EL 100.80 m	INSULATION	NONE	INSULATION	NONE	INSULATION	NONE	INSULATION
		ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION

Counter Signing	Sign	Date
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# Node 7201



- FROM X 7203  
 6 barg | 85 °C  
 2 barg | 40 °C  
 4"-NS-72-205-B40-N  
 7215 | 7200-PID-004
- FROM D 7205  
 6 barg | 85 °C  
 1.5 barg | 40 °C  
 2"-PA-72-203-B24-N  
 7218 | 7200-PID-005
- FROM X 7202  
 6 barg | 85 °C  
 2 barg | 40 °C  
 4"-SU-72-206-S1B-N  
 7212 | 7200-PID-004
- FROM X 7203  
 6 barg | 85 °C  
 2 barg | 40 °C  
 4"-NS-72-206-B40-N  
 7216 | 7200-PID-004

NOTE 34

- FROM D 7205  
 6 barg | 85 °C  
 1.5 barg | 40 °C  
 2"-PA-72-204-B24-N  
 7219 | 7200-PID-005
- FROM X 7202  
 6 barg | 85 °C  
 2 barg | 40 °C  
 4"-SU-72-207-S1B-N  
 7213 | 7200-PID-004

## GENERAL NOTES

- NOTE 1: THIS INSTRUMENT IS A TWO-CHANNEL SILICON TRANSMITTER.
- NOTE 2: P7201 A/B STANDBY PUMP AUTOSTARTS WHEN PRESSURE INDICATED ON PT-7209 IS 1 BAR.
- NOTE 3: POLISHING UNIT IS GENERALLY REVISED BECAUSE DMW WATER FROM DAMAVAND NEEDS TO BE POLISHED, THE CAPACITY OF POLISHING UNIT WAS REVISED FROM 126 M3/H TO 250 M3/H. THE DRAWING IS ONLY FOR REFERENCE, VENDOR SHALL FINISH THE DETAILED DESIGN OF THIS DRAWING AND APPROVED BY TCC.
- NOTE 4: POLISHING UNIT SHOULD BE PACKAGE SUPPLIED, INCLUDING ALL THE EQUIPMENT, PLC, INSTRUMENT, CONTROL VALVE SHOWN IN P&ID, MOTORS AND PUMPS. THE MAIN PROCESS P7002 A/B, MP 7002 A/B, TK 7201 AND TK7001 1/2 WITH LEVEL TRANSMITTER AND GAUGE SHALL BE IN TCC'S WORKING SCOPE.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
△	Approved For Construction	23.01.2017	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Approved For Construction	05.01.2017	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Issued For Approval	12.12.2016	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Issued For Approval	10.10.2016	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Issued For Approval	27.07.2016	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Issued For Review	05.07.2016	Liang Zhipeng		Tian Tao	Xie Xuan	
△	Issued For Comments	06.06.2016	Liang Zhipeng		Tian Tao	Xie Xuan	

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OWNER: **Middle East Kimiaye Pars Company**

HALDOR TOPSØE A/S DOCUMENT NAME: \_\_\_\_\_ JOB NO. \_\_\_\_\_ DOC. NO. \_\_\_\_\_ REV. \_\_\_\_\_

**TCC 中國天辰工程有限** CONTRACTOR DRAWING NO. MKP-11-DE-7200-EE06-PID-002

SHEET 01 TOTAL 01 SUB-CONTRACTOR DRAWING NO. \_\_\_\_\_

SHEET TOTAL PROJECT MKP Methanol Project UNIT POLISHING UNIT PHASE DETAIL ENGINEERING

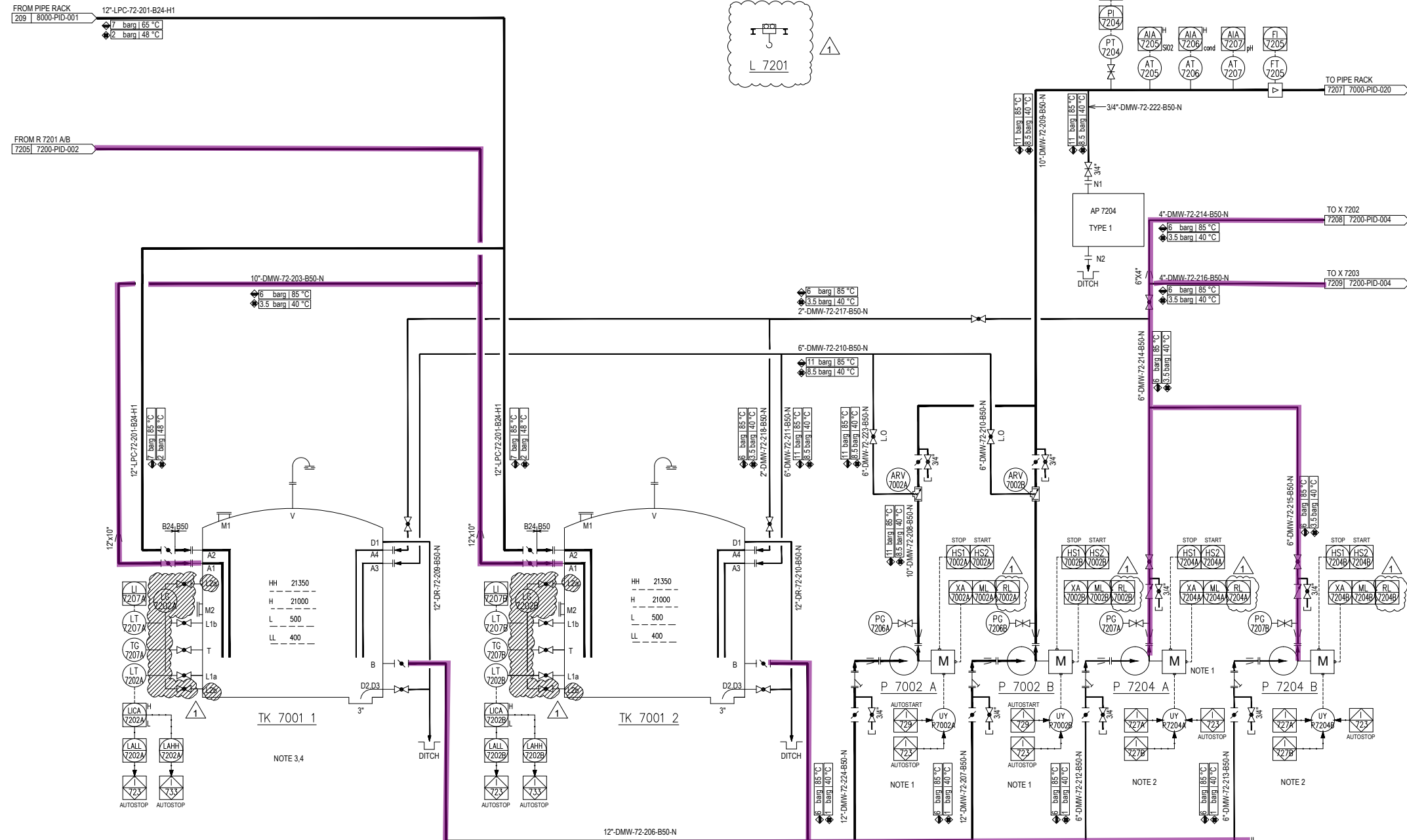
MIXED-ION EXCHANGER P&ID FOR POLISHING UNIT SCALE - SHEET 1 TOT. 1 SIZE A1 OWNER DWG. NO. MKP-11-DE-7200-PR-PID-002

TK 7201 1/2	INTERMEDIATE WATER TANK	P 7201 A/B	INTERMEDIATE WATER PUMP	R 7201 A/B	MIXED-ION EXCHANGER
ID x HEIGHT	8000 x 12000 mm	CAPACITY	300 m <sup>3</sup> /h	ID x LENGTH(T-T)	2500X5500 mm
NOMINAL CAPACITY	450 m <sup>3</sup>	HEAD	50 m	DESIGN PRESS.	10 barg
DESIGN PRESS.	ATM barg	DENSITY@OT	992.2 kg/m <sup>3</sup>	DESIGN TEMP.	85 °C
DESIGN TEMP.	85 °C	INSULATION/TRACING	NONE	INSULATION	NONE
INSULATION	NONE	AUXILIARY PIPING	By Vendor	MATERIAL	C.S.
MATERIAL	SS304	TYPE	CENTRIFUGAL	CLADDING/LINING	RUBBER
ELEV. OF FOUNDATION	EL 100.80 m	MATERIAL	SS304	ELEV. OF FOUNDATION	EL 100.80 m
		ELEV. OF FOUNDATION	EL 100.80 m		

Counter Signing Sign Date



# Node 7201



## GENERAL NOTES

- NOTE 1: PUMP P7002 A/B AUTOSTARTS WHEN PRESSURE INDICATED ON PT-7204 IS 1 BAR.
- NOTE 2: PUMP P7204 A/B AUTOSTARTS WHEN REGENERATION PROCESS STARTS, STANDBY PUMP STARTS WHEN THE WORKING PUMP IS MALFUNCTIONING.
- NOTE 3: POLISHING UNIT IS GENERALLY REVISED BECAUSE DMW WATER FROM DAMAVAND NEEDS TO BE POLISHED, THE CAPACITY OF POLISHING UNIT WAS REVISED FROM 126 M3/H TO 250 M3/H. THE DRAWING IS ONLY FOR REFERENCE, VENDOR SHALL FINISH THE DETAILED DESIGN OF THIS DRAWING AND APPROVED BY TCC.
- NOTE 4: POLISHING UNIT SHOULD BE PACKAGE SUPPLIED, INCLUDING ALL THE EQUIPMENT, PLC, INSTRUMENT, CONTROL VALVE SHOWN IN P&ID, MOTORS AND PUMPS. THE MAIN PROCESS P7002 A/B, MP 7002 A/B, TK 7201 AND TK7001 1/2 WITH LEVEL TRANSMITTER AND GAUGE SHALL BE IN TCC'S WORKING SCOPE.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
1	Approved For Construction	23.01.2017	Liang Zhipeng	Tian Tao	Xie Xuan		
2	Approved For Construction	05.01.2017	Liang Zhipeng	Tian Tao	Xie Xuan		
3	Issued For Approval	12.12.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
4	Issued For Approval	10.10.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
5	Issued For Approval	27.07.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
6	Issued For Review	05.07.2016	Liang Zhipeng	Tian Tao	Xie Xuan		
7	Issued For Comments	06.06.2016	Liang Zhipeng	Tian Tao	Xie Xuan		

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OWNER: **Middle East Kimiaye Pars Company**

HALDOR TOPSØE A/S DOCUMENT NAME: PROJECT NO.: DOC. NO.: REV.:

**TCC 中國天辰工程有限** CONTRACTOR DRAWING NO. MKP-11-DE-7200-EE06-PID-003

SHEET 01 TOTAL 01 SUB-CONTRACTOR DRAWING NO. SHEET TOTAL

DMW STORAGE AND FEEDING P&ID FOR POLISHING UNIT PROJECT: MKP Methanol Project UNIT: POLISHING UNIT PHASE: DETAIL ENGINEERING

SCALE - SHEET 1 TOT. 1 SIZE A1 OWNER DWG. NO. MKP-11-DE-7200-PR-PID-003

TK 7001 1/2	DEMIN WATER TANK	P 7002 A/B	DEMIN WATER PUMP	P 7204 A/B	REGENERATION PUMP	L 7201	HOIST
ID x HEIGHT	15000 x 22000 mm	CAPACITY	265 m <sup>3</sup> /h	CAPACITY	85 m <sup>3</sup> /h	TYPE	ELECTRICAL HOIST
NOMINAL CAPACITY	3500 m <sup>3</sup>	HEAD	85 m	HEAD	35 m	CAPACITY	2 t
DESIGN PRESS.	ATM barg	DENSITY@OT	992.2 kg/m <sup>3</sup>	DENSITY@OT	992.2 kg/m <sup>3</sup>	LIFT HEIGHT	4.5 m
DESIGN TEMP.	85 °C	INSULATION/TRACING	NONE	INSULATION/TRACING	NONE	SLIDING DISTANCE	41 m
INSULATION	NONE	AUXILIARY PIPING	By Vendor	AUXILIARY PIPING	By Vendor		
MATERIAL	SS 304	TYPE	CENTRIFUGAL	TYPE	CENTRIFUGAL		
ELEV. OF FOUNDATION	EL 100.80 m	MATERIAL	SS304	MATERIAL	SS304		
		ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION	EL 100.80 m		

Counter Signing	Sign	Date
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# Node 7201

## GENERAL NOTES

- NOTE 1: STORAGE BOUND SHALL BE PROVIDED WITH CHEMICAL PROOF FLOORING, RESIST TO ACID AND CAUSTIC.
- NOTE 2: ACID AND CAUSTIC STORAGE TANKS TO BE LOCATED IN SEPARATE BOUNDED AREAS.
- NOTE 3: H2SO4 IS USED INSTEAD OF HCl. EJECTORS WERE REPLACED BY DOSING PUMPS TO GUARANTEE THE CONCENTRATION OF REGENERATION ACID/ALKALI.

### +GENERAL NOTES

- NOTE 1: PUMPS TO BE LOCATED IN KERBED WALL.
- NOTE 2: AN EMERGENCY EYEWASH AND SHOWER TO BE PROVIDED AS CLOSE AS POSSIBLE.
- NOTE 3: THE ENTIRE PIPING SYSTEM CONTAINING 46% CAUSTIC SOLUTION SHALL BE PROPERLY HEATED, AND INSULATED TO PREVENT THE CAUSTIC SOLUTION FROM FREEZING. ELECTRICAL/STEAM HEAT TRACING TO BE APPLIED (20°C).
- NOTE 4: REQUIRED THE EARTHING OF TRUCK FOR UNLOADING, WITH UNLOCK OR EARTHING SWITCH.
- NOTE 5: PROVIDE DIFFERENT COLORS FOR THE ACID AND CAUSTIC LINES AND TRUCK UNLOADING CONNECTIONS, IN ORDER TO AVOID OPERATOR FAULT.
- NOTE 6: POLISHING UNIT IS GENERALLY REVISED BECAUSE DMW WATER FROM DAMAVAND NEEDS TO BE POLISHED, THE CAPACITY OF POLISHING UNIT WAS REVISED FROM 126 M3/H TO 250 M3/H. THE DRAWING IS ONLY FOR REFERENCE, VENDOR SHALL FINISH THE DETAILED DESIGN OF THIS DRAWING AND APPROVED BY TCC.
- NOTE 7: POLISHING UNIT SHOULD BE PACKAGE SUPPLIED, INCLUDING ALL THE EQUIPMENT, PLC, INSTRUMENT, CONTROL VALVE SHOWN IN P&ID, MOTORS AND PUMPS. THE MAIN PROCESS P7002 A/B, MP 7202 A/B, TK 7201 AND TK7001 1/2 WITH LEVEL TRANSMITTER AND GAUGE SHALL BE IN TCC'S WORKING SCOPE.
- NOTE 8: STANDBY PUMP SHALL BE CONSIDERED FOR ACID TRANSFER PUMP AND ALKALI TRANSFER PUMP. IF THERE IS NO SPACE FOR INSTALLATION, THE STANDBY PUMP WILL BE STORED IN THE WAREHOUSE. THIS MATTER WILL BE DISCUSSED WITH POLISHING UNIT PACKAGE VENDOR.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS


## KEY PLAN

REV.	PURPOSE OF ISSUE	DATE	DESIGN	DRAW	CHECK	REVIEW	APPROVE
Δ	Approved For Construction	10.02.2017	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Approval	23.01.2017	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Approval	05.01.2017	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Approval	12.12.2016	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Approval	10.10.2016	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Approval	27.07.2016	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Review	05.07.2016	Uang Zhipeng		Tian Tao	Xie Xuan	
Δ	Issued For Comments	06.06.2016	Uang Zhipeng		Tian Tao	Xie Xuan	

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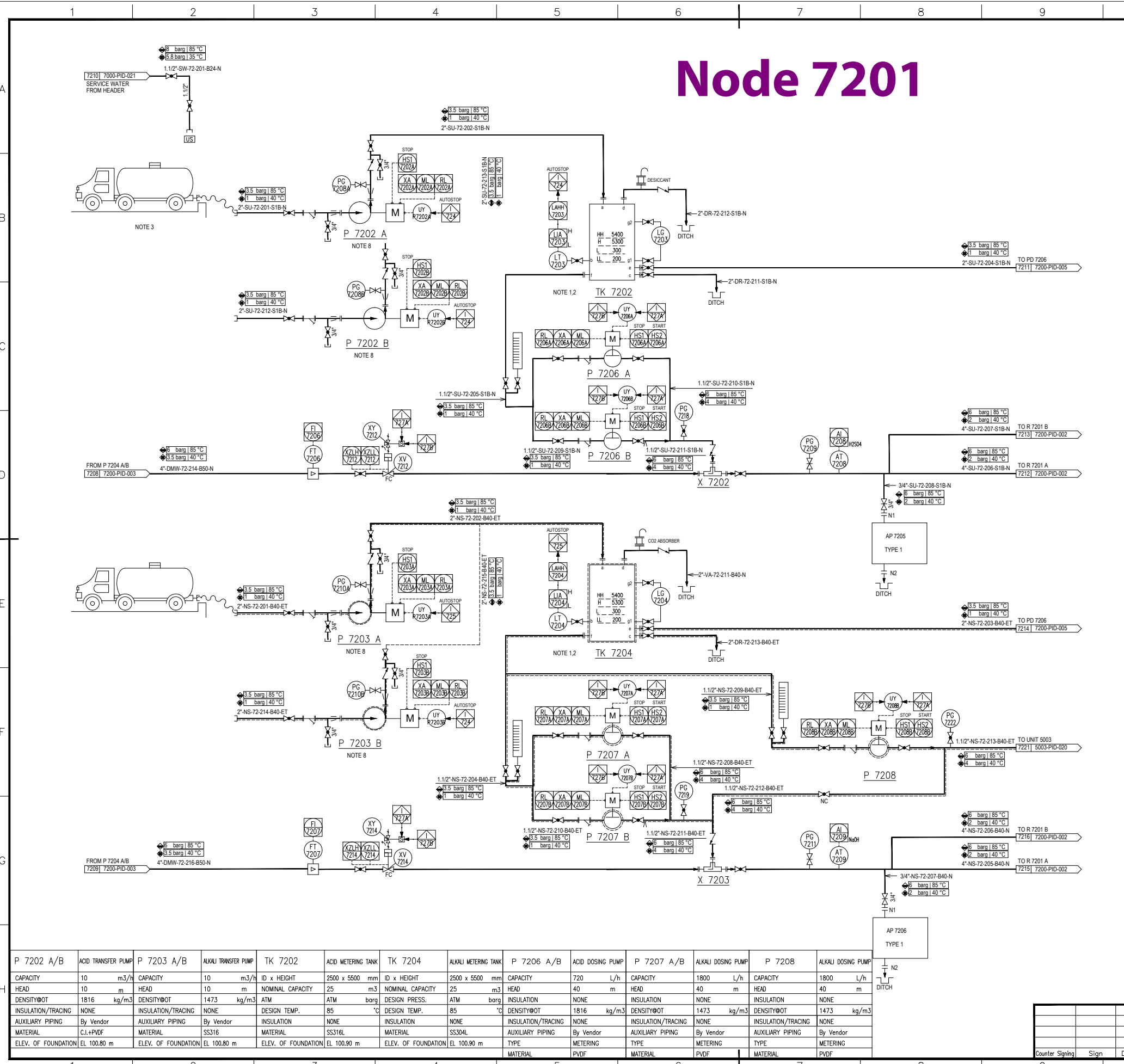
OWNER:

**Middle East  
Kimiaye Pars Company**

 <b>TCC</b> 中国天辰工程有限公司 CHINA TIANCHEN ENGINEERING CORPORATION	<b>HALDOR TOPSØE A/S</b> OPERATOR GENERAL	DOCUMENT NAME: SHEET NO.: SHEET TOTAL:	JOB NO.: SHEET TOTAL:	REV. NO.: SHEET TOTAL:
	CONTRACTOR DRAWING NO. MKP-11-DE-7200-EE06-PID-004 SHEET 01 TOTAL			
SUB-CONTRACTOR DRAWING NO.				
SHEET TOTAL				

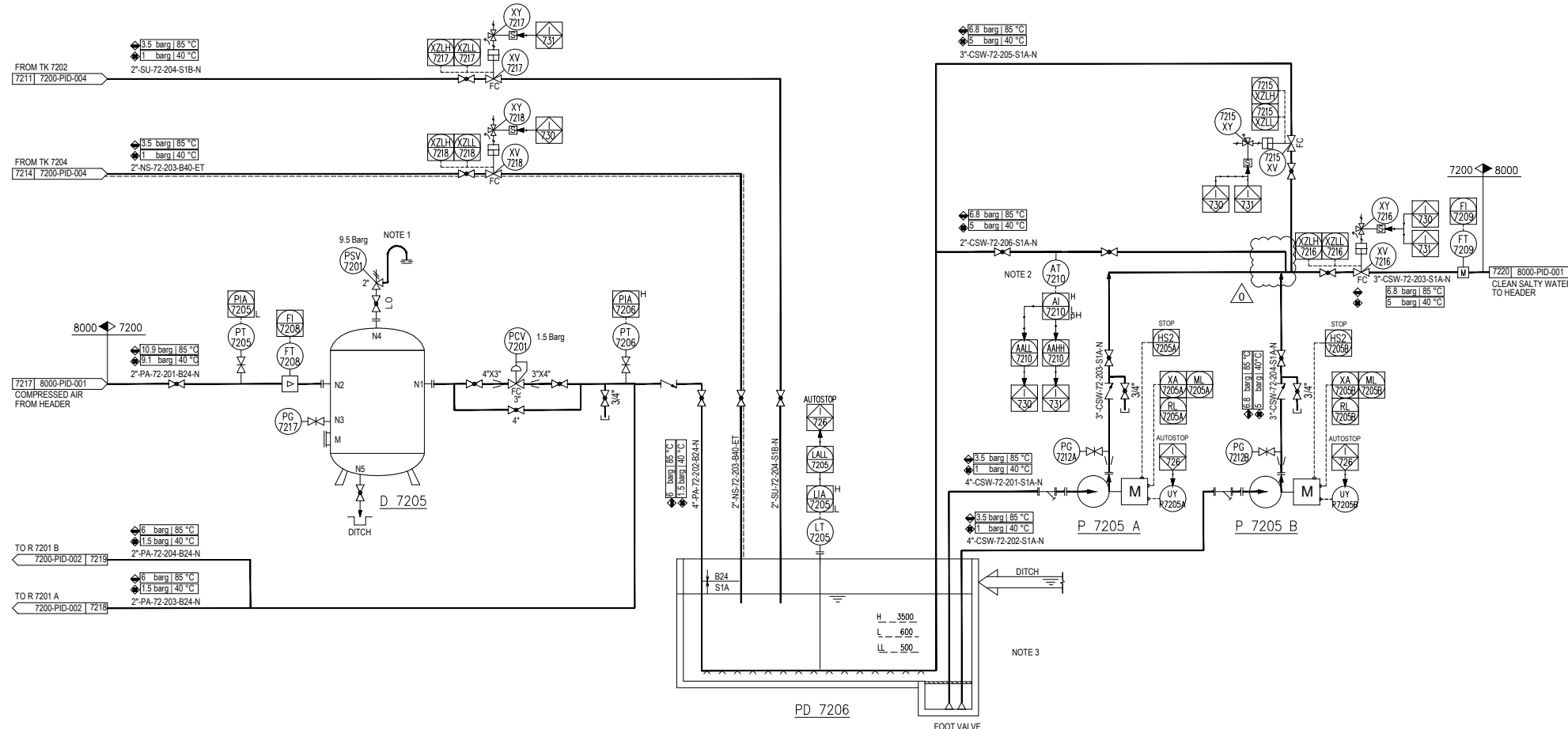
<b>ACID AND ALKALI REGENERATION P&amp;ID FOR POLISHING UNIT</b>	PROJECT	MKP Methanol Project
	UNIT	POLISHING UNIT
	PHASE	DETAIL ENGINEERING

SCALE	SHEET 1	TOT. 1	SIZE A1	OWNER DWG NO.	MKP-11-DE-7200-PR-PID-004
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P 7202 A/B	ACID TRANSFER PUMP	P 7203 A/B	ALKALI TRANSFER PUMP	TK 7202	ACID METERING TANK	TK 7204	ALKALI METERING TANK	P 7206 A/B	ACID DOSING PUMP	P 7207 A/B	ALKALI DOSING PUMP	P 7208	ALKALI DOSING PUMP
CAPACITY	10 m <sup>3</sup> /h	CAPACITY	10 m <sup>3</sup> /h	ID x HEIGHT	2500 x 5500 mm	ID x HEIGHT	2500 x 5500 mm	CAPACITY	720 L/h	CAPACITY	1800 L/h	CAPACITY	1800 L/h
HEAD	10 m	HEAD	10 m	NOMINAL CAPACITY	25 m <sup>3</sup>	NOMINAL CAPACITY	25 m <sup>3</sup>	HEAD	40 m	HEAD	40 m	HEAD	40 m
DENSITY@OT	1816 kg/m <sup>3</sup>	DENSITY@OT	1473 kg/m <sup>3</sup>	DESIGN PRESS.	ATM barg	DESIGN PRESS.	ATM barg	INSULATION	NONE	INSULATION	NONE	INSULATION	NONE
INSULATION/TRACING	NONE	INSULATION/TRACING	NONE	DESIGN TEMP.	85 °C	DESIGN TEMP.	85 °C	DENSITY@OT	1816 kg/m <sup>3</sup>	DENSITY@OT	1473 kg/m <sup>3</sup>	DENSITY@OT	1473 kg/m <sup>3</sup>
AUXILIARY PIPING	By Vendor	AUXILIARY PIPING	By Vendor	INSULATION	NONE	INSULATION	NONE	INSULATION/TRACING	NONE	INSULATION/TRACING	NONE	INSULATION/TRACING	NONE
MATERIAL	C.I.+PVDF	MATERIAL	SS316	MATERIAL	SS316L	MATERIAL	SS304L	AUXILIARY PIPING	By Vendor	AUXILIARY PIPING	By Vendor	AUXILIARY PIPING	By Vendor
ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION	EL 100.80 m	ELEV. OF FOUNDATION	EL 100.90 m	ELEV. OF FOUNDATION	EL 100.90 m	TYPE	METERING	TYPE	METERING	TYPE	METERING
								MATERIAL	PVDF	MATERIAL	PVDF	MATERIAL	PVDF

# Node 7201



## GENERAL NOTES

- NOTE 1: VENT WILL CONNECT TO A SAFE LOCATION
- NOTE 2: AT-7210 HAS AN INDICATOR ON THE SITE, TO BE VISIBLE FROM THE LOCATION OF ALKALI AND ACID VALVES ON THE LINE SU-204 AND NS-203. PD 7206 WILL BE NEUTRALIZED AUTOMATICALLY.
- NOTE 3: INTERNAL SURFACE OF PD-7206 SHALL BE EQUIPPED WITH UNIT ACID BRICK.
- NOTE 4: POLISHING UNIT IS GENERALLY REVISED BECAUSE DMW WATER FROM DAMAVAND NEEDS TO BE POLISHED. THE CAPACITY OF POLISHING UNIT WAS REVISED FROM 126 M3/H TO 250 M3/H. THE DRAWING IS ONLY FOR REFERENCE. VENDOR SHALL FINISH THE DETAILED DESIGN OF THIS DRAWING AND APPROVED BY TCC.
- NOTE 5: POLISHING UNIT SHOULD BE PACKAGE SUPPLIED, INCLUDING ALL THE EQUIPMENT, PLC, INSTRUMENT, CONTROL VALVE SHOWN IN P&ID. MOTORS AND PUMPS THE MAIN PROCESS P7002 AB, MP 7002 AB, TK 7201 AND TK7001 1/2 WITH LEVEL TRANSMITTER AND GAUGE SHALL BE IN TCC'S WORKING SCOPE.

## REFERENCE DRAWINGS

## SYMBOLS AND LEGENDS

## KEY PLAN

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Δ	Issued For Approval	05.01.2017	Liang Zhipeng		Tian Tao	Xie Xuan	
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OWNER:

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Kimiaye Pars Company**

		DOCUMENT NAME:	CONTRACTOR DRAWING NO.
		CONTRACTOR DRAWING NO.	MKP-11-DE-7200-EE06-PID-005
SHEET 01		TOTAL 01	
SUB-CONTRACTOR DRAWING NO.			
SHEET		TOTAL	

PROJECT	MKP Methanol Project
UNIT	POLISHING UNIT
PHASE	DETAIL ENGINEERING
SCALE	- SHEET 1 TOT. 1 SIZE A1
OWNER DWG NO.	MKP-11-DE-7200-PR-PID-005

NOTE 4.5

PD 7206	NEUTRALIZATION PIT	P 7205 A/B	NEUTRALIZATION WATER PUMP	D 7205	COMPRESSED AIR VESSEL
L x B x H	1100 x 600 x 400 mm	CAPACITY	25 m <sup>3</sup> /h	ID x LENGTH(T-I)	2000 x 4880mm
NOMINAL CAPACITY	200 m <sup>3</sup>	HEAD	50 m	DESIGN PRESS.	10.5 barg
DESIGN PRESS.	ATM barg	DENSITY@OT	1000 kg/m <sup>3</sup>	DESIGN TEMP.	85 °C
DESIGN TEMP.	85 °C	INSULATION/TRACING	NONE	INSULATION	NONE
INSULATION	NONE	AUXILIARY PIPING	By Vendor	CLADDING/LINING	NONE
		TYPE	SELF-PRIMING	MATERIAL	SS304
		MATERIAL	SS316L	ELEV. OF FOUNDATION	EL 100.80 m
		ELEV. OF FOUNDATION	EL 100.50 m		

Counter Signing Sign Date